## A. INTRODUCTION

This transportation chapter examines the potential for the Proposed Action to result in significant adverse impacts on study area transportation systems through a comparison of 2023 conditions with the Proposed Action (the With-Action condition) to conditions in the future without the Proposed Action (the No-Action condition).

As described in Chapter 1, "Project Description," the Applicant is proposing several discretionary actions to facilitate a new mixed-use predominantly residential development (the "proposed project") on an 8.7-acre waterfront site in the Astoria neighborhood of Queens Community District (CD) 1. The Proposed Action, which includes a zoning map amendment, a zoning text amendment, and a City Map amendment, along with other related land use actions, would facilitate a new approximately 2,189,068 gross square feet (gsf) mixed-use development on the project site. The proposed project would be comprised of approximately 1,689 dwelling units (DU), approximately 109,470 gsf of local retail space (including a 25,000 gsf supermarket), a site for an elementary school with approximately 456 seats (PK-5), approximately 900 accessory parking spaces, and approximately 83,846 sf of publicly accessible open space. The project site is shown in Figure 1-1 in Chapter 1, "Project Description." It is anticipated that the proposed project would be completed in 2023.

The assessment of the Proposed Action's potential transportation impacts is based on the methodologies set forth in the *City Environmental Quality Review* (CEQR) *Technical Manual*.

## **B. PRINCIPAL CONCLUSIONS**

#### <u>Weekday</u> Traffic

Weekday AM(7:30-8:30 AM), midday (12-1 PM), and PM (4:30-5:30 PM) peak hour traffic conditions were evaluated at 30 intersections generally bounded by Hoyt Avenue North to the north, Broadway to the south,  $33^{rd}$  Street to the east, and  $4^{th}$  Street to the west. These 30 intersections, where project-generated trips are expected to be most concentrated, were analyzed for a reasonable worst-case development scenario (RWCDS) that assumes full completion of the nearby Halletts Point project, which has a 2022 build year.

The traffic impact analysis indicates that there would be a potential for significant adverse impacts at  $\underline{21}$  intersections during the weekday AM peak hour, nine intersections during the weekday midday peak hour, and  $\underline{17}$  intersections during the weekday PM peak hour, as outlined in Table 13-1<u>a</u>.

As the impacts shown in Table 13-1<u>a</u> would result from an increase of traffic volumes due to both the Proposed Action and the Halletts Point development, an additional impact analysis is included in this chapter as per guidance by the New York City Department of City Planning (DCP) and the New York City Department of Transportation (NYCDOT) to determine whether these impacts would occur absent the Halletts Point development. As discussed in detail in Section G, "Traffic," the analysis of future conditions without accounting for the Halletts Point development shows that, although the majority of

significant adverse impacts were identified at the same locations for both the future conditions, generally fewer impacts would occur absent the Halletts Point development. A total of 20 of the 30 analyzed intersections would be significantly adversely impacted in one or more peak hours as a result of the Proposed Action absent the Halletts Point development, while 23 of the 30 analyzed intersections would be impacted when accounting for the Halletts Point development.

Intersection	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour
1. 26 <sup>th</sup> Ave. & 4 <sup>th</sup> St.			
A. 26 <sup>th</sup> Ave. & 9 <sup>th</sup> St.			
2. 27 <sup>th</sup> Ave. & 4 <sup>th</sup> St.			Х
3. 27 <sup>th</sup> Ave. & 8 <sup>th</sup> St.	Х	Х	Х
4. 27 <sup>th</sup> Ave. & 12 <sup>th</sup> St.	Х		Х
5. 27 <sup>th</sup> Ave. & 14 <sup>th</sup> St.	X		
6. 27 <sup>th</sup> Ave. & 18 <sup>th</sup> St.			
7. Astoria Blvd. & 21 <sup>st</sup> St.	X	X	Х
8. Astoria Blvd. & 23 <sup>rd</sup> St.	X		Х
9. Astoria Blvd. & Crescent St.	X X	X	Х
10. Astoria Blvd. & 27 <sup>th</sup> St.	Х		
11. Astoria Blvd. & 28 <sup>th</sup> St.			
12. Astoria Blvd. & 29 <sup>th</sup> St.	Х	Х	Х
13. Astoria Blvd. & 30 <sup>th</sup> St.			
14. Astoria Blvd. & 31 <sup>st</sup> St.	Х		
15. Hoyt Ave. S./Astoria Blvd. &	Х	Х	Х
33 <sup>rd</sup> St.			21
16. Hoyt Ave. N. & 29 <sup>th</sup> St.	X		
17. Hoyt Ave. N. & 31 <sup>st</sup> St.	X		X
18. Astoria Blvd. N. & 32 <sup>nd</sup> St.	Х	X	Х
19. Astoria Blvd. & 8 <sup>th</sup> St.			Х
20. 30 <sup>th</sup> Ave. & 14 <sup>th</sup> St.	X X		
21. 30 <sup>th</sup> Ave. & 21 <sup>st</sup> St.	X		
22. Vernon Blvd. & Welling Court/8 <sup>th</sup> St.	Х	X	Х
23. Astoria Blvd. & 18 <sup>th</sup> St.			
24. Hoyt Ave. N. & 21 <sup>st</sup> St.	X		X
24. Hoyt Ave. N. & 21 St. 25. Hoyt Ave. S./Astoria Park S. &			
25. Hoyt Ave. S./Astoria Park S. $\approx$ 21 <sup>st</sup> St.	Х		Х
$26. 27^{\text{th}} \text{ Ave. } \& 9^{\text{th}} \text{ St.}$	X	X	Х
27. Vernon Blvd. & 31 <sup>st</sup> Ave.	X		X
28. Vernon Blvd. & Broadway/11 <sup>th</sup>		v	
St.	Х	Х	Х
29. 31 <sup>st</sup> Ave. & 21 <sup>st</sup> St.			

#### Table 13-1a: Summary of Weekday Impact Locations

Notes:

X – denotes potential for significant adverse impact. *This table has been updated for the FEIS.* 

#### Transit

#### Subway

The project site is served by the N. O. and F lines: the 30<sup>th</sup> Avenue Station (to the southeast of the project site) is served by the N and Q lines, and the 21<sup>st</sup> Street-Queensbridge Station (to the south of the project site) is served by the F line. Based on current station usage, the proximity to the project site, and the proposed shuttle service to the 30<sup>th</sup> Avenue Station, it was estimated that the majority (approximately 80 percent) of subway riders would utilize the 30<sup>th</sup> Avenue Station via a shuttle, while the remaining 20 percent would utilize the 21<sup>st</sup> Street-Queensbridge Station. Therefore, according to CEOR Technical Manual criteria, a detailed analysis of subway station elements was only warranted at the 30<sup>th</sup> Avenue Station. In addition, a subway line haul analysis was conducted for the three subway lines serving the project site. The results of the analysis of future conditions indicate that the Proposed Action would result in significant adverse impacts on the 30<sup>th</sup> Avenue Station's northwest street stair during the PM peak hour. Due to the high volumes of Manhattan-bound morning commuter traffic, significant adverse impacts to the 30<sup>th</sup> Avenue Station's southbound fare array are anticipated during the AM peak hour. Potential mitigation measures for these significant adverse subway station element impacts are discussed in Chapter 20, "Mitigation." While the Manhattan-bound Q line would operate over capacity in future With-Action conditions, as the Proposed Action would add less than five passengers per car (the CEQR impact criterion), no significant adverse subway line haul impact would result.

#### Bus

In addition to new bus riders resulting from the Proposed Action, the level of new bus demand on the analyzed local bus route Q103 would include project-generated F line subway riders that are expected to take the Q103 bus to and from the 21<sup>st</sup> Street-Queensbridge Station. The results of the bus transit impact analysis indicate that the Q103 route would experience significant adverse impacts in the southbound direction during both the weekday AM and PM peak hours, as well as in the northbound direction during the PM peak hour. Potential mitigation measures for these significant adverse bus impacts are discussed in Chapter 20, "Mitigation."

#### Pedestrians

The Proposed Action would not result in any significant adverse impacts to sidewalks, corner areas or crosswalks. A total of 11 existing sidewalks, three corners, and one crosswalk in the vicinity of the project site and close to the 30<sup>th</sup> Avenue subway station were selected for analysis in the three peak hours. Four additional future sidewalk elements on the project site were analyzed for the With-Action condition only. The results of the analysis of future conditions with the Proposed Action indicate that all analyzed sidewalks, corners, and crosswalks would operate at acceptable levels of service during the weekday AM, midday, and PM peak hours under With-Action conditions.

#### **Pedestrian and Vehicular Safety Evaluation**

As shown in Section J, "Pedestrian and Vehicular Safety Evaluation," none of the analyzed study area intersections exceeded one pedestrian and/or bicyclist injury crash in one or more years from 2010-2012 or reached the *CEQR Technical Manual* threshold for the total number of crashes per year. Therefore, based on the accident data presented below in Table 13-4<u>6</u>, a significant safety impact on pedestrian, bicyclist, and vehicular safety is not anticipated. In addition, no pedestrian and vehicular safety concerns are anticipated on future project site streets. However, the Applicant will work with NYCDOT to implement required school signage and other typical safety features applied in proximity to schools where necessary.

#### Parking

As discussed below in Section K, "Parking," the maximum parking demand, which is expected to occur from 8-9 PM, as well as the overnight demand, are expected to be accommodated by new parking spaces that would be created as part of the proposed project as well as on-street parking in the immediate vicinity. Therefore, no significant adverse parking impacts are expected.

#### Weekend Conditions Assessment

Between issuance of the Draft Environmental Impact Statement (DEIS) and this Final EIS (FEIS), a semiquantitative/qualitative assessment of a representative weekend peak period (Saturday 2-3 PM) was prepared. This assessment included estimates of action-generated Saturday peak hour trips and comparisons of weekday and Saturday background conditions, as well as detailed traffic LOS analyses, where warranted. Saturday peak hour traffic conditions were analyzed at thirteen of the 30 study area intersections, as requested by NYCDOT. The traffic impact analysis indicates that there would be a potential for significant adverse impacts at seven intersections during the Saturday midday peak hour. As discussed in detail in Section L, "Weekend Conditions Assessment," the analysis of future conditions without accounting for the Halletts Point development shows that, although the majority of significant adverse impacts were identified at the same locations for both the future conditions, generally fewer impacts would occur absent the Halletts Point development. The Saturday impact locations under both future scenarios are shown in Table 13-1b, below.

Intersection	With-Action Condition	Alternate With-Action Condition
2. 27 <sup>th</sup> Ave. & 4 <sup>th</sup> St.	Х	
3. 27 <sup>th</sup> Ave. & 8 <sup>th</sup> St.	Х	
4. 27 <sup>th</sup> Ave. & 12 <sup>th</sup> St.		Х
5. 27 <sup>th</sup> Ave. & 14 <sup>th</sup> St.		
6. 27 <sup>th</sup> Ave. & 18 <sup>th</sup> St.		
7. Astoria Blvd. & 21 <sup>st</sup> St.	Х	Х
14. Astoria Blvd. & 31 <sup>st</sup> St.		Х
15. Hoyt Ave. S./Astoria Blvd. & 33 <sup>rd</sup> St.	Х	Х
18. Astoria Blvd. N. & 32 <sup>nd</sup> St.	Х	
19. Astoria Blvd. & 8 <sup>th</sup> St.		
24. Hoyt Ave. N. & 21 <sup>st</sup> St.	Х	Х
25. Hoyt Ave. S./Astoria Park S. &		
21 <sup>st</sup> St.		
26. 27 <sup>th</sup> Ave. & 9 <sup>th</sup> St.	Х	Х

#### <u>Table 13-1b: Summary of Weekend Impact Locations—With-Action and Alternate</u> With-Action Conditions

Notes:

<u>X – denotes potential for significant adverse impact.</u>

<u>This table is new to the FEIS.</u>

Potential mitigation measures for these significant adverse traffic impacts are discussed in Chapter 20, "Mitigation."

## C. PRELIMINARY ANALYSIS METHODOLOGY

The *CEQR Technical Manual* describes a two-level screening procedure for the preparation of a "preliminary analysis" to determine if quantified analyses of transportation conditions are warranted. As discussed in the following sections, the preliminary analysis begins with a trip generation (Level 1) analysis to estimate the amount of person and vehicle trips expected to be generated by the proposed project. By *CEQR Technical Manual* guidelines, if the proposed project is expected to result in fewer than 50 peak-hour vehicle trips and fewer than 200 peak hour transit or pedestrian trips, further quantified analyses are not warranted. When these thresholds are exceeded, detailed trip assignments (Level 2) are to be performed to estimate the incremental trips that could be incurred at specific transportation elements and to identify potential locations for further analyses. If the trip assignments show that the proposed project would generate 50 or more peak hour vehicle trips at an intersection, 200 or more peak hour subway trips at a station, 50 or more peak hour bus trips in one direction along a bus route, or 200 or more peak hour pedestrian trips traversing a sidewalk, corner area, or crosswalk, further quantified operational analyses may be warranted to assess the potential for significant adverse impacts on traffic, transit, pedestrian, parking, and pedestrian and vehicular safety. The results of the two-level screening assessments are described in the following.

## D. LEVEL 1 SCREENING ASSESSMENT

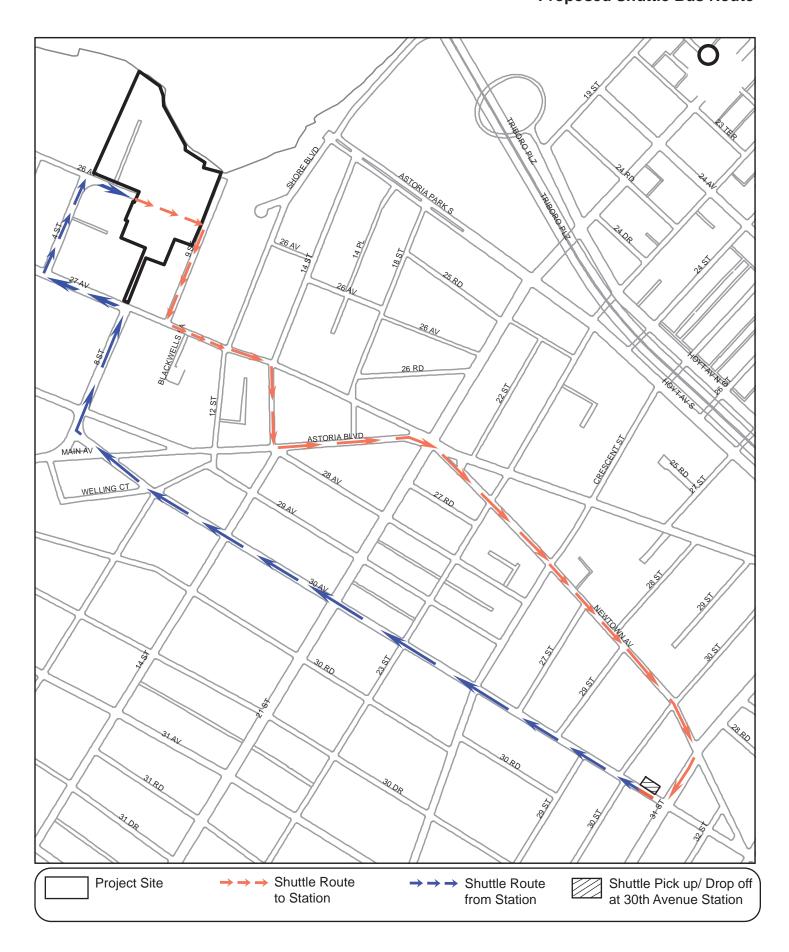
A Level 1 screening assessment was conducted to estimate the volume of person and vehicle trips by mode expected to be generated by the proposed project during the weekday AM, midday, and PM peak hours. These estimates were then compared to the *CEQR Technical Manual* analysis thresholds of 50 peak hour vehicle trips, 200 peak hour subway/rail or bus riders, and 200 peak hour pedestrian trips to determine if a Level 2 screening and/or quantified operational analyses were warranted.

The Level 1 screening assessment relies on the project's proposed uses. As discussed in Chapter 1, "Project Description", the proposed project would include residential, local retail, supermarket and school uses. The proposed project's program is shown in Table 13-2 below. As detailed in Chapter 1, "Project Description" and as also shown in Figures 1-1 and 1-2, the project site is spread over several upland and waterfront blocks with substantial street frontages. The Proposed Action would have four garages with a total of 900 parking spaces and access/egress points on 26<sup>th</sup> Avenue and 4<sup>th</sup> and 9<sup>th</sup> Streets. It should be noted that the proposed project would also provide a shuttle service for the proposed project's residents to the 30<sup>th</sup> Avenue subway station, located at 30<sup>th</sup> Avenue and 31<sup>st</sup> Street, southe<u>a</u>st of the project site. The anticipated shuttle route is shown in Figure 13-1. For transit analysis purposes, it is assumed that the existing Q18/Q102 bus stop would be lengthened west to accommodate the shuttle bus, potentially with a second berth for the shuttle bus. It is anticipated that 40-passenger buses would be used for the shuttle <u>service</u>, with each shuttle bus making up to four roundtrips per hour during the weekday AM and PM peak hour.

It also should be noted that while a <u>Food Retail Expansion to Support Health (FRESH)</u> supermarket certification will likely be pursued in the future, per the guidance of DCP, the transportation analyses will assume a RWCDS that includes a generic supermarket usage. In general, a RWCDS with a FRESH supermarket and corresponding residential floor area <u>bonus</u> is the appropriate analysis basis as most of the density-related analyses are more sensitive to the number of dwelling units and/or residential population. However, for conservative purposes the transportation analyses is based on a RWCDS with a generic supermarket and less residential floor area (1,668 DU), as this program is expected to generate substantially more vehicular traffic, as discussed below.



## Figure 13-1 Proposed Shuttle Bus Route



Programming
$1,689 \mathrm{DU}^1$
84,470 gsf
25,000 gsf
456 seats
900 spaces
1.92 acres

#### Table 13-2: Astoria Cove Program

Notes:

<sup>1</sup>Includes an additional 21 dwelling units as a result of the FAR credit of 20,000 sf potentially to be awarded by a FRESH supermarket usage; 1,668 dwelling units with a generic supermarket.

Tables 13-3 and 13-4 show the transportation planning factors used for the travel demand forecast of the proposed project in the weekday AM, midday, and PM peak hours for the program with <u>a\_FRESH</u> supermarket and with a generic supermarket usage, respectively. The <u>tables</u> include trip generation rates, temporal and directional distributions, mode choice factors, and vehicle occupancy rates for each of the land uses. Given the size and anticipated programming of the proposed project's open space, it is anticipated that the majority of associated trips would be generated by other project site uses or linked to other project-generated trips. As such, the discussion below focuses on the residential, commercial, and school land uses.

#### **Transportation Planning Factors**

#### Local Retail

As shown above in Table 13-2, the Proposed Action would result in the development of 84,470 sf of local retail. The trip generation rates and temporal distributions for the local retail component were based on the *CEQR Technical Manual*. The modal splits, in/out splits, and vehicle occupancy rates were based on the *Dutch Kills Rezoning and Related Actions FEIS* (2008).

#### Residential

As also shown in Table 13-2, in the RWCDS with FRESH supermarket and generic supermarket usage scenarios, the proposed project would include 1,689 and 1,668 residential units, respectively, as the floor area ratio (FAR) available for residential development would be increased with FRESH supermarket usage. It should be noted that credit was assumed for the 166 residential units that would be developed on the project site in the future without the Proposed Action, resulting in a net increment of 1,523 and 1,502 residential units in the program with FRESH supermarket and generic supermarket usage scenarios, respectively (see Tables 13-3 and 13-4).

The trip generation rates and temporal distributions for the residential component were based on the *CEQR Technical Manual*. The modal splits and vehicle occupancy rates were based on 2007-2011 ACS Journey to Work data for census tracts 81, 83, 91, 97, 101, 103, and 105 in Queens, which were deemed appropriate by DCP for representing travel characteristics of the proposed project's future residents. As shown in Tables 13-3 and 13-4, the predominant mode choices for future residents are expected to be subway (55.4 percent) and private auto (32.4 percent). The directional in/out splits were based on the *ITE Trip Generation Handbook*,  $8^{th}$  Edition, Land Use Code (220) Apartments.

Land Use:	Local	Retail	Resid	ential	FRESH Su	permarket	PS S	School	PS	Staff	Existing	Industrial
Size/Units:	84,470	gsf	1,523	DU*	25,000	gsf	456	seats	35	staff	-194,700	gsf
Trip Generation:	(1	l)	(1	)	(:	5)	(	(9)	(	9)	(	(7)
Weekday	20	)5	8.0	75	20	)5		2		2	Ν	JA
-	per 1,0	000 gsf	per	DU	per 10	00 gsf	per s	tudent	per	staff		
Temporal Distribution:	(1	I)	(1	)	(:	5)	(	(9)	(	9)	(	(7)
AM	3.0	)%	10.0	)%	3.0	)%	5	0%	50	)%	Ν	ΙA
MD	19.	0%	5.0	%	12.	0%	(	)%	0	%	Ν	JA
PM	10.	0%	11.0	)%	10.	0%	5	5%	50	)%	Ν	ΙA
		2)	(3			5)	`	10)		8)		(7)
Modal Splits:	AM/M		AM/M		AM/M			Internal		ID/PM		AD/PM
Auto/Auto-dropoff	2.0		32.4		4.0		5.0%	0.0%		.0%		ΝA
Taxi	3.0		0.5		3.0		0.0%	0.0%		0%		ЛА
Subway/Shuttle	6.0		55.4		5.0		0.0%	0.0%		.0%	N	ΙA
Bus	6.0	)%	3.2	%	5.0	)%	0.0%	0.0%	11	.0%	Ν	ΙA
Schoolbus							5.0%	0.0%			Ν	λA
Walk/Ferry/Other	83.	0%	8.5	%	83.	0%	5.0%	85.0%	13	.0%	N	JA
	100	.0%	100.	0%	100	.0%	15.0%	85.0%	100	0.0%	Ν	λA
		2)	(4			5)		(9)		9)		(7)
In/Out Splits:	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
AM	50%	50%	20.0%		45%	55%	100%	0%	100%	0%	NA	NA
MD	50%	50%	50.0%		46%	54%	0%	0%	0%	100%	NA	NA
PM	50%	50%	65.0%	35.0%	47%	53%	0%	100%	0%	100%	NA	NA
Vehicle Occupancy:	(2	2)	(3			5)		(9)	(	8)		(7)
		kday	Weel		Wee			ekday		kday		ekday
Auto	2.	00	1.1	1	1.0		1	.3	1.	20	Ν	JА
Taxi	2.	00	1.	4	1.4	40	1	1.3	1.	20	Ν	ΝA
Truck Trip Generation:	(1	l)	(1	)	(:	5)	(	(6)			(	(7)
	0.	35	0.0	)6	0.1	35	6	.25			Ν	JA
	per 1,	000 sf	per	DU	per 1,	000 sf	stude	nts/bus				
		l)	(1			5)						(7)
AM	8.0		12.0		10.							JA
MD	11.		9.0		8.0							JA
PM	2.0	)%	2.0	%	5.0	)%					Ν	ΝA
	In	Out	In	Out	In	Out					In	Out
AM	50.0%	50.0%	50.0%		50.0%	50.0%					NA	NA
MD	50.0%	50.0%	50.0%		50.0%	50.0%					NA	NA
PM	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%					NA	NA

#### Table 13-3: <u>Weekday</u> Transportation Planning Assumptions (FRESH Supermarket)

Notes:

(1) CEQR Technical Manual

(2) Dutch Kills Rezoning and Related Actions FEIS (2008)

(3) Modal split and vehicle occupancy rates based on 2007-2011 ACS Journey to Work data (census tracts 81,83,91,97,101,103,105)

(4) Based on ITE Trip Generation Handbook, 8th Edition, Land Use Code (220) Apartment.

(5) The Food Retail Expansion to Support Health (FRESH) Food Store Program EAS (2009)

(6) Based on data from survey conducted by PHA (October 2012) on PS 35, Hollis, Queens.

(7) Vehicular travel demand was based on counts in 2013. Credit for transit and pedestrian trips are not being taken for conservative purposes.

(8) Modal split and vehicle occupancy data based on 2000 Census Reverse Journey to Work data (census tracts 87, 91) in Queens.

(9) Brownsville Ascend Charter School Assessment (2011).

(10) Halletts Point FEIS (2013).

(11) CEQR local retail delivery truck trip generation rate.

\* 166 residential units in upland area in No-Action condition (1,689 DUs in With-Action condition) for net increment of 1,523.

Land Use:	Local R	<u>etail</u>	Resid	<u>lential</u>	Su	permark	et	PS S	<u>chool</u>	<u>PS S</u>	<u>Staff</u>	Existing Ir	ndustrial
Size/Units:	84,470 g	gsf	1,502	DU*	25,000	gsf		456	seats	35	staff	-194,700	gsf
Trip Generation:	(1)		(	1)		(1)		C	9)	(9	<del>)</del> )	(7)	)
Weekday	205			075		175			2		2	NA	
	per 1,00	00 sf	per	DU	p	er 1000 gs	f	per st	udent	per	staff		
Temporal Distribution:	(1)		(	1)		(5)		(	9)	(9	<del>)</del> )	(7)	)
AM	3.0%	, D	10.	.0%		5.0%		50	1%	50	1%	NA	A
MD	19.09	%	5.0	0%		6.0%		0	%	09	%	NA	A
PM	10.09	%	11.	.0%		10.0%		5	%	50	1%	NA	A
	(2)		(	3)		(5)		(1	0)	(8	3)	(7)	)
Modal Splits:	AM/ME	D/PM	AM/N	1D/PM	AM	MD	PM	Outsider	Internal	AM/N	ID/PM	AM/M	D/PM
Auto/Auto-dropoff	2.0%	ò	32.	.4%	61.0%	68.0%	67.0%	5.0%	0	57.	0%	NA	A
Taxi	3.0%	, D	0.5	5%	0.0%	0.0%	0.0%	0.0%	0	1.0	)%	NA	A
Subway/Shuttle	6.0%	ó	55.	.4%	1.0%	0.0%	0.0%	0.0%	0	18.	0%	NA	A
Bus	6.0%	ó	3.2	2%	5.0%	5.0%	3.0%	0.0%	0	11.	0%	NA	A
Schoolbus								5.0%	0			NA	A
Walk/Ferry/Other	83.0%	6	8.	5%	33.0%	27.0%	30.0%	5.0%	85%	13.	0%	NA	4
	100.0	%	100	0.0%	100.0%	100.0%	100.0%	15.0%	85.0%	100	.0%	NA	A
	(2)		(•	4)		(5)		C	9)	(9	<del>)</del> )	(7)	)
In/Out Splits:	In	Out	In	Out	In	Out		In	Out	In	Out	In	Out
AM	50%	50%	20.0%	80.0%	57%	43%		100%	0%	100%	0%	NA	NA
MD	50%	50%	50.0%	50.0%	50%	50%		0%	0%	0%	100%	NA	NA
PM	50%	50%	65.0%	35.0%	52%	48%		0%	100%	0%	100%	NA	NA
Vehicle Occupancy:	(2)		(	3)		(5)		(	9)	(8	8)	(7)	)
	Weeka	lay	Wee	kday	AM	MD	PM	Wee	kday	Wee	kday	Week	day
Auto	2.00	)	1.	11	1.12	1.32	1.34	1	.3	1.	20	NA	A
Taxi	2.00	)	1	.4				1	.3	1.1	20	NA	A
Truck Trip Generation:	(1)		(	1)		(11)		(	6)			(7)	)
	0.35	5	0.	06		0.35		6.	25			NA	A
	per 1,00	00 sf	per	DU	р	er 1,000 s	f	studer	ts/bus				
	(1)			1)		(1)						(7)	
AM	8.0%	, D	12.	.0%		8.0%						NA	A
MD	11.09	%	9.0	0%		11.0%						NA	A
PM	2.0%	ò	2.0	0%		2.0%						NA	A
	In	Out	In	Out	In	Out						In	Out
AM		50.0%	50.0%	50.0%	50.0%	50.0%						NA	NA
MD	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%						NA	NA
PM	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%						NA	NA

Table 13-4: Weekday Trans	portation Planning	Assumptions (	Generic Supermarket)

Notes:

(1) CEQR Technical Manual

(2) Dutch Kills Rezoning and Related Actions FEIS (2008)

(3) Modal split and vehicle occupancy rates based on 2007-2011 ACS Journey to Work data (census tracts 81,83,91,97,101,103,105)

(4) Based on *ITE Trip Generation Handbook*, 8th Edition, Land Use Code (220) Apartment.

(5) Based on 1525 Albany Avenue Pathmark Supermarket Survey

(6) Based on data from survey conducted by PHA (October 2012) on PS 35, Hollis, Queens.

(7) Vehicular travel demand was based on counts in 2013. Credit for transit and pedestrian trips are not being taken for conservative purposes.

(8) Modal split and vehicle occupancy data based on 2000 Census Reverse Journey to Work data (census tracts 87, 91) in Queens.

(9) Brownsville Ascend Charter School Assessment (2011).

(10) Halletts Point FEIS (2013).

(11) CEQR local retail delivery truck trip generation rate.

\* 166 residential units in upland area in No-Action condition (1,668 DUs in With-Action condition) for net increment of 1,502.

#### **FRESH** Supermarket

As discussed above, the proposed project would include a 25,000 sf FRESH supermarket. The trip generation rates, modal splits, directional in/out splits, and vehicle occupancies are all based on the *Food Retail Expansion to Support Health (FRESH) Food Store Program EAS* (2009). As noted above, while the RWCDS with a FRESH supermarket forms the appropriate basis for most of the density-related analyses presented in this EIS, the RWCDS with a generic supermarket was conservatively used for the transportation analysis as it is expected to generate more vehicular traffic based its transportation planning factors described in the following.

#### Generic Supermarket

The trip generation rates and temporal distribution for truck trips for the 25,000 sf generic supermarket components were based on the *CEQR Technical Manual*, while the temporal distribution for person trips, modal splits, and directional in/out splits were based on the *1525 Albany Avenue Supermarket Survey* (2009). As shown in Table 13-4, private auto is expected to be the predominant mode choice for the generic supermarket use, with auto shares of 61 percent, 68 percent, and 67 percent in the weekday AM, midday, and PM peak periods, respectively, while for the FRESH supermarket the auto share is assumed to only be four percent (see Table 13-3). Therefore, as noted above, the RWCDS with the generic supermarket with its higher auto share and consequently greater vehicular traffic was conservatively used for the detailed transportation analyses presented in this chapter.

#### **Public School Students**

As shown earlier in Table 13-2, the Proposed Action would also result in a public elementary school with 456 seats. The trip generation rates, temporal distributions, directional in/out splits, and vehicle occupancy rates for the public school student component were based on the *Brownsville Ascend Charter School Assessment* (2011). The modal splits were based on the *Halletts Point FEIS* (2013). It should be noted that 85 percent of students are expected to come from the new residential developments included in the proposed project, who would all walk to/from school, while 15 percent of students from outside of the project site would visit the new school by auto drop-off, school bus, and on foot. The number of students per school bus was based on an October 2012 survey conducted by PHA at PS 35 in Hollis, Queens. A 90 percent attendance rate was assumed for all students.

#### Public School Staff

The proposed school is also expected to generate new trips by approximately 35 staff members. The trip generation rates, temporal distributions, and directional in/out splits for school staff were also based on the *Brownsville Ascend Charter School Assessment* (2011), while the modal splits and vehicle occupancy rates were based on 2000 Census Reverse Journey to Work data for census tracts 87 and 91 in Queens.

#### **Existing Industrial Land Uses**

As shown in Tables 13-3 and 13-4, credit was taken for 194,700 sf of existing industrial land uses, which are expected to continue to occupy a portion of the project site in the future without the Proposed Action. In coordination with NYCDOT, vehicular travel demand was forecasted based on counts conducted by PHA in November 2013.

#### **Travel Demand Forecast**

Table 13-5 summarizes the results (presented in detail in Tables 13-6 and 13-7) of the travel demand forecast for the vehicular traffic resulting from the Proposed Action based on the factors discussed above for a RWCDS with a FRESH supermarket and a RWCDS with a generic supermarket, respectively.

Supermar	ket						
		SH Supe (Variant	rmarket 1)		ric Super (Variant		Differences
Peak Hour	In	Out	Total	In	Out	Total	Difference (Variant 2 – Variant 1)
AM	124	334	458	169	365	534	76
MD	150	146	296	185	180	365	69
PM	304	197	501	373	260	633	132

Table 13-5: WeekdayTravel Demand Forecast Summary Comparison—RWCDSwithFRESHSupermarketvs.RWCDSSupermarket

Note:

<sup>1</sup>Used for the detailed transportation analyses presented in this chapter

As discussed above, the transportation analysis is based on the RWCDS with a generic supermarket due to its higher project-generated vehicular traffic. As shown in Table 13-5, the RWCDS scenario with a generic supermarket would result in 76, 69, and 132, more incremental vehicle trips than the RWCDS with the FRESH supermarket during the weekday AM, midday, and PM peak periods, respectively. Therefore, the following detailed transportation analyses are based on a RWCDS with a generic supermarket.

As shown in Table 13-7 the Proposed Action would result in an increase of 2,216, 3,272, and 3,040 person trips in the weekday AM, midday, and PM peak hours, respectively. Table 13-7 also shows that, compared to the No-Action condition, there would be an increase of approximately 534, 365, and 633 vehicle trips during the weekday AM, midday, and PM peak hours respectively. Vehicles include automobiles, school buses, shuttles, taxis, and trucks. Compared to the No-Action condition, the Proposed Action would generate approximately 705, 484, and 823 additional subway trips and 77, 180, and 135 new bus trips during the weekday AM, midday, and PM peak hours, respectively. Net pedestrian trips (including walk/other, subway and bus trips) would total 1,635, 2,814, and 2,292 during these time periods, respectively. Of these total pedestrian trips, 853, 2,150, and 1,334 would be walk-only trips during the weekday AM, midday, and PM peak hours, respectively, compared to No-Action conditions.

As the numbers of peak hour trips generated by the Proposed Action would exceed the *CEQR Technical Manual* analysis thresholds for vehicular traffic, transit trips, and pedestrian trips (including walk-only, subway and bus trips) during one or more of the peak hours, a Level 2 screening assessment was undertaken to identify specific locations where additional detailed analyses may be warranted.

## E. LEVEL 2 SCREENING ASSESSMENT

A Level 2 screening assessment involves the assignment and distribution of project-generated trips to the study area street network, transit facilities, and pedestrian elements and the identification of specific locations where the incremental increase in demand may potentially exceed the *CEQR Technical Manual* analysis thresholds and therefore require a quantitative analysis. These assignments are discussed below for each mode.

Land Use	:	Local	Retail	Resid	ential	FRESHSup	ermarket	PS S	chool			PS	Staff	Existing I	ndustrial		
Size/Unit	s:	84,470	gsf	1,523	DU	25,000	gsf	456	seats			35	staff	-194,700	gsf	То	otal
Peak Hou	ır Trips:																
	AM	39	90	1,2	230	115	5	4	12			3	35	NA	1	2,	182
	MD	2,4	468	6	15	463	3		0				0	NA	1	3,	546
	PM	1,3	300	1,3	354	385	5		42			3	35	NA	1		116
Person T	rips:							Ofi	-site	On-	site						
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
AM	Auto	4	4	80	319	2	2	21	0	0	0	20	0	NA	NA	127	325
	Taxi	6	6	1	5	2	2	0	0	0	0	0	0	NA	NA	9	13
	Subway	12	12	136	545	2	3	0	0	0	0	6	0	NA	NA	156	560
	Bus	12	12	8	31	2	4	0	0	0	0	4	0	NA	NA	26	47
	Schoolbus							20	0	0	0			NA	NA	20	0
	Walk/Other	161	161	21	84	43	53	21	0	350	0	5	0	NA	NA	601	298
	Total	195	195	246	984	51	64	62	0	350	0	35	0	NA	NA	939	1,24
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
MD	Auto	25	25	100	100	8	10	0	0	0	0	0	0	NA	NA	133	135
	Taxi	37	37	2	2	7	7	0	0	0	0	0	0	NA	NA	46	46
	Subway	74	74	170	170	11	13	0	0	0	0	0	0	NA	NA	255	257
	Bus	74	74	10	10	11	13	0	0	0	0	0	0	NA	NA	95	97
	Schoolbus							0	0	0	0			NA	NA	0	0
	Walk/Other	1,024	1,024	26	25	176	207	0	0	0	0	0	0	NA	NA	1,226	1,25
	Total	1,234	1,234	308	307	213	250	0	0	0	0	0	0	NA	NA	1,755	1,79
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Ou
PM	Auto	13	13	285	154	7	8	0	3	0	0	0	20	NA	NA	305	198
	Taxi	20	20	4	2	5	6	0	0	0	0	0	0	NA	NA	29	28
	Subway	39	39	488	263	9	11	0	0	0	0	0	6	NA	NA	536	319
	Bus	39	39	28	15	9	11	0	0	0	0	0	4	NA	NA	76	69
	Schoolbus							0	0	0	0			NA	NA	0	0
	Walk/Other	539	539	75	40	150	169	0	3	0	36	0	5	NA	NA	764	792
	Total	650	650	880	474	180	205	0	6	0	36	0	35	NA	NA	1,710	1,400
Vehicle 1	rips :																
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
AM	Auto (Total)	2	2	72	287	2	2	16	16	0	0	17	0	-18	-8	91	299
	Taxi	3	3	1	4	1	2	0	0	0	0	0	0	0	0	5	9
	Taxi Balanced	6	6	5	5	3	3	0	0	0	0	0	0	0	0	14	14
	Shuttle/Schoolbus			11	11			3	3	0	0			0	0	14	14
	Truck	1	1	5	5	1	1	0	0	0	0	0	0	-2	0	5	7
	Total	9	9	93	308	6	6	19	19	0	0	17	0	-20	-8	124	334
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Ou
MD	Auto (Total)	13	13	90	90	5	6	0	0	0	0	0	0	-11	-15	97	94
	Taxi	19	19	1	1	4	5	0	0	0	0	0	0	0	0	24	25
	Taxi Balanced	38	38	2	2	9	9	0	0	0	0	0	0	0	0	49	49
	Shuttle/Schoolbus			0	0			0	0					0	-1	0	-1
	Truck	1	1	4	4	1	1	0	0	0	0	0	0	-2	-2	4	4
	Total	52	52	96	96	15	16	0	0	0	0	0	0	-13	-18	150	146
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Ou
PM	Auto (Total)	7	7	257	139	4	5	2	2	0	0	0	17	-5	-16	265	154
	Taxi	10	10	3	1	4	4	0	0	0	0	0	0	0	0	17	15
	Taxi Balanced	20	20	4	4	8	8	0	0	0	0	0	0	0	0	32	32
	Shuttle/Schoolbus			10	10			0	0					-3	0	7	10
	Truck	0	0	1	1	0	0	0	0	0	0	0	0	-1	0	0	1
	Total	27	27	272	154	12	13	2	2	0	0	0	17	-9	-16	304	19
			Total									Q103	Bus Der	nand*			
	Total Vehicle	In	Out	Total								In	Out	Total			
	AM	124	334	458								40	128	168			
	MD	150	146	296								83	83	166			
	PM	304	197	501								132	87	219			

#### Table 13-6: <u>Weekday</u> Travel Demand Forecast (FRESH Supermarket)

Notes: 25 percent link trips applied to retail and supermarket uses 80 percent of resident subway users will be shuttled to subway station at 30<sup>th</sup> Avenue and 31<sup>st</sup> Street 10 percent absentee rate applied for students of the public school. \* 20 percent of subway demand added to Q103 bus trips.

Land Use	:	Local	Retail	Resid	ential	Superi	narket	PS S	chool			PS S	Staff	Existing Is	ndustrial		
Size/Uni	ts:	84,470	gsf	1,502	DU	25,000	gsf	456	seats			35	staff	-194,700	gsf	То	otal
Pool Ho	ur Trips:																
reak no		2	00	1.2	14	14			12			-	-	N		2	216
	AM		90	1,2			55						5	NA			216
	MD		468		)6	19			0			(		NA			272
	PM	1,3	300	1,3	34	32	29		42			3	5	NA	A	3,0	040
Person T	rips:							Ofi	f-site	On-	site						
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
AM	Auto	4	4	79	315	57	43	21	0	0	0	20	0	NA	NA	181	362
	Taxi	6	6	1	5	0	0	0	0	0	0	0	0	NA	NA	7	11
	Subway	12	12	135	538	1	1	0	0	0	0	6	0	NA	NA	154	551
	Bus	12	12	8	31	5	5	0	0	0	0	4	0	NA	NA	29	48
	Schoolbus	12	12	0	51	2	5	20	0	0	0	·	0	NA	NA	20	0
	Walk/Other	161	161	21	81	30	23	20	0	350	0	5	0	NA	NA	588	265
	Total	195	195	244	970	93	72	62	0	350	0	35	0	NA	NA	979	1,23
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
MD	Auto	25	25	98	98	67	67	0	0	0	0	0	0	NA	NA	190	190
	Taxi	37	37	2	2	0	0	0	0	0	0	0	0	NA	NA	39	39
	Subway	74	74	168	168	0	0	0	0	0	0	0	0	NA	NA	242	242
	Bus	74	74	10	10	6	6	0	0	0	0	0	0	NA	NA	90	90
	Schoolbus			-	-	-		0	0	0	0			NA	NA	0	0
	Walk/Other	1,024	1,024	25	25	26	26	0	0	0	0	0	0	NA	NA	1,075	1,07
	Total	1,234	1,234	303	303	99	99	0	0	0	0	0	0	NA	NA	1,636	1,63
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
PM	Auto	13	13	281	151	115	106	0	3	0	0	0	20	NA	NA	409	293
	Taxi	20	20	4	2	0	0	0	0	0	0	0	0	NA	NA	24	22
	Subway	39	39	480	259	0	0	0	0	0	0	0	6	NA	NA	519	304
	Bus	39	39	28	15	5	5	0	0	0	0	0	4	NA	NA	72	63
	Schoolbus							0	0	0	0			NA	NA	0	0
	Walk/Other	539	539	74	40	50	48	0	3	0	36	0	5	NA	NA	663	671
	Total	650	650	867	467	170	159	0	6	0	36	0	35	NA	NA	1,687	1,353
Vehicle	Frine +																
venicie	imps :	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
AM	Auto (Total)	2	2	71	284	51	39	16	16	0	0	17	0	-18	-8	139	333
	Taxi	3	3	1	4	0	0	0	0	0	0	0	0	0	0	4	7
	Taxi Balanced	6	6	5	5	0	0	0	0	0	0	0	0	0	0	11	11
	Shuttle/Schoolbus			11	11			3	3	0	0			0	0	14	14
	Truck	1	1	5	5	1	1	0	0	0	0	0	0	-2	0	5	7
	Total	9	9	92	305	52	40	19	19	0	0	17	0	-20	-8	169	365
		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
MD	Auto (Total)	13	13	88	88	51	51	0	0	0	0	0	0	-11	-15	141	137
	Taxi	19	19	1	1	0	0	0	0	0	0	0	0	0	0	20	20
	Taxi Balanced	38	38	2	2	0	0	0	0	0	0	0	0	0	0	40	40
	Shuttle/Schoolbus			0	0			0	0					0	-1	0	-1
	Truck	1	1	4	4	1	1	0	0	0	0	0	0	-2	-2	4	4
	Total	52	52	94	94	52	52	0	0	0	0	0	0	-13	-18	185	180
		7	0		0.1		0		0.1		0.1		0.1	·	0		~
D) /		In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out	In	Out
PM	Auto (Total)	7	7	253	136	85	79	2	2	0	0	0	17	-5	-16	342	225
	Taxi	10	10	3	1	0	0	0	0	0	0	0	0	0	0	13	11
	Taxi Balanced	20	20	4	4	0	0	0	0	0	0	0	0	0	0	24	24
	Shuttle/Schoolbus			10	10			0	0					-3	0	7	10
	Truck	0	0	1	1	0	0	0	0	0	0	0	0	-1	0	0	1
	Total	27	27	268	151	85	79	2	2	0	0	0	17	-9	-16	373	260
												-		~ ~			
	Total Vehicle	In	Total Out	Total								In	0103 Bus Out	Demand* Total	-		
	AM	169	365	534								40	127	167			
	MD	185	180	365								78	78	156			
	PM	373	260	633								127	81	208			

#### Table 13-7: Weekday Travel Demand Forecast (Generic Supermarket)

#### Notes:

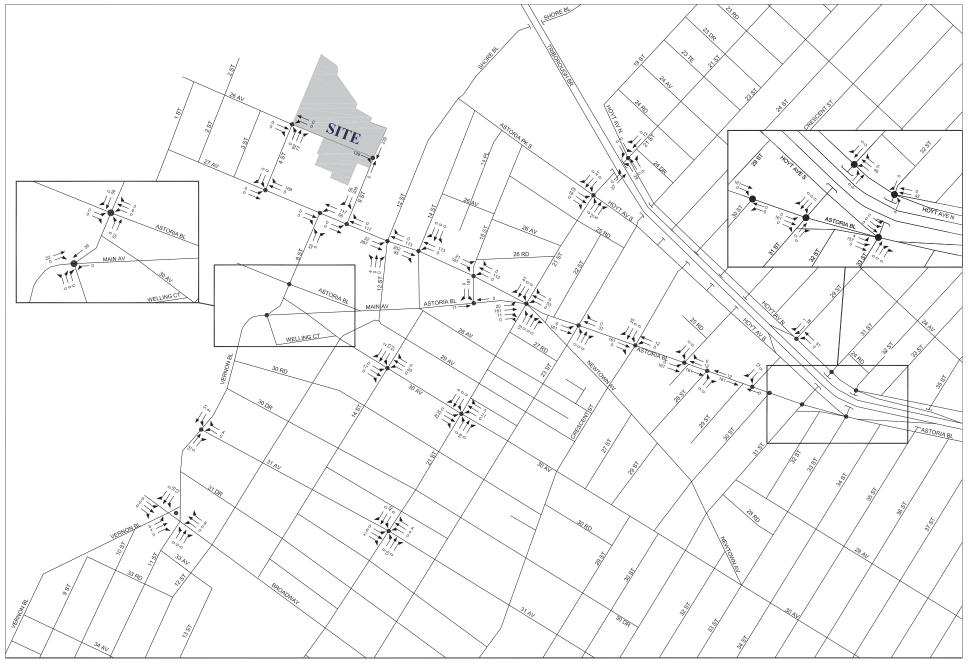
25 percent link trips applied to retail and supermarket uses
80 percent of resident subway users will be shuttled to subway station at 30<sup>th</sup> Avenue and 31<sup>st</sup> Street
10 percent absentee rate applied for students of the public school.
\* 20 percent of subway demand added to Q103 bus trips.

#### Traffic

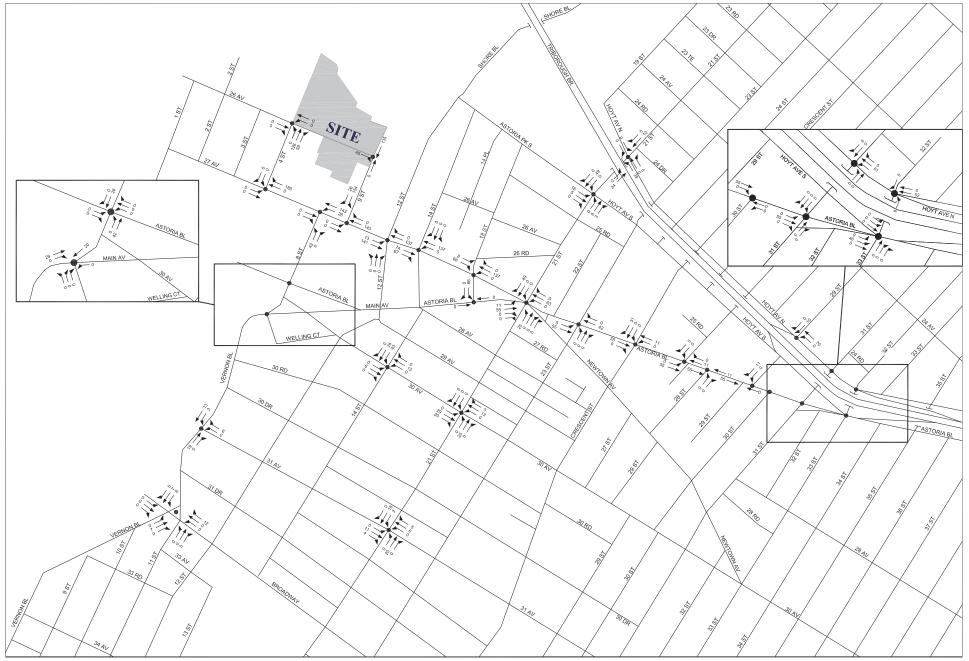
Figures 13-2, 13-3, and 13-4 show the assignment of vehicle trips (including auto, taxi, school bus, shuttle, and truck trips) generated by the proposed project to and from the project site during the weekday AM, midday, and PM peak hours, respectively. Based on the project-generated traffic shown in Figures 13-2 through 13-4 and in coordination with DCP and NYCDOT, 30 intersections within the study area were selected for detailed analysis to assess for potential significant adverse impacts as a result of the proposed project. These intersections are generally located within the vicinity of the project site and along the primary routes to and from the project site.

The 30 intersections selected for detailed analysis are listed below and their locations are also depicted in Figure 13-5. Of these intersections, 18 are currently signalized and 11 are unsignalized; one additional intersection (26<sup>th</sup> Avenue and 9<sup>th</sup> Street) does not exist under existing conditions and would be developed under future No-Action and With-Action conditions.

- 1.  $26^{\text{th}}$  Avenue &  $4^{\text{th}}$  Street (unsignalized)
- A. 26<sup>th</sup> Avenue & 9<sup>th</sup> Street (unsignalized; to be opened under future No-Action and future With-Action conditions)
- 2. 27<sup>th</sup> Avenue & 4<sup>th</sup> Street (unsignalized)
- 3.  $27^{\text{th}}$  Avenue &  $8^{\text{th}}$  Street (signalized)
- 4. 27<sup>th</sup> Avenue & 12<sup>th</sup> Street (unsignalized)
- 5. 27<sup>th</sup> Avenue & 14<sup>th</sup> Street (unsignalized)
- 6. 27<sup>th</sup> Avenue & 18<sup>th</sup> Street (unsignalized)
- 7. Astoria Boulevard & 21<sup>st</sup> Street (signalized)
- 8. Astoria Boulevard & 23<sup>rd</sup> Street (signalized)
- 9. Astoria Boulevard & Crescent Street (signalized)
- 10. Astoria Boulevard & 27<sup>th</sup> Street (signalized)
- 11. Astoria Boulevard & 28<sup>th</sup> Street (unsignalized)
- 12. Astoria Boulevard & 29<sup>th</sup> Street (signalized)
- 13. Astoria Boulevard & 30<sup>th</sup> Street (unsignalized)
- 14. Astoria Boulevard & 31<sup>st</sup> Street (signalized)
- 15. Hoyt Avenue South/Astoria Boulevard & 33<sup>rd</sup> Street (signalized)
- 16. Hoyt Avenue North & 29<sup>th</sup> Street (signalized)
- 17. Hoyt Avenue North & 31<sup>st</sup> Street (signalized)
- 18. Astoria Boulevard North & 32<sup>nd</sup> Street (signalized)
- 19. Astoria Boulevard & 8<sup>th</sup> Street (signalized)
- 20. 30<sup>th</sup> Avenue & 14<sup>th</sup> Street (unsignalized)
- 21.  $30^{\text{th}}$  Avenue &  $21^{\text{st}}$  Street (signalized)
- 22. Vernon Boulevard & Welling Court/8<sup>th</sup> Street (signalized)
- 23. Astoria Boulevard & 18<sup>th</sup> Street (unsignalized)
- 24. Hoyt Avenue North & 21<sup>st</sup> Street (signalized)
- 25. Hoyt Avenue South/Astoria Park South & 21<sup>st</sup> Street (signalized)
- 26.  $27^{th}$  Avenue &  $9^{th}$  Street (unsignalized)
- 27. Vernon Boulevard & 31<sup>st</sup> Avenue (unsignalized)
- 28. Vernon Boulevard & Broadway & 11<sup>th</sup> Street (signalized)
- 29.  $31^{st}$  Avenue &  $21^{st}$  Street (signalized)

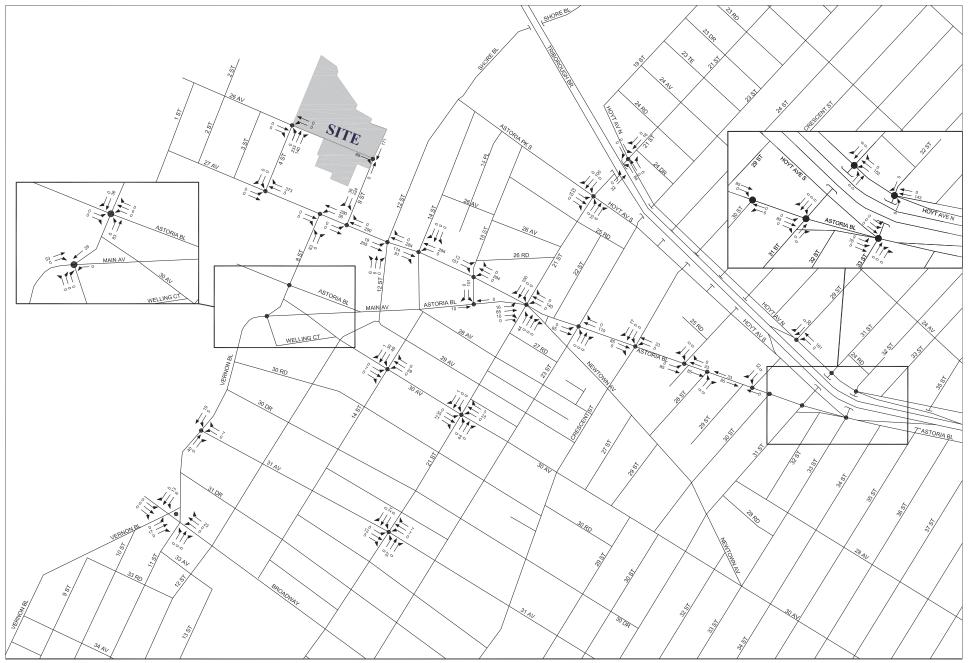


## Astoria Cove



## Astoria Cove

Figure 13-3



## Astoria Cove

Figure 13-4



• Weekday AM, Midday, and PM Analysis Locations

#### Transit

#### Subway

As shown earlier in Table 13-7, new peak hour subway trips would be 705, 484, and 823 in the weekday AM, midday and PM peak hours, respectively. According to the general thresholds used by the Metropolitan Transportation Authority—New York City Transit (NYCT) and specified in the *CEQR Technical Manual*, a Level 2 screening assessment is required if a Proposed Action is projected to result in 200 or more peak hour subway trips.

Project generated peak hour subway trips were assigned to the 30<sup>th</sup> Avenue (N and Q lines) Station and 21<sup>st</sup> Street-Queensbridge (F line) Station (see Figure 13-6), with the majority of trips allotted to the former. NYCT ridership data shows that the 30<sup>th</sup> Avenue Station serves nearly twice as many weekday riders as the 21<sup>st</sup> Street-Queensbridge Station. Considering current station usage, the proximity of stations to the project site, and the shuttle service to the 30<sup>th</sup> Avenue Station, it was estimated that 80 percent of subway riders would utilize the 30<sup>th</sup> Avenue Station via shuttle, while the remaining 20 percent would utilize the 21<sup>st</sup> Street-Queensbridge Station. Therefore, approximately 564, 387, and 658, new subway riders would use the 30<sup>th</sup> Avenue station during the weekday AM, midday, and PM peak hours, respectively, while ridership would increase by 141, 96, and 165 subway trips at the 21<sup>st</sup> Street-Queensbridge Station during these peak hours, respectively.

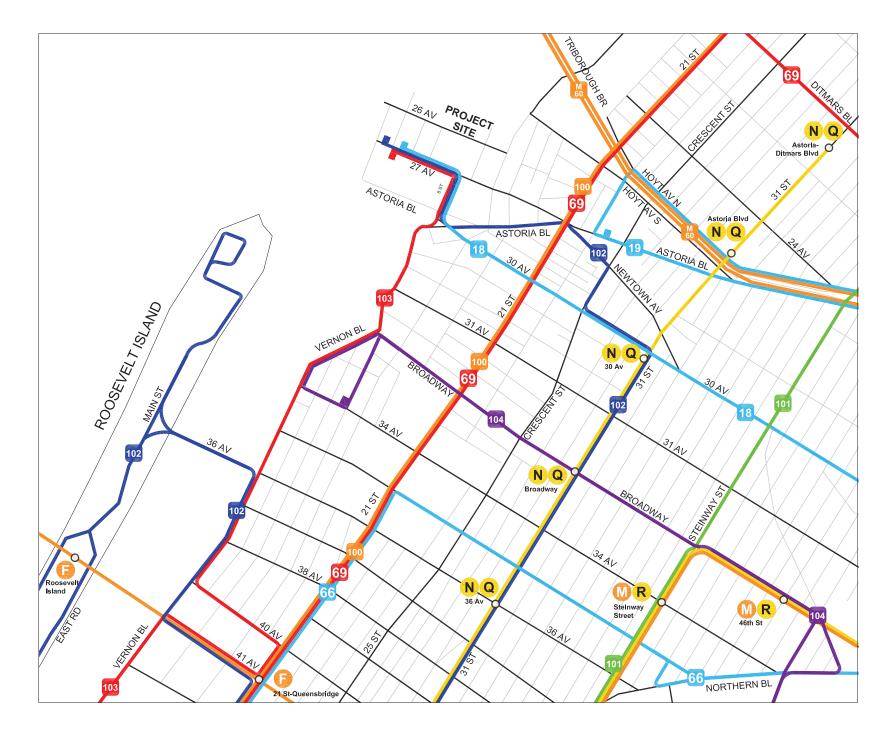
Based on a detailed assignment of these project-generated subway trips to available area subway lines and specific station entrance elements, it was determined that the northwest station-to-street staircase, the platform stairs, and the fare array elements within the control area at the 30<sup>th</sup> Avenue (N and Q lines) Station would require detailed analyses as the increment in subway riders would exceed the 200 trips per hour per subway station *CEQR Technical Manual* threshold.

#### Line Haul Analysis Screening Assessment

In addition to the detailed analysis of station elements at the 30<sup>th</sup> Avenue N and Q subway station, an analysis of line haul conditions on each of the subway routes serving the project site (N, Q, and F) was also conducted.

#### Bus

According to general thresholds used by NYCT and specified in the *CEQR Technical Manual*, a detailed bus line haul analysis is generally not required if the project-generated increase in passengers assigned to a single bus line (in one direction) is fewer than 50 passengers. As shown in Figure 13-6, the local bus routes servicing the area, with stops near the project site, include the Q18, Q102, and Q103. As the project site is located some distances from the nearest subway stations, project-generated subway trips are expected to use bus-to-subway connections. As a shuttle bus service to and from the 30<sup>th</sup> Avenue (N and Q lines) Station would be provided <u>during the weekday AM and PM peak hours</u> for the project's future residences, all subway trips to this station generated by the proposed project's residents in the weekday <u>AM and PM peak hours</u> would use the shuttle bus service. However, project-generated F line subway riders are expected to take the Q103 bus to and from the 21<sup>st</sup> Street-Queensbridge Station as this route provides a convenient and direct route to/from this station. As a result, the combined project generated increment in bus-only and bus-subway transfer ridership exceeds the *CEQR Technical Manual* threshold on only the Q103 bus route, as shown in Table 13-8. Therefore, a detailed bus line haul analysis for the Q103 bus route was performed for the <u>weekday AM</u> and PM peak hours in both directions.



				Subwa	y Linked			
		Bus On	y Trips	Bus	Trips	Total B	us Trips	
Bus	Direction	AM	PM	AM	PM	AM	PM	Screening Result
	To Site	10	24	8	16	18	40	
Q18	From Site	16	21	5	19	21	40	Screened Out
	Total	26	45	13	35	39	80	
	To Site	9	24	8	16	17	40	
Q102	From Site	16	21	5	18	21	39	Screened Out
	Total	26	45	13	34	38	<i>79</i>	
	To Site	10	24	30	103	40	127	Den ince leteiled
Q103	From Site	16	21	111	60	127	81	Requires detailed analysis
	Total	26	45	141	163	167	208	allarysis
ź	Total	77	135	167	232	244	367	

<b>Table 13-8:</b>	<b>Bus Line</b>	Haul	Screening	Analysis
Table 13-0.	Dus Line	: Ilaul	screening	Allarysis

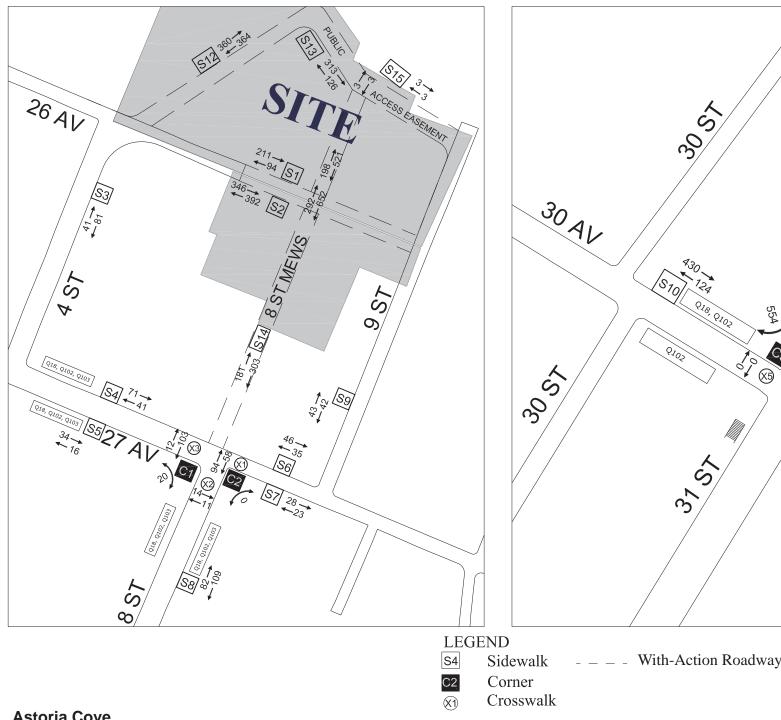
#### Pedestrians

According to *CEQR Technical Manual* criteria, projected pedestrian volume increases of less than 200 pedestrians per hour at any pedestrian element would not typically be considered a significant impact, since that level of increase would generally not be noticeable and therefore would not require further analysis. As shown in Table 13-7 and as noted above, the proposed project would generate a total of 1,635, 2,814, and 2,292 new pedestrian trips (including walk-only, subway and bus trips) during the weekday AM, midday, and PM peak hours, respectively. Since the project-generated pedestrian trips would exceed the *CEQR Technical Manual* threshold for analysis during each of the peak hours, a Level 2 screening assessment is required.

The project-generated trips were assigned to pedestrian elements within the vicinity of the project site and the nearest subway stations. Based on the pedestrian trip increments shown in Figures 13-7, 13-8, and 13-9 for the weekday AM, midday, and PM peak periods, respectively, the following existing and proposed sidewalks, corner areas, and crosswalks at several area intersections were selected for a detailed analysis (see Figure 13-10). It should be noted that the sidewalk elements 12 through 15 are only included in the With-Action analysis as they would be created as part of the Proposed Action. No new signalized corners or crosswalks would be introduced on the project site as part of the Proposed Action, and therefore, a detailed analysis of new crosswalk and/or corner elements on the project site is unwarranted pursuant to CEQR.

#### Sidewalks

- 1.  $26^{\text{th}}$  Avenue east of  $4^{\text{th}}$  Street (north)
- 2.  $26^{\text{th}}$  Avenue east of  $4^{\text{th}}$  Street (south)
- 3. 27<sup>th</sup> Avenue between 4<sup>th</sup> Street and 8<sup>th</sup> Street (north)
- 4. 27<sup>th</sup> Avenue between 4<sup>th</sup> Street and 8<sup>th</sup> Street (south)
- 5. 27<sup>th</sup> Avenue between 8<sup>th</sup> Street and 9<sup>th</sup> Street (north)
- 6.  $27^{\text{th}}$  Avenue between  $8^{\text{th}}$  Street and  $9^{\text{th}}$  Street (south)
- 7. 30<sup>th</sup> Avenue between 30<sup>th</sup> Street and 31<sup>st</sup> Street (north)
- 8.  $4^{\text{th}}$  Street between  $26^{\text{th}}$  Avenue and  $27^{\text{th}}$  Avenue (east)
- 9. 8<sup>th</sup> Street between 27<sup>th</sup> Avenue and Astoria Boulevard (east)
- 10. 9<sup>th</sup> Street north of 27<sup>th</sup> Avenue (west)
- 11. 31<sup>st</sup> Street between Newtown Avenue and 30<sup>th</sup> Avenue (west)
- 12.  $4^{th}$  Street between  $26^{th}$  Avenue and the public access easement (west)
- 13. Public access easement between  $4^{th}$  Street and the  $8^{th}$  Street Mews (south)

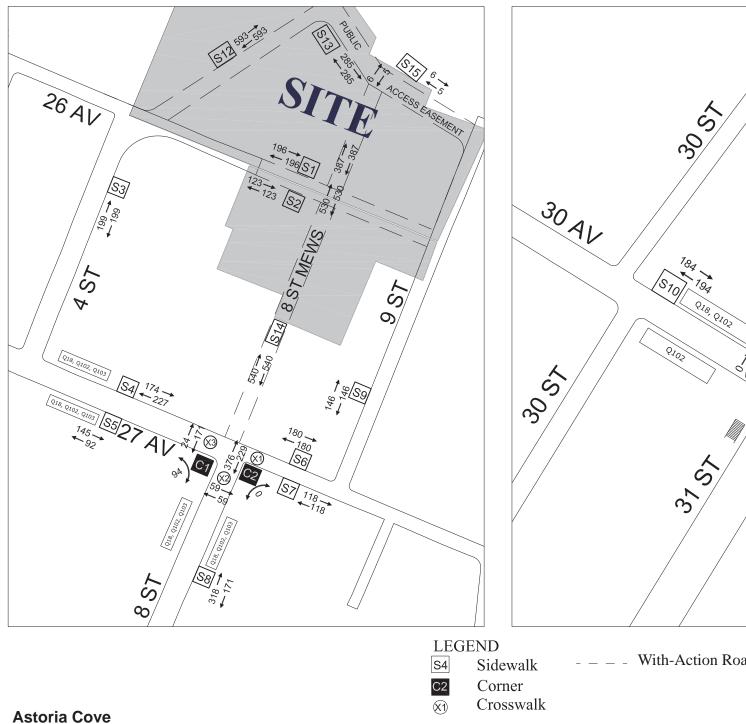




**Astoria Cove** 

Figure 13-7

**AM Peak Hour Pedestrian Increment** 



NEWTOWN AV Les Cor 18 378 1000 C3 0 30AV 9<sub>18</sub> 20 20 20

With-Action Roadway Geometry

Figure 13-8

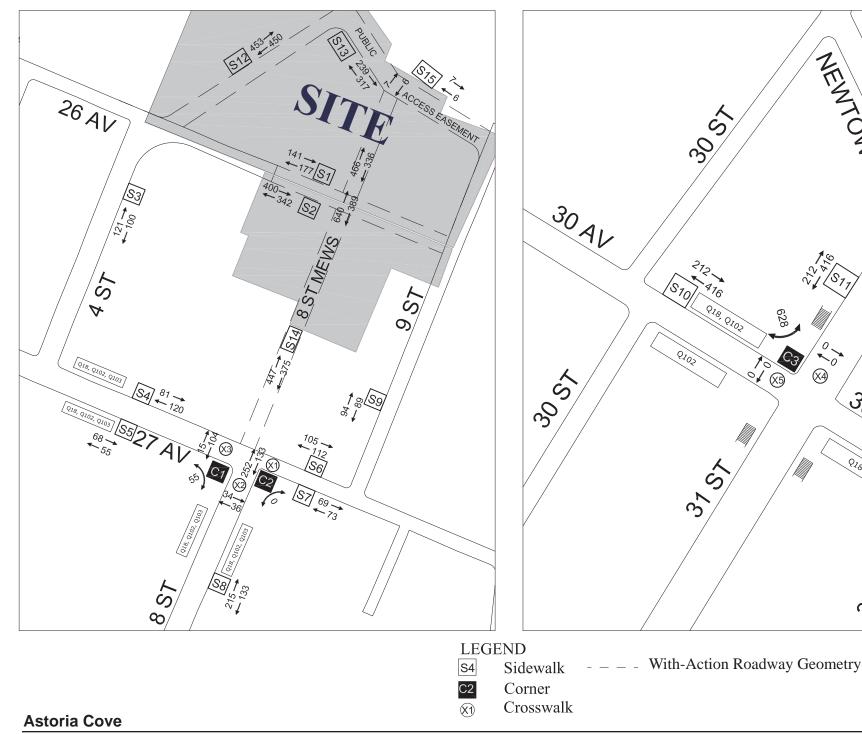


Figure 13-9

**PM Peak Hour Pedestrian Increment** 

NEWTOWN AV

91×

0

30AV

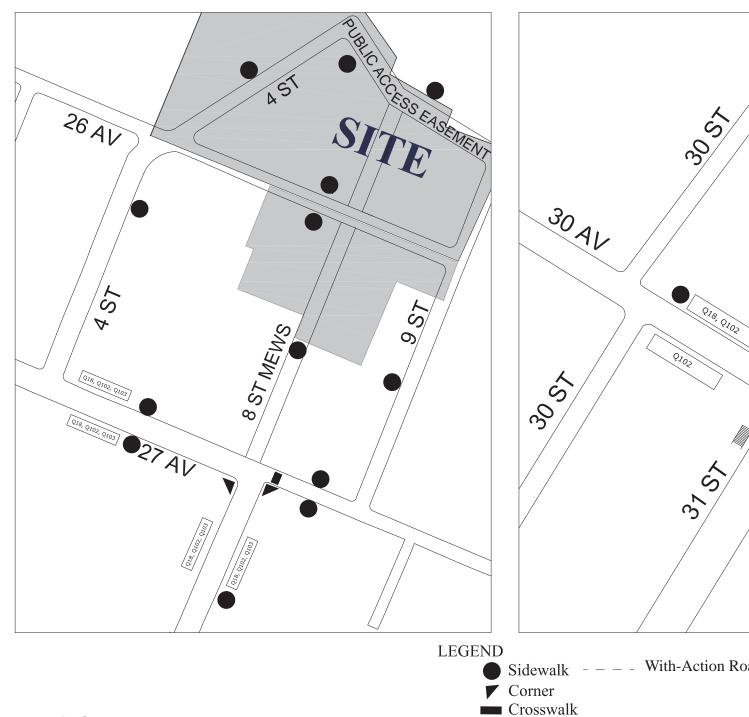
20 20 20

9<sub>18</sub>

628

C3

Les Control



NEWTOWN AV 50 CD Q18, Q102 30AV 9<sub>18</sub> 20 20 20 With-Action Roadway Geometry

Figure 13-10

- 14.  $8^{\text{th}}$  Street Mews south of  $26^{\text{th}}$  Avenue
- 15. Waterfront esplanade walkway/public access easement (north)

#### Corners

- 27<sup>th</sup> Avenue and 8<sup>th</sup> Street (southeast)
   27<sup>th</sup> Avenue and 8<sup>th</sup> Street (southwest)
   20<sup>th</sup> Avenue and 21<sup>st</sup> Street (northwest)
- 3.  $30^{\text{th}}$  Avenue and  $31^{\text{st}}$  Street (northwest)

#### Crosswalks

1. 27<sup>th</sup> Avenue and 8<sup>th</sup> Street (east)

#### Pedestrian and Vehicular Safety Evaluation

According to *CEQR Technical Manual* guidelines, sensitive land uses, including schools, require a detailed pedestrian and vehicular safety evaluation as increased traffic and pedestrian volumes generated by the proposed project may result in increasingly unsafe conditions at documented high-accident locations. In addition, as several new roadways would be created under the Proposed Action, a discussion of potential pedestrian and vehicular safety concerns at these project site locations is warranted. As discussed below in more detail, accident data was obtained from NYCDOT to identify these high-accident locations.

## F. TRANSPORTATION ANALYSIS METHODOLOGY

#### Traffic

#### Analysis Methodology

The capacity analyses at study area intersections are based on the methodology presented in the *Highway Capacity Manual (HCM) Software HCS+ Version 5.5.* Traffic data required for these analyses include the hourly volumes on each approach and various other physical and operational characteristics. Field inventories were conducted to document the physical layout, lane markings, curbside parking regulations, and other relevant characteristics needed for the analysis.

The HCM methodology provides a volume-to-capacity (v/c) ratio for each signalized intersection approach. The v/c ratio represents the ratio of traffic volumes on an approach to the approach's carrying capacity. A ratio of less than 0.90 is generally considered indicative of non-congested conditions in dense urban areas; when higher than this value, the ratio reflects increasing congestion. At a v/c ratio of between 0.95 and 1.0, near-capacity conditions are reached and delays can become substantial. Ratios of greater than 1.0 indicate saturated conditions with queuing. The HCM methodology also expresses quality of flow in terms of level of service (LOS), which is based on the amount of delay that a driver typically experiences at an intersection. LOS range from A, with minimal delay (10 seconds or less per vehicle), to F, which represents long delays (greater than 80 seconds per vehicle).

For unsignalized intersections, the HCM methodology generally assumes that major street traffic is not affected by minor street flows. Left turns from the major street are assumed to be affected by the opposing (or oncoming) major street flow. Minor street traffic is obviously affected by all conflicting movements. Similar to signalized intersections, HCM methodology expresses the quality of flow at unsignalized intersections in terms of LOS based on the amount of delay that a driver experiences. This relationship differs somewhat from the criteria used for signalized intersections, primarily because drivers expect different levels of performance from the two different kinds of transportation facilities. For

unsignalized intersections, LOS range from A, with minimal delay (10 seconds or less per vehicle), to F, which represents long delays (over 50 seconds per vehicle).

Table 13-9 shows the LOS/delay relationship for signalized and unsignalized intersections using the HCM methodology. LOS A, B, and C generally represent highly favorable to fair levels of traffic flow. At LOS D, the influence of congestion becomes noticeable. LOS E is considered to be the limit of acceptable delay, and LOS F is considered to be unacceptable to most drivers. In this study, a signalized lane grouping operating at LOS E or F or a v/c ratio of 0.90 or above is identified as congested.

	Average Delay p	er Vehicle (seconds)
LOS	Signalized Intersections	<b>Unsignalized Intersections</b>
А	0 - 10	0 - 10
В	> 10 - 20	> 10 - 15
С	> 20 - 35	> 15 - 25
D	> 35 - 55	> 25 - 35
Е	> 55 - 80	> 35 - 50
F	> 80	> 50

Source: 2000 Highway Capacity Manual.

#### Significant Impact Criteria

The identification of significant adverse traffic impacts at analyzed intersections is based on criteria presented in the CEOR Technical Manual. According to CEOR Technical Manual criteria, if a lane group under the With-Action condition is within LOS A, B, C, or marginally acceptable LOS D (average control delay less than or equal to 45 seconds per vehicle for signalized intersections or less than or equal to 30 seconds per vehicle for unsignalized intersections), the impact is not considered significant. If the lane group LOS deteriorates from LOS A, B, or C in the No-Action condition to worse than mid-LOS D (i.e., delay greater than 45 seconds per vehicle at signalized intersections or 30 seconds per vehicle for unsignalized intersections) or to LOS E or F under the With-Action condition, then a significant traffic impact has occurred. For a lane group operating at LOS D under the No-Action condition, a delay increase of five or more seconds is considered significant if the With-Action delay exceeds mid-LOS D. For a lane group operating at LOS E under the No-Action condition, an increase in projected delay of four or more seconds is considered significant, and for a lane group operating at LOS F under the No-Action condition, an increase in projected delay of three or more seconds is considered significant. For unsignalized intersections, the same criteria used for signalized intersections apply. Pursuant to CEQR, for a minor street to trigger a significant impact, 90 Passenger Car Equivalents (PCEs) in any peak hour must be identified in the future With-Action condition.

#### Transit

#### Subway

#### Analysis Methodology

The methodology presented in the *CEQR Technical Manual* for assessing subway station pedestrian circulation elements (stairs, escalators, and passageways), fare control elements (regular turnstiles, high entry/exit turnstiles [HEETs], and high exit turnstiles) compares existing and projected pedestrian volumes with the element's design capacity to yield a v/c ratio. All analyses reflect pedestrian flow volumes over a 15-minute interval during each peak hour.

The estimated v/c ratio is compared to NYCT criteria to determine an LOS for the operation of an element. Table 13-10 shows the LOS and corresponding v/c ratios for all subway station elements. Six levels of service are defined with letters A through F. LOS A is representative of free flow conditions without pedestrian conflicts and LOS F depicts severe congestion and queuing.

LOS	Description	V/C Ratio	
А	Free Flow	0.00 to 0.45	
В	Fluid Flow	0.45 to 0.70	
С	Fluid, somewhat restricted	0.70 to 1.00	
D	Crowded, walking speed restricted 1.00 to 1.33		
Е	Congested, some shuffling and queuing 1.33 to 1.67		
F	Severely congested, queued > 1.67		

Table 13-10: LOS	Criteria	for Subway	Station	Elements
10010 10 100 100	~			

Source: CEQR Technical Manual

Stairways and Passageways

Under *CEQR Technical Manual* guidelines, the capacity of a stairway or passageway is determined based on four factors: the NYCT guideline capacity, the effective width, surging <u>factors</u>, and <u>friction/</u>counter-flow factors, if applicable. NYCT guideline capacity is ten passengers per foot per minute (pfm) for stairs and 15 pfm for passageways. The effective width of a stair or passageway is the actual width adjusted to reflect pedestrian avoidance of sidewalls and center handrails, if present. A surging factor is applied to existing pedestrian volumes to reflect conditions where pedestrian flows tend to be concentrated (or surged) during shorter periods within the 15-minute analysis interval. This factor, which is based on the size of the station and the proximity of the pedestrian element to the station platforms, can reduce the calculated capacity by up to 25 percent. Lastly, a friction (or counter-flow) factor reducing calculated capacity by ten percent is applied where opposing pedestrian flows use the same stair or passageway. No friction factor is applied if the flow is all or predominantly in one direction.

#### Escalators and Turnstiles

In contrast with stairways and passageways, under *CEQR Technical Manual* guidelines the capacity of an escalator or turnstile is determined based on only two factors: the NYCT guideline capacity for a 15-minute interval and a surging factor of up to 25 percent.

#### Line Haul

An analysis of line haul capacity addresses the ability of trains to accommodate passenger loads. The analysis determines whether there is sufficient capacity per car per train to handle existing and projected future transit loads at the maximum load point of a subway line or at the location where the addition of project-generated passengers to No-Action passenger volumes would be the greatest. Line haul capacity analyses are based on per-car practical guidelines used by NYCT. These are 110 passengers per car for a 51-foot subway car, 145 passengers per car for a 60-foot car, and 175 passengers per car for a 75-foot car.

#### Significant Impact Criteria

The *CEQR Technical Manual* identifies a significant impact for stairways and passageways in terms of the minimum width increment threshold (WIT) based on the minimum amount of additional capacity that would be required to restore conditions to either their No-Action v/c ratio or to a v/c ratio of 1.00 (LOS C/D), whichever is greater. Stairways that are substantially degraded in level of service or that experience the formation of extensive queues are classified as significantly impacted. Significant adverse stairway or

passageway impacts are typically considered to have occurred once the thresholds shown in Table 13-11 are reached or exceeded.

and I assage ways				
With-Action	WIT for Significant Impact (inches)			
V/C Ratio	Stairway	Passageway		
1.00-1.09	8	13		
1.10-1.19	7	11.5		
1.20-1.29	6	10		
1.30-1.39	5	8.5		
1.40-1.49	4	6		
1.50-1.59	3	4.5		
<u>&gt;</u> 1.6	2	3		

Table 13-11: Significant Impact Thresholds for Stairways	
and Passageways	

Source: CEQR Technical Manual

For turnstiles, escalators, and high-wheel exit gates, the *CEQR Technical Manual* defines a significant impact as an increase from a No-Action v/c ratio of below 1.00 to a v/c ratio of 1.00 or greater. Where a facility is already at a v/c ratio of 1.00 or greater, a 0.01 change in v/c ratio is considered significant.

For subway line haul conditions, *CEQR Technical Manual* criteria specify that any increases in load levels that remain within practical capacity limits are generally not considered significant impacts. However, projected increases from a No-Action to a With-Action condition that exceeds practical capacity may be considered significant impacts if the Proposed Action generates five or more additional passengers per car.

#### Bus

#### Analysis Methodology

The operating conditions for bus service are measured in terms of the number of passengers carried per bus at the maximum load point for each route. This is determined by dividing the peak hour passenger count by the number of buses during that hour. The bus load levels are compared with the loading guidelines of 54 passengers for a 40-foot standard bus and 85 passengers for a 60-foot articulated bus. The bus analyses focus on the weekday AM and PM commuter peak hours as it is during these periods that overall demand on the bus system is usually highest.

#### Significant Impact Criteria

According to the *CEQR Technical Manual* and NYCT and MTA Bus Company guidelines, additional bus service along a route is recommended when load levels exceed maximum guideline capacity at the route's maximum load point. A significant impact is considered at the route's maximum load point where an increase in bus load levels would exceed the maximum capacity. NYCT's and MTA Bus Company's general policy is to provide additional bus service where demand warrants increased service, taking into account fiscal and operational constraints.

## Chapter 13: Transportation

#### Pedestrians

#### Analysis Methodology

Peak 15-minute pedestrian flow conditions during the weekday AM and PM peak hours are analyzed using the 2000 *Highway Capacity Manual* methodology and procedures outlined in the *CEQR Technical Manual*. Using this methodology, the congestion level of pedestrian facilities is determined by considering pedestrian volume, measuring the sidewalk or crosswalk width, determining the available pedestrian capacity and developing a ratio of volume flows to capacity conditions. The resulting ratio is then compared with LOS standards for pedestrian flow, which define a qualitative relationship at a certain pedestrian traffic concentration level. The evaluation of street crosswalks and corners is more complicated as these spaces cannot be treated as corridors due to the time incurred waiting for traffic lights. To effectively evaluate these facilities, a "time-space" analysis methodology is employed which takes into consideration the traffic light cycle at intersections.

LOS standards are based on the average area available per pedestrian during the analysis period, typically expressed as a 15-minute peak period. LOS grades from A to F are assigned, with LOS A representative of free flow conditions without pedestrian conflicts and LOS F depicting significant capacity limitations and inconvenience. Table 13-12 defines the LOS criteria for pedestrian crosswalk/corner area and sidewalk conditions, as based on the *Highway Capacity Manual* methodology.

LOS	Description	Crosswalk/Corner Area and Non-Platoon Sidewalk Criteria (ft <sup>2</sup> /ped)	Platoon Sidewalk Criteria (ft²/ped)
А	Unrestricted	> 60	> 530
В	Slightly Restricted	>40-60	> 90 - 530
С	Restricted but fluid	> 24 - 40	> 40 - 90
D	Restricted, necessary to continuously alter walking stride and direction	> 15 - 24	> 23 - 40
Е	Severely restricted	> 8 - 15	> 11 - 23
F	Forward progress only by shuffling; no reverse movement possible	<u>&lt;</u> 8	<u>&lt;</u> 11

Table 13-12: Pedestrian Crosswalk/Corner Area and Sidewalk Levels of Service Descriptions

**Notes:** Based on average conditions for 15 minutes

 $ft^2/ped =$  square feet of area per pedestrian

Sources: 2000 Highway Capacity Manual, 2014 CEQR Technical Manual

The analysis of sidewalk conditions includes a "platoon" factor in the calculation of pedestrian flow to more accurately estimate the dynamics of walking. "Platooning" is the tendency of pedestrians to move in bunched groups or "platoons" once they cross a street where cross traffic required them to wait for a signal. Platooning generally results in a level of service one level poorer than that determined for average flow rates.

#### Significant Impact Criteria

#### Sidewalks

As the project site is not located within a Central Business District (CBD), *CEQR Technical Manual* criteria define a significant adverse sidewalk impact to have occurred under platoon conditions if the average pedestrian space under the No-Action condition is greater than 44.3 square feet per pedestrian

 $[ft^2/ped]$  of effective sidewalk width, and the average pedestrian space under the With-Action condition is less than or equal to 40.0 ft<sup>2</sup>/ped (LOS D or worse). If the average pedestrian space under the With-Action condition is greater than 40.0 ft<sup>2</sup>/ped (LOS C or better), the impact should not be considered significant. If the No-Action pedestrian space is between 6.4 and 44.3 ft<sup>2</sup>/ped, a decrease in the average pedestrian space under the With-Action condition should be considered significant based on Table 13-13, which shows a sliding-scale that identifies what decrease in pedestrian space is considered a significant impact for a given pedestrian space value in the No-Action condition. If the decrease in average pedestrian space is less than the value indicated in Table 13-13, the impact is not considered significant. If the average pedestrian space under the No-Action condition is less than 6.4 sf/ped, then a decrease in pedestrian space greater than or equal to 0.3 ft<sup>2</sup>/ped under the With-Action condition should be considered significant.

#### Corner Areas and Crosswalks

For non-CBD areas, *CEQR Technical Manual* criteria define a significant adverse corner area or crosswalk impact to have occurred if the average pedestrian space under the No-Action condition is greater than 26.6  $\frac{ft^2/ped}{ped}$  and, under the With-Action condition, the average pedestrian space decreases to 24 ft<sup>2</sup>/ped or less (LOS D or worse). If the pedestrian space under the With-Action condition is greater than 24 ft<sup>2</sup>/ped (LOS C or better), the impact should not be considered significant. If the average pedestrian space under the No-Action condition is between 5.1 and 26.6 ft<sup>2</sup>/ped, a decrease in pedestrian space under the With-Action condition should be considered significant based on Table 13-14 which shows a sliding-scale that identifies what decrease in pedestrian space is considered a significant impact for a given amount of pedestrian space in the No-Action condition. If the average pedestrian space is less than the value in Table 13-14, the impact is not considered significant. If the average pedestrian space under the No-Action condition is less than 5.1 ft<sup>2</sup>/ped, then a decrease in pedestrian space greater than or equal to 0.2 ft<sup>2</sup>/ped should be considered significant.

#### **Pedestrian and Vehicular Safety Evaluation**

Under *CEQR Technical Manual* guidelines, an evaluation of pedestrian and vehicular safety is needed for locations within the traffic and pedestrian study areas that have been identified as high accident locations. These are defined as locations where 48 or more total reportable and non-reportable crashes or five or more pedestrian/bicyclist injury crashes have occurred in any consecutive 12 months of the most recent three-year period for which data are available. For these locations, accident trends would be identified to determine whether projected vehicular and pedestrian traffic would further impact safety, or whether existing unsafe conditions could adversely impact the flow of the projected new trips. The determination of potential significant safety impacts depends on the type of area where the project site is located, traffic volumes, accident types and severity, and other contributing factors. Where appropriate, measures to improve traffic and pedestrian safety should be identified and coordinated with NYCDOT.

#### Parking

The parking analysis identifies the extent to which on- and off-street parking is available and utilized under existing and future conditions and estimates the parking demand resulting from the proposed project during peak periods. It takes into consideration anticipated changes in area parking supply and provides a comparison of parking needs versus availability to determine if a parking shortfall is likely to result from parking displacement attributable to or additional demand generated by the Proposed Acton.

# Table 13-13: Significant Impact Criteria forSidewalks with Platooned Flow in a Non-CBDLocation

(	strian S ft²/ped	space	With-Action Condition Pedestrian Space Reduction to be Considered a Significant Impact (ft <sup>2</sup> /ped)
	> 44.3		With Action Condition $\leq 40.0$
43.5	to	44.3	Reduction $\geq 4.3$
42.5	to	43.4	Reduction $\geq 4.2$
41.6	to	42.4	Reduction $\geq 4.1$
40.6	to	41.5	Reduction $\geq 4.0$
39.7	to	40.5	Reduction $\geq 3.9$
38.7	to	39.6	Reduction $\geq 3.8$
37.8	to	38.6	Reduction $\geq 3.7$
36.8	to	37.7	Reduction $\geq 3.6$
35.9	to	36.7	Reduction $\geq 3.5$
34.9	to	35.8	Reduction $\geq 3.4$
34.0	to	34.8	Reduction $\geq 3.3$
33.0	to	33.9	Reduction $\geq 3.2$
32.1	to	32.9	Reduction $\geq 3.1$
31.1	to	32.0	Reduction $\geq 3.0$
30.2	to	31.0	Reduction $\geq 2.9$
29.2	to	30.1	Reduction $\geq 2.8$
28.3	to	29.1	Reduction $\geq 2.7$
27.3	to	28.2	Reduction $\geq 2.6$
26.4	to	27.2	Reduction $\geq 2.5$
25.4	to	26.3	Reduction $\geq 2.4$
24.5	to	25.3	Reduction $\geq 2.3$
23.5	to	24.4	Reduction $\geq 2.2$
22.6	to	23.4	Reduction $\geq 2.1$
21.6	to	22.5	Reduction $\geq 2.0$
20.7	to	21.5	Reduction $\geq 1.9$
19.7	to	20.6	Reduction $\geq 1.8$
18.8	to	19.6	Reduction $\geq 1.7$
17.8	to	18.7	Reduction $\geq 1.6$
16.9	to	17.7	Reduction $\geq 1.5$
15.9	to	16.8	Reduction $\geq 1.4$
15.0	to	15.8	Reduction $\ge 1.3$
14.0	to	14.9	Reduction $\geq 1.2$
13.2	to	13.9	Reduction $\geq 1.1$
12.1	to	13.0	Reduction $\ge 1.0$
11,2	to	12.0	Reduction $\ge 0.9$
10.2	to	11.1	Reduction $\ge 0.8$
9.3	to	10.1	Reduction $\ge 0.7$
8.3	to	9.2	Reduction $\ge 0.6$
7.4	to	8.2	Reduction $\ge 0.5$
6.4	to	7.3	Reduction $\ge 0.4$
	< 6.4		Reduction $\ge 0.3$

## Table 13-14: Significant Impact Criteria forCorners and Crosswalks in a Non-CBD Location

Pede	tion Cor estrian S (ft²/ped)	pace	With-Action Condition Pedestrian Space Reduction to be Considered a Significant Impact (ft <sup>2</sup> /ped)
	> 26.6		With Action Condition $\leq 24.0$
25.8	to	26.6	Reduction $\geq 2.6$
24.9	to	25.7	Reduction $\geq 2.5$
24	to	24.8	Reduction $\geq 2.4$
23.1	to	23.9	Reduction $\geq 2.3$
22.2	to	23	Reduction $\geq 2.2$
21.3	to	22.1	Reduction $\geq 2.1$
20.4	to	21.2	Reduction $\geq 2.0$
19.5	to	20.3	Reduction $\ge 1.9$
18.6	to	19.4	Reduction $\geq 1.8$
17.7	to	18.5	Reduction $\geq 1.7$
16.8	to	17.6	Reduction $\geq 1.6$
15.9	to	16.7	Reduction $\ge 1.5$
15	to	15.8	Reduction $\geq 1.4$
14.1	to	14.9	Reduction $\geq 1.3$
13.2	to	14	Reduction $\ge 1.2$
12.3	to	13.1	Reduction $\geq 1.1$
11.4	to	12.2	Reduction $\geq 1.0$
10.5	to	11.3	Reduction $\geq 0.9$
9.6	to	10.4	Reduction $\geq 0.8$
8.7	to	9.5	Reduction $\ge 0.7$
7.8	to	8.6	Reduction $\geq 0.6$
6.9	to	7.7	Reduction $\ge 0.5$
6	to	6.8	Reduction $\ge 0.4$
5.1	to	5.9	Reduction $\ge 0.3$
G	< 5.1		Reduction $\geq 0.2$

Source: 2014 CEQR Technical Manual

Source: 2014 CEQR Technical Manual

### G. TRAFFIC

#### Existing <u>Weekday</u> Conditions

#### Study Area Network

Due to the proximity of the Astoria Cove project site to the Halletts Point project site to the west, many intersections included as part of this traffic analysis overlap with the intersections analyzed as part of the *Halletts Point FEIS*. Therefore, at the request of DCP, the 2011 existing conditions traffic network presented as part of the *Halletts Point FEIS* traffic analyses was utilized to create a baseline traffic network for this EIS's weekday peak hour analyses. Traffic data was collected at the following three intersections identified for analysis in this EIS as these locations were not included in the *Halletts Point FEIS* baseline network: 26<sup>th</sup> Avenue at 4<sup>th</sup> Street (unsignalized), 30<sup>th</sup> Avenue at 14<sup>th</sup> Street (unsignalized), and 30<sup>th</sup> Avenue at 21<sup>st</sup> Street (signalized). The 2012 baseline traffic count data collected and existing street conditions recorded at the three additional analyzed intersections. Lastly, a one year background growth rate (*CEQR Technical Manual* guideline suggests a rate of 0.5 percent be applied for the first five years of background growth) was applied to the baseline *Halletts Point FEIS* 2011 traffic network, supplemented with the additional data discussed above, to create the 2012 representative traffic network analyzed in this EIS.

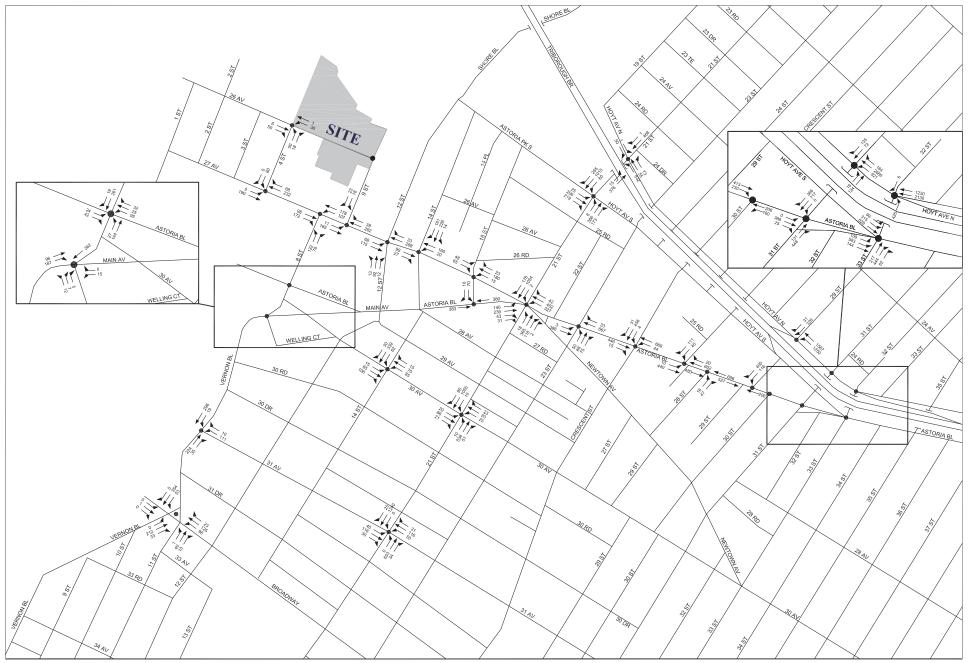
29 existing intersections within the primary traffic study area (bounded by Hoyt Avenue North to the north, Broadway to the south,  $33^{rd}$  Street to the east, and  $4^{th}$  Street to the west) were included in the detailed <u>weekday peak hour</u> traffic analysis discussed below.<sup>1</sup> Of these 29 intersections, which are shown in Figure 13-5, currently 18 are signalized and 11 are unsignalized. Existing traffic volumes for the weekday AM, midday, and PM peak hours at analyzed intersections are shown in Figures 13-11, 13-12, and 13-13, respectively.

The roadway network around the project site generally consists of a grid of local streets within the Astoria neighborhood in Western Queens. The network provides access to major City and regional connections, including the Grand Central Parkway (GCP), the Robert F. Kennedy Bridge (RFK Bridge), the Brooklyn-Queens Expressway (BQE), and the Ed Koch Queensboro/59<sup>th</sup> Street Bridge to the south. The study area's key north-south roadways include Vernon Boulevard, 21<sup>st</sup> Street, and 31<sup>st</sup> Street. Key east-west roadways within the study area include Hoyt Avenue, the GCP, Astoria Boulevard, and 27<sup>th</sup> Avenue.

Vernon Boulevard is a two-way north-south street along the East River waterfront in Queens. The roadway extends from Borden Avenue in Hunter's Point (to the south) to Main Avenue in Astoria (to the north). Vernon Boulevard between Main Avenue and Broadway is traversed by approximately 250 to 300 vehicles per hour (vph), 200 to 300 vph, and 300 to 500 vph in the northbound direction in the <u>weekday</u> AM, midday, and PM peak hours, respectively. Southbound vehicular volumes are approximately 300 to 400, 200 to 250, and 200 to 300 vph in the <u>weekday</u> AM, midday, and PM peak hours, respectively. Within the study area, the road operates with one travel lane and a buffered bike lane in each direction. In addition, Vernon Boulevard is a local truck route and has local bus service <u>via</u> the Q103, which provides weekday-only service between Astoria and Hunter's Point. Curbside parking is found in the northbound direction.

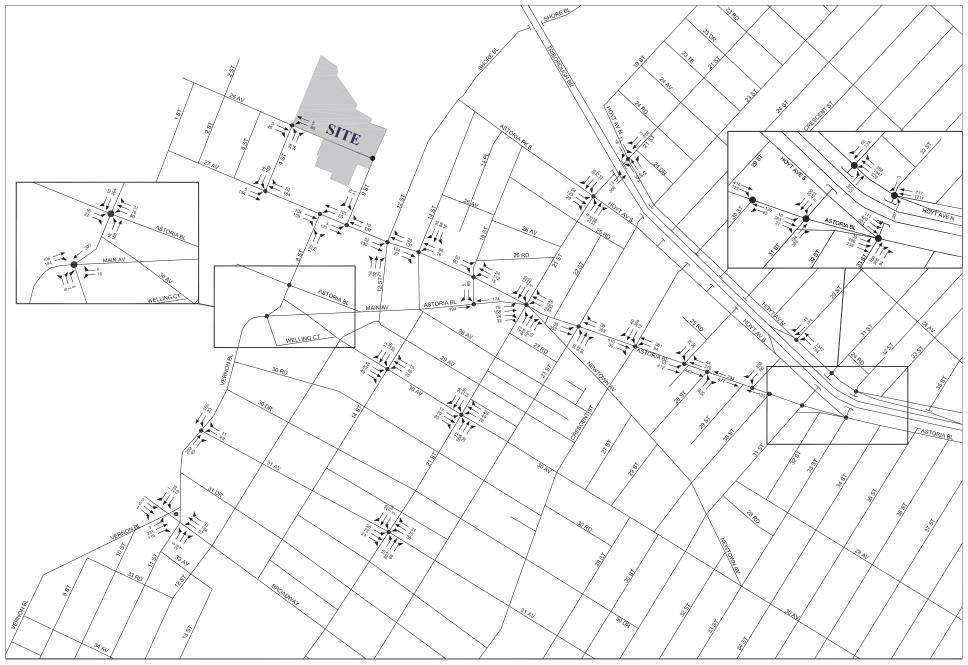
21<sup>st</sup> Street is also a two-way north-south street that runs between Hunter's Point (from Borden Avenue in the south) and Astoria (from 20<sup>th</sup> Avenue in the north). The roadway provides direct access to the Ed

<sup>&</sup>lt;sup>1</sup> One additional intersection (analysis location A at the intersection of 26<sup>th</sup> Avenue and 9<sup>th</sup> Street) does not exist under existing conditions and is therefore only included in the future No-Action and future With-Action analyses.

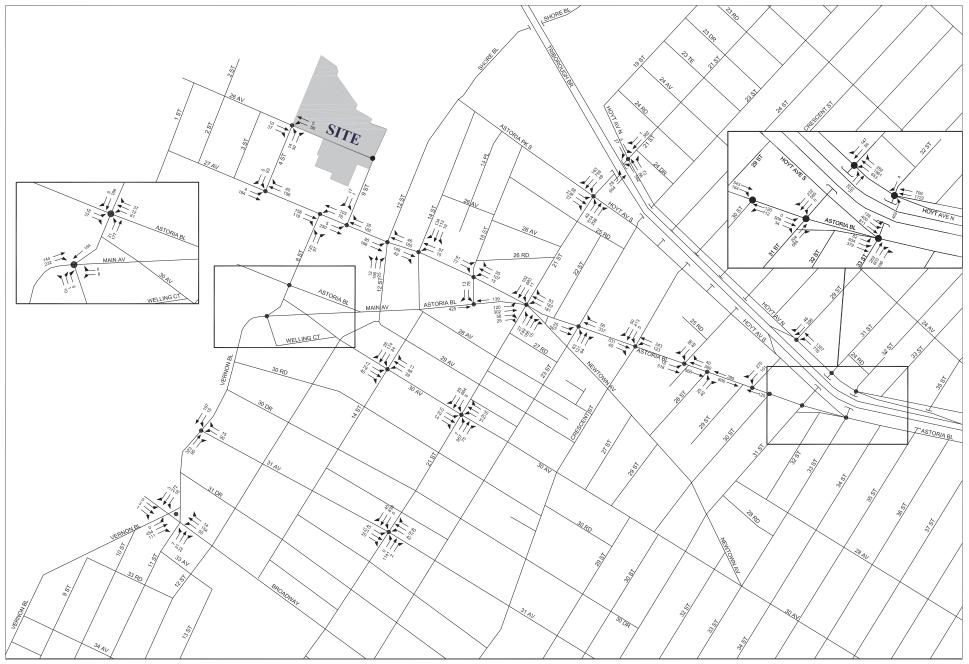


## Astoria Cove

Figure 13-11



## Astoria Cove



## Astoria Cove

Koch Queensboro Bridge and the Queens Midtown Tunnel. 21<sup>st</sup> Street between 24<sup>th</sup> Drive and 31<sup>st</sup> Avenue is traversed in the northbound direction by approximately 500 to 700 vph, 350 to 850 vph, and 650 to 1,200 vph in the weekday AM, midday, and PM peak hours, respectively. For the southbound direction, volumes are 1,100 to 1,350 vph, 550 to 900 vph, and 700 to 1,000 vph in the <u>weekday</u> AM, midday and PM peak hours, respectively. Within the study area, and south of the RFK Bridge, 21<sup>st</sup> Street operates with two lanes and a parking lane in each direction. North of the RFK Bridge, it provides one lane, a Class II bike lane, and a parking lane in each direction. In addition, 21<sup>st</sup> Street is a local truck route and is served by multiple local bus routes: the Q66, which provides daily service between Flushing and Long Island City; the Q69, which operates daily between Long Island City and Jackson Heights; and the Q100, which provides limited-stop service between Long Island City and Riker's Island.

31<sup>st</sup> Street is a two-way north-south street extending from Northern Boulevard and 40<sup>th</sup> Avenue near Queens Plaza (in the south) to 20<sup>th</sup> Avenue in Astoria (to the north). 31<sup>st</sup> Street generally carries approximately 200 to 500 vehicles during the weekday peak hours in both northbound and southbound directions. As 31<sup>st</sup> Street intersects Hoyt Avenue North and Hoyt Avenue South at Triborough Plaza, the range in northbound and southbound vehicle volume increases to 550 to 750 vph and 600 to 1,100 vph, respectively during all peak hours. The on- and off-ramp connections to the RFK Bridge and GCP are located at this junction. The road typically consists of one travel lane and a parking lane in each direction. Elevated tracks and stations for the N/Q subway lines are located directly above the roadway. In addition, 31<sup>st</sup> Street is served by the Q102 local bus route, which operates daily between Roosevelt Island and Astoria.

Hoyt Avenue, a designated truck route, operates as Hoyt Avenue North in the westbound direction and Hoyt Avenue South in the eastbound direction. <u>During the weekday peak hours</u>, Hoyt Avenue South carries approximately 350 to 750 vph west of 29<sup>th</sup> Street and 1,050 to 1,450 vph between 29<sup>th</sup> and 33<sup>rd</sup> Streets. West of 29<sup>th</sup> Street, Hoyt Avenue North carries approximately 950 to 1,600 vph during the <u>weekday</u> AM peak hour and 650 to 1,400 vph during the <u>weekday</u> midday and PM peak hours. Between 29<sup>th</sup> and 31<sup>st</sup> Streets, volumes along Hoyt Avenue North are approximately 2,800 vph in the <u>weekday</u> AM peak hour and 2,100 vph in the <u>weekday</u> midday and PM peak hours. West of 32<sup>nd</sup> Street, the roadway functions as a service road to the GCP and typically provides three to four travel lanes to traffic, with more at GCP merge/diverge points. Additionally, a parking lane and a Class II bike lane are provided in each direction. Hoyt Avenue is served by the Q19 local bus route, which operates daily between Flushing and Astoria, as well as the M60, which provides daily service between Morningside Heights <u>in</u> Manhattan, and LaGuardia Airport<u>in Queens</u>.

The GCP is a major east-west parkway with three lanes in each direction. The highway extends from the RFK Bridge in the west to Long Island in the east, where it becomes the Northern State Parkway at the Queens-Nassau County border. The GCP carries heavy traffic between the Bronx and Manhattan and between Queens and Long Island, as well as providing direct connection to LaGuardia Airport in East Elmhurst, Queens. The GCP is also a truck route between the RFK Bridge and the BQE.

Astoria Boulevard is an east-west thoroughfare running between the Astoria Houses campus in the west to access points to the GCP and Whitestone Expressway in the east. The roadway is one-way eastbound west of 31<sup>st</sup> Street. East of 31<sup>st</sup> Street, Astoria Boulevard functions as the eastbound and westbound service road to the GCP after merging with Hoyt Avenue South and Hoyt Avenue North, respectively. <u>During the weekday peak hours, approximately, 200 to 500 vph and 125 to 375 vph travel along Astoria Boulevard between 8<sup>th</sup> and 21<sup>st</sup> Streets in the eastbound direction westbound directions, respectively. Between 21<sup>st</sup> and 31<sup>st</sup> Streets, traffic volumes increase to 400 to 700 vph and 250 to 750 vph in the eastbound and westbound directions, respectively. Astoria Boulevard is also a local truck route and is served by the Q19 local bus route, which operates daily between Flushing and Astoria, and the M60,</u>

which provides daily service between Morningside Heights<u>in</u> Manhattan, and LaGuardia Airport<u>in</u> <u>Queens</u>.

27<sup>th</sup> Avenue is a two-way east-west road that runs between 1<sup>st</sup> Street <u>in</u> the west and 21<sup>st</sup> Street <u>in</u> the east, where it merges with Astoria Boulevard. The street provides one travel lane in each direction with parking typically on either side. Between 18<sup>th</sup> and 21<sup>st</sup> Streets, 27<sup>th</sup> Avenue is one-way westbound only. 27<sup>th</sup> Avenue serves as the primary east-west access route to the peninsula <u>on which</u> the project site is located. Between 4<sup>th</sup> and 21<sup>st</sup> Streets, 27<sup>th</sup> Avenue has eastbound traffic volumes ranging from approximately 100 to 250 vph in the <u>weekday</u> AM and PM peak hours and 150 to 275 in the <u>weekday</u> midday peak hour. Westbound traffic volumes range from approximately 175 to 325 vph, 100 to 250 vph, and 150 to 300 vph in the <u>weekday</u> AM, midday, and PM peak hours, respectively.

8<sup>th</sup> Street is a two-way street with one travel lane, a parking lane, and a Class II bike lane in each direction. It is the primary north-south access to the peninsula and extends between 27<sup>th</sup> Avenue to the north and Main Avenue to the south. During all weekday peak hours, traffic volumes along 8<sup>th</sup> Street range from approximately 175 to 200 vph and 200 to 300 vph in the northbound and southbound directions, respectively. 8<sup>th</sup> is served by multiple local bus routes: the Q18, which operates daily between Maspeth and Astoria; the Q102, which operates daily between Roosevelt Island and Astoria; and the Q103, which provides weekday-only service between Astoria and Hunter's Point.

Additional designated truck routes within the study area include 29<sup>th</sup> Street, 24<sup>th</sup> Avenue, Broadway, and the RFK Bridge.

Existing traffic volumes are generally low along 26<sup>th</sup> Avenue and 4<sup>th</sup> and 9<sup>th</sup> Streets, the project site's main roadway frontages.

### <u>Weekday</u> Intersection Capacity Analysis

Table 13-15 summarizes the existing lane group LOS during the weekday AM, midday, and PM peak periods. During the AM peak hour, ten individual lane groups operate at LOS E and three operate at LOS F. During the midday peak hour, one traffic movement operates at LOS E and one operates at LOS F, while during the PM peak hour eight individual traffic movements operate at LOS E and none operate at LOS F.

	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour
Overall LOS A/B/C	64	85	72
Overall LOS D	25	16	22
Overall LOS E	10	1	8
Overall LOS F	3	1	0
Number of movements at LOS E or F of approximately 102 movements analyzed	13	2	8

 Table 13-15: Existing Weekday Lane Group LOS Summary

Table 13-16 shows the detailed v/c ratios, delays, and LOS by movement at each of the 29 analyzed existing intersections in each peak hour and identifies those movements that are considered congested in one or more peak hour (i.e., movements operating at LOS E or F and/or with a high v/c ratio—0.90 and above). These congested locations are listed in the following.

<b>T 11 13 16 6</b>					<b>T</b> 4 4 •
Table 13-16: 2	2012 Existing	Weekday Con	ditions–LOS a	t Analyzed	Intersections

		AN	1 Peak H	our		Midd	ay Peak 1	Hour		PN	A Peak Ho	ur	
Intersection	Lane	V/C	Delay	LOS		V/C	Delay	LOS		V/C	Delay	LOS	
	Group	Ratio	(sec/weh)			Ratio	(sec/veh)		1	Ratio	(sec/veh)		
1. 26 <sup>th</sup> Avenue & 4 <sup>th</sup> Street	WB-LT	0.03	7.7	А		0.07	7.9	А		0.05	7.9	А	
(Unsignalized-Two Way Stop)	NB-LR	0.10	10.1	В		0.08	10.3	В		0.06	9.5	А	
2. 27 <sup>th</sup> Avenue & 4 <sup>th</sup> Street	EB-LT	NA	10.0	А		NA	9.6	А		NA	9.8	А	_
(Unsignalized-All Way Stop)	WB-T	NA	11.1	В		NA	10.4	В		NA	10.5	В	
	WB-R	NA	7.9	А		NA	8.1	А		NA	8.0	А	
	SB-LR	NA	9.8	А		NA	9.8	А		NA	9.5	А	
3. 27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street	EB-TR	0.59	18.5	В		0.54	17.2	В		0.48	15.6	В	_
	WB-LT	0.81	30.7	С		0.55	18.4	В		0.41	14.9	В	
	NB-L	0.41	24.5	С		0.30	22.3	С		0.33	22.9	С	
	NB-R	0.26	22.0	С		0.28	22.4	С		0.30	22.6	С	
4. 27 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	EB-LT	0.07	8.6	А		0.05	8.0	А		0.08	8.4	А	
(Unsignalized-Two Way Stop)	NB-LTR	0.43	25.5	D		0.24	15.9	С		0.69	38.3	Е	*
5. 27 <sup>th</sup> Avenue & 14 <sup>th</sup> Street	EB-TR	NA	10.6	В		NA	9.2	А		NA	9.9	А	
(Unsignalized-All Way Stop)	WB-LT	NA	12.1	В		NA	9.0	А		NA	9.6	А	
	SB-LTR	NA	16.8	С		NA	9.2	А		NA	10.5	В	
6. 27 <sup>th</sup> Avenue & 18 <sup>th</sup> Street	EB-L	0.07	9.3	А		0.07	8.2	А	+	0.09	8.1	А	-
(Unsignalized-Two Way Stop)	WB-L	0.01	7.5	А		0.01	7.6	А		0.01	7.7	А	
7. Astoria Boulevard & 21 <sup>st</sup> Street	EB-L	0.82	59.3	Е	*	0.25	34.6	С	+	0.45	41.9	D	-
	EB-TR	0.82	52.5	D		0.38	36.1	D		0.75	47.7	D	
	WB-L	0.95	57.8	Е	*	0.81	49.3	D		0.83	58.3	Е	*
	WB-TR	0.72	42.7	D		0.36	35.0	D		0.69	48.1	D	
	NB-LTR	0.80	35.7	D		1.05	69.9	2	*	1.02	46.2	D	*
	SB-LTR	1.05	60.8	Е	*	0.97	49.1	D	*	0.87	34.4	С	
8. Astoria Boulevard & 23 <sup>rd</sup> Street	EB-LT	0.64	20.1	С		0.61	16.5	В		0.69	21.1	С	
	WB-TR	0.81	24.4	С		0.66	15.3	В		0.63	18.4	В	
	NB-LTR	0.48	33.0	С		0.53	27.8	С		0.57	35.3	D	
9. Astoria Boulevard & Crescent Street	EB-TR	0.72	24.0	С		0.63	17.3	В		0.82	27.9	С	_
	WB-LT	0.86	27.5	С		0.98	31.1	C		0.99	38.6	D	*
	SB-LTR	1.05	66.5	Е	*	1.03	54.2	D	*	1.00	50.7	D	*
10. Astoria Boulevard & 27 <sup>th</sup> Street	EB-LT	0.54	15.2	В		0.44	13.6	В		0.57	15.7	В	
	WB-TR	0.76	19.6	В		0.62	16.3	В		0.52	14.3	В	
	SB-LR	0.75	38.8	D		0.47	34.1	С		0.71	38.0	D	
11. Astoria Boulevard & 28 <sup>th</sup> Street	NB-LR	0.32	20.8	С		0.30	18.9	С	$\uparrow$	0.25	17.4	С	-
(Unsignalized-Two Way Stop)													
12. Astoria Boulevard & 29 <sup>th</sup> Street	EB-T	0.97	65.6	Е	*	0.75	24.9	С	+	0.97	58.4	Е	*
	WB-T	0.42	27.1	С		0.22	13.4	В		0.21	20.2	С	
	SB-L	0.17	16.9	В		0.12	18.0	В		0.16	19.5	В	
	SB-R	0.65	26.9	С		0.58	26.2	С		0.48	25.1	С	
	эд-к	0.65	20.9	U		0.58	20.2	C		0.48	23.1		L

Table 13-16 (	(continued):	: 2012 Existing	Weekday	Conditions-I	OS at Anal	yzed Intersections
14010 10 10 (	commucu	· avia Lansung	<u> </u>	conditions 1	100 ut minu	y hear intersections

	12 Existing <u>Weekday</u> Conditions–1 AM Peak Hour								PM Peak Hour			
<b>T</b> ( )	Ŧ	A V/C			$\neg$		ay Peak H		_			
Intersection	Lane		Delay	LUS		V/C	Delay	LUS		V/C	Delay	LUS
	Group		(sec/weh)		-		(sec/veh)				(sec/veh)	
13. Astoria Boulevard & 30 <sup>th</sup> Street (Unsignalized-Two Way Stop)	WB-LT	0.26	11.3	В		0.08	9.2	А		0.17	10.4	В
14. Astoria Boulevard & 31 <sup>st</sup> Street		0.70	27.7	D	-	0.95	21.7	C		0.00	46.4	D
14. Astoria Boulevard & 31 Street	EB-LTR	0.79	37.7	D		0.85	31.7	C		0.96	46.4	D
	NB-T	0.49	41.2	D		0.51	33.2	C		0.49	41.0	D
	NB-R	0.63	15.3	B		0.50	8.5	A		0.79	21.4	C
	SB-T SB-R	0.86 0.53	31.4 19.0	C B		0.62 0.29	19.1 14.1	B B		0.67 0.30	21.8 14.9	C B
15. Hoyt Avenue S./Astoria Boulevard	Astoria Blvd (EB-LT)	0.91	50.4	D	*	0.02	44.5	D	*	1.05	73.9	Е
	NB-TR	1.05	50.4 78.6	D E	*	0.92 0.77	44.5 37.3			1.05	73.9 69.4	E
33rd Street	NB-IR NB-R	1.05	78.0 79.3	E	*	0.77	40.7	D D		1.05 1.04	69.4 69.9	E
	Hoyt Ave (EB-LT)	0.54	25.6	C	Ì	0.70	40.7 26.7	C		0.73	35.1	D
16. Hoyt Avenue N. & 29 <sup>th</sup> Street	WB-L	0.71	11.6	В		0.54	11.5	В		0.41	12.3	В
10. Hoyt Avenue A. & 25 Sheet	WB-LT	0.71	11.3	B		0.50	10.8	В		0.56	14.1	B
	SB-R	0.99	90.5	F	*	0.30	34.5	C		0.78	49.8	D
17. Hoyt Avenue N. & 31 <sup>st</sup> Street	WB-L	1.02	87.8	F	*	1.01	83.2	F	*	0.42	16.0	В
	WB-T	0.90	21.6	С	*	0.71	17.2	В		0.68	20.1	С
	WB-R	0.31	10.2	В		0.61	19.6	В		0.65	23.6	С
	NB-LT	0.28	35.6	D		-	-	-		0.28	28.1	С
	NB-DefL	-	-	-		0.50	29.3	С		-	-	-
	NB-T	-	-	-		0.22	21.1	Ĉ		-	-	-
	SB-T	0.26	36.0	D		0.44	24.1	C		0.15	26.5	С
	SB-R	0.69	53.7	D		0.24	21.9	C		0.46	33.6	C
18. Astoria Boulevard N. & 32 <sup>nd</sup> Street	WB-Main-T	0.51	8.6	А		0.35	7.8	А		0.31	9.1	А
	WB-Ramp-T	1.05	81.1	F	*	0.92	22.0	С	*	0.89	23.5	С
	NB-L	0.56	43.7	D		0.33	28.5	С		0.50	38.4	D
	SB-R	0.03	38.0	D		0.02	25.9	С		0.02	33.3	С
	Overall											
19. Astoria Boulevard & 8th Street	EB-LR	0.25	28.5	С		0.12	26.4	С		0.26	28.6	С
	WB-L	0.26	28.5	С		0.25	28.5	С		0.16	27.0	С
	WB-TR	0.20	27.7	С		0.15	27.0	С		0.15	26.9	С
	NB-LT	0.34	15.1	В		0.31	14.8	В		0.40	15.5	В
	SB-TR	0.50	17.9	В		0.31	15.1	В		0.29	14.8	В
20. 30 <sup>th</sup> Avenue & 14 <sup>th</sup> Street	EB-LTR	NA	11.5	В		NA	8.7	А		NA	9.1	А
(Unsignalized-All Way Stop)	WB-LTR	NA	12.3	В		NA	8.7	А		NA	9.0	А
	SB-LTR	NA	22.3	С		NA	9.2	А		NA	10.6	В
21. 30 <sup>th</sup> Avenue & 21 <sup>st</sup> Street	EB-LTR	0.41	36.1	D		0.30	33.5	С		0.32	33.9	С
	WB-LTR	0.43	36.7	D		0.33	34.2	С		0.41	36.2	D
	NB-LTR	0.47	13.9	В		0.48	14.1	В		0.71	19.1	В
	SB-LTR	0.69	18.1	В		0.37	12.4	В		0.42	13.1	В
22. Vernon Boulevard & Welling Court/	EB-LT	0.96	47.1	D	*	0.79	37.7	D		1.04	66.2	E
8th Street	WB-TR	0.03	21.0	С		0.03	21.0	С		0.04	21.1	С
	NB-LTR	0.24	31.2	С		0.14	28.9	С		0.08	28.2	С
i	SB-R	0.73	36.2	D		0.55	31.3	С		0.47	29.5	С

Table 13-16 (	(continued)	: 2012 Existing	Weekday	Conditions_L	OS at Analy	zed Intersections
10010 10 10 (	commucu,	· avia Lansung	ricchau	Contaitions L	OD at minur	

		Al	M Peak H	lour		Midd	ay Peak	Hour	PN	PM Peak Hour			
Intersection	Lane	V/C	Delay	LOS		V/C	Delay	LOS	V/C	Delay	LOS		
	Group	Ratio	(sec/veh)	)		Ratio	(sec/veh	)	Ratio	(sec/veh)			
23. Astoria Boulevard & 18 <sup>th</sup> Street (Unsignalized-Two Way Stop)	SB-LR	0.30	20.8	С		0.20	12.7	В	0.21	14.3	В		
24. Hoyt Avenue N. & 21 <sup>st</sup> Street	EB-L EB-R WB-L WB-TR NB-L NB-T SB-TR	0.02 0.36 0.89 0.24 0.27 1.00 0.97	40.4 47.1 43.3 14.7 30.4 75.1 47.2	D D B C E D	* *	0.11 0.13 0.67 0.16 0.10 0.74 0.55	42.0 42.3 38.0 14.1 25.1 41.1 32.7	D D B C D C	0.09 0.17 0.59 0.27 0.16 1.05 0.73	41.7 43.0 36.4 15.5 25.8 78.2 37.6	D D B C E *		
25. Hoyt Avenue S./Astoria Park S. & 21st Street	EB-L EB-TR NB-LTR SB-LTR	0.12 1.02 0.52 0.98	29.9 61.1 14.6 33.2	C E B C	* *	0.21 0.40 0.41 0.59	31.5 35.3 13.1 15.5	C D B B	0.17 0.73 0.86 0.84	30.7 43.2 22.5 23.6	C D C C		
26. 27 <sup>th</sup> Avenue & 9 <sup>th</sup> Street (Unsignalized-Two Way Stop)	EB-LT SB-LR	0.01 0.11	8.2 12.0	A B		0.00 0.07	7.7 10.0	A A	0.01 0.04	7.8 9.7	A A		
27. Vernon Boulevard & 31st Avenue (Unsignalized-Two Way Stop)	WB-LR SB-LT	0.49 0.02	23.5 8.1	C A		0.20 0.03	15.0 7.9	B A	0.37 0.02	19.8 8.4	C A		
28. Vernon Boulevard & Broadway/ 11th Street	EB-LTR WB-LTR NB(Vernon Blvd)-LT NB(Vernon Blvd)-R NB(11 Street)-LTR SB-LTR	0.01 1.01 0.24 0.04 0.36 0.96	28.2 56.0 7.8 6.4 40.8 45.8	C E A D D	* *	0.02 0.86 0.25 0.16 0.21 0.51	26.1 43.8 8.2 7.5 32.8 26.2	C D A C C	0.03 0.82 0.44 0.12 0.32 0.57	33.2 50.8 9.0 6.3 38.0 28.0	C D A D C		
29. 31st Avenue & 21st Street	EB-LTR WB-LTR NB-TR SB-TR	0.64 0.56 0.43 0.78	43.9 40.0 13.2 20.7	D D B C		0.33 0.40 0.58 0.50	34.2 35.5 15.6 14.4	C D B B	0.48 0.40 0.69 0.57	34.4 32.0 20.8 18.1	C C C B		

#### Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9) Analysis is based on the 2010 *Highway Capacity Manual* methodology (HCS+, version 5.5) *This table has been updated for the FEIS.* 

27<sup>th</sup> Avenue and 12<sup>th</sup> Street (unsignalized)

- Northbound shared left-turn/through/right-turn (PM)

Astoria Boulevard and 21<sup>st</sup> Street

- Eastbound left-turn (AM)
- Westbound left-turn (AM and PM)
- Northbound shared left-turn/through/right-turn (midday and PM)
- Southbound shared left-turn/through/right-turn (AM and midday)

Astoria Boulevard and Crescent Street

- Westbound shared left-turn/through (midday and PM)
- Southbound shared left-turn/through/right-turn (AM, midday, and PM)

Astoria Boulevard and 29<sup>th</sup> Street

- Eastbound through (AM and PM)

Astoria Boulevard and 31<sup>st</sup> Street

Eastbound shared left-turn/through/right-turn (PM)

Hoyt Avenue South/Astoria Boulevard and 33<sup>rd</sup> Street

- Eastbound shared left-turn/through on Astoria Boulevard (AM, midday, and PM)
- Northbound shared through/right-turn (AM and PM)
- Northbound right-turn (AM and PM)

Hoyt Avenue North and 29th Street

- Southbound right-turn (AM)

Hoyt Avenue North and 31st Street

- Westbound left-turn (AM and midday)
- Westbound through (AM)

Astoria Boulevard North and 32<sup>nd</sup> Street

- Westbound through from off-ramp (AM and midday)

Vernon Boulevard and Welling Court/8<sup>th</sup> Street

- Eastbound shared left-turn/through (AM and PM)

Hoyt Avenue North and 21st Street

- Northbound through (AM and PM)
- Southbound shared through/right-turn (AM)

*Hoyt Avenue South/Astoria Park South and 21<sup>st</sup> Street* 

- Eastbound shared through/right-turn (AM)
- Southbound shared left-turn/through/right-turn (AM)

Vernon Boulevard and Broadway/11<sup>th</sup> Street

- Westbound shared left-turn/through/right-turn (AM)
- Southbound shared left-turn/through/right-turn (AM)

#### Future without the Proposed Action (No-Action Condition)

As impact analyses are based on the incremental change to expected future conditions as a result of a proposed project, a future without the Proposed Action condition, the 2023 No-Action condition, was developed. The 2023 No-Action condition incorporates changes to the study area's traffic network as a result of general background growth and traffic demand and traffic operation changes associated with developments anticipated to be completed by 2023.

As per *CEQR Technical Manual* guidelines, an annual background growth rate of 0.5 percent was assumed for the first five years (2012 - 2017) and 0.25 percent for the remaining years (2018 - 2023). In addition, a total of 67 projects/developments are planned or proposed within or just beyond the study area. <u>Based on their size, it</u> was determined that background growth would account for the increase in travel demand for 36 of the 67 No-Action projects. 2023 No-Action traffic volumes were determined by adding the background growth and estimated volume increments associated with the remaining 31 more substantial No-Action projects to the existing 2012 baseline traffic volume network. These 31 No-Action projects include, but are not limited to, the sites included as part of the Astoria Rezoning, Phase I of the Cornell NYC Tech development, the Roosevelt Island Southtown:Main Street project, and the Halletts Point development.

#### Traffic Improvements

Operational changes at two analysis intersections are expected in the future as a result of the implementation of traffic mitigation measures proposed in the *Cornell NYC Tech FEIS* (2012) for its Phase I (2018 build year) development. These measures are assumed to be in place by the proposed project's 2023 Build Year, therefore they have been incorporated into the No-Action traffic analysis.

The traffic network analyzed for the No-Action condition also includes the mitigation measures that would be implemented at several of the <u>30</u> intersections analyzed in this chapter as part of the Halletts Point Rezoning project. In addition to signal timing changes, parking regulation changes, and lane restriping, these mitigation measures, which are described in detail in the Chapter 22, "Mitigation" of the *Halletts Point Rezoning FEIS* (2013), include installations of signals at four of the currently unsignalized intersections: 27<sup>th</sup> Avenue at 4<sup>th</sup> Street; 27<sup>th</sup> Avenue at 12<sup>th</sup> Street; 27<sup>th</sup> Avenue at 14<sup>th</sup> Street; and Astoria Boulevard at 18<sup>th</sup> Street. Table 13-17 presents a summary of the mitigation measures proposed for the *Cornell NYC Tech FEIS* and *Halletts Point Rezoning FEIS* at the study area intersections, which have been incorporated into the No-Action traffic analysis.

In addition, in conjunction with the No-Action as-of-right residential development on the project site's upland parcels, the currently unimproved and inaccessible portion of 26<sup>th</sup> Avenue is expected to be builtout in the future without the Proposed Action, thereby providing access to 9<sup>th</sup> Street. For the purposes of the traffic analysis, it is assumed that 26<sup>th</sup> Avenue would operate one-way eastbound with one travel lane and on-street parking on both sides. The resulting new intersection at 26<sup>th</sup> Avenue and 9<sup>th</sup> Street would be two-way stop controlled and is included in the detailed intersection capacity analyses for both the No-Action and With-Action conditions (analysis location A).

Since certification of the DEIS, NYCDOT proposed improvements for Astoria Boulevard between 33<sup>rd</sup> and 31<sup>st</sup> Streets as part of the Vision Zero initiative; the proposed improvements were reviewed and approved by Queens Community Board (CB) 1 in May 2014. Specifically, NYCDOT plans to restripe the lane markings at Astoria Boulevard and 31<sup>st</sup> Street, install a quick curb to separate the Astoria Boulevard North westbound and RFK exit ramp traffic, as well as installing a median extension to eliminate one lane from the Astoria Boulevard North westbound approach at 32<sup>nd</sup> Street. These measures are intended to simplify traffic patterns and sideswiping/collisions. The improvements will be implemented by the proposed project's 2020 Build Year. These planned improvements and the resultant traffic diversions have been incorporated into the future conditions analyses in consultation with NYCDOT.

It should also be noted that DCP's Transportation Division and the Queens Office are in the process of finalizing the Western Queens Transportation Study in coordination with the various City agencies, the MTA, local civic organizations, and members from Queens CB 1 and 2. The Western Queens Transportation Study aims to link existing and new development and improve access and mobility around them; establish connectivity to points of interest; and focus on bike, pedestrian, and transit improvements.

As the study includes recommendations and the timing of the implementation of any recommended improvement measures has not been determined, it is therefore not included in the quantitative traffic analysis provided below. However, a qualitative discussion of the potential implications of the Western Queens Transportation Study is included in Chapter 20, "Mitigation."

Intersection	Halletts Mitigation Measures	Cornell Mitigation Measures <sup>1</sup>
2. 27 <sup>th</sup> Avenue & 4 <sup>th</sup> Street	- Installing a traffic signal	
3. 27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street	<ul> <li>Daylighting 27<sup>th</sup> Avenue (AM, midday, and PM)</li> <li>Restripting (27<sup>th</sup> Avenue</li> <li>Modifying signal timing (AM only)</li> </ul>	
4. 27 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	- Installing a traffic signal	
5. 27 <sup>th</sup> Avenue & 14 <sup>th</sup> Street	- Installing a traffic signal	
6. 27 <sup>th</sup> Avenue & 18 <sup>th</sup> Street	- Installing a traffic signal	
7. Astoria Boulevard & 21 <sup>st</sup> Street	<ul> <li>Daylighting 21<sup>st</sup> Street (AM, midday, and PM)</li> <li>Restriping 21<sup>st</sup> Street</li> </ul>	- Modifying signal timing (AM, midday, and PM)
8. Astoria Boulevard & 23 <sup>rd</sup> Street	- Modifying signal timing (PM only)	
14. Astoria Boulevard & 31 <sup>st</sup> Street	<ul> <li>Daylighting Astoria Boulevard (AM, midday, and PM)</li> <li>Restriping Astoria Boulevard</li> </ul>	
15. Hoyt Avenue South/Astoria Boulevard & 33 <sup>rd</sup> Street	-Modifying signal timing (midday only)	
16. Hoyt Avenue North & 29 <sup>th</sup> Street	- Modifying signal timing (AM only)	
19. Astoria Boulevard & 8 <sup>th</sup> Street	<ul> <li>Restriping Astoria Boulevard</li> <li>Daylighting Astoria Boulevard (AM, midday, and PM)</li> <li>Modifying signal timing (AM and PM)</li> </ul>	
22. Vernon Boulevard & Welling Court/8 <sup>th</sup> Street	-Modifying signal timing (AM and midday)	
23. Astoria Boulevard & 18 <sup>th</sup> Street	-Installing a traffic signal	
24. Hoyt Avenue North & 21 <sup>st</sup> Street	- Modifying signal timing (midday and PM)	
25. Hoyt Avenue South/Astoria Park South & 21 <sup>st</sup> Street	- Modifying signal timing (AM and midday) -Daylighting (PM only)	- Modifying signal timing (AM only) - Restriping Hoyt Avenue South
28. Vernon Boulevard & Broadway/11 <sup>th</sup> Street	- Daylighting Broadway (AM and PM) -Modifying signal timing (midday only)	

Table 13-17	: No-Action	<b>Traffic</b>	Mitigation	Measures
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Notes:

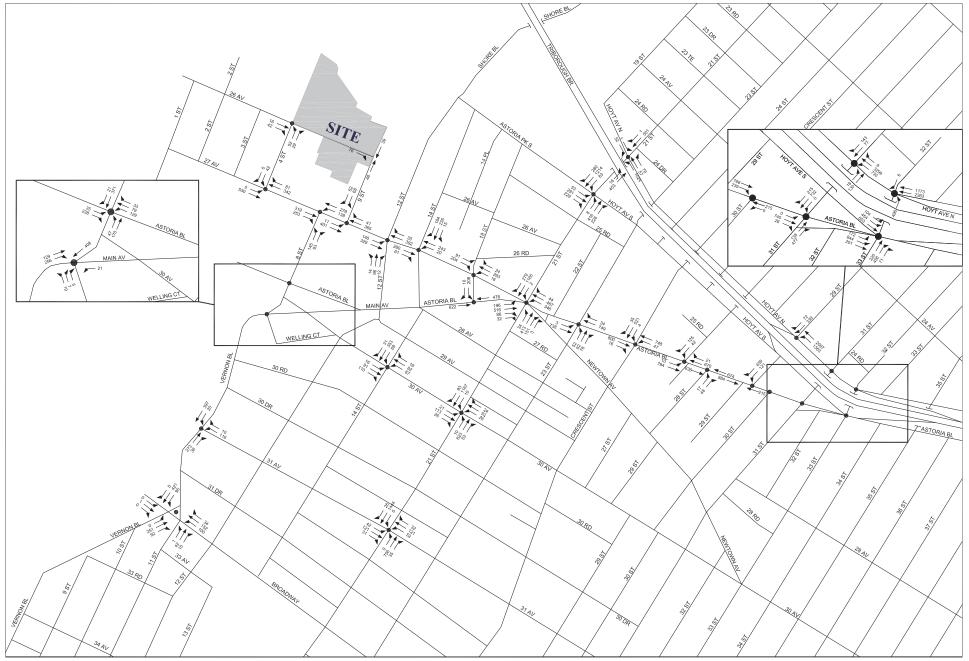
<sup>1</sup> Reflects only 2018 build year mitigation measures.

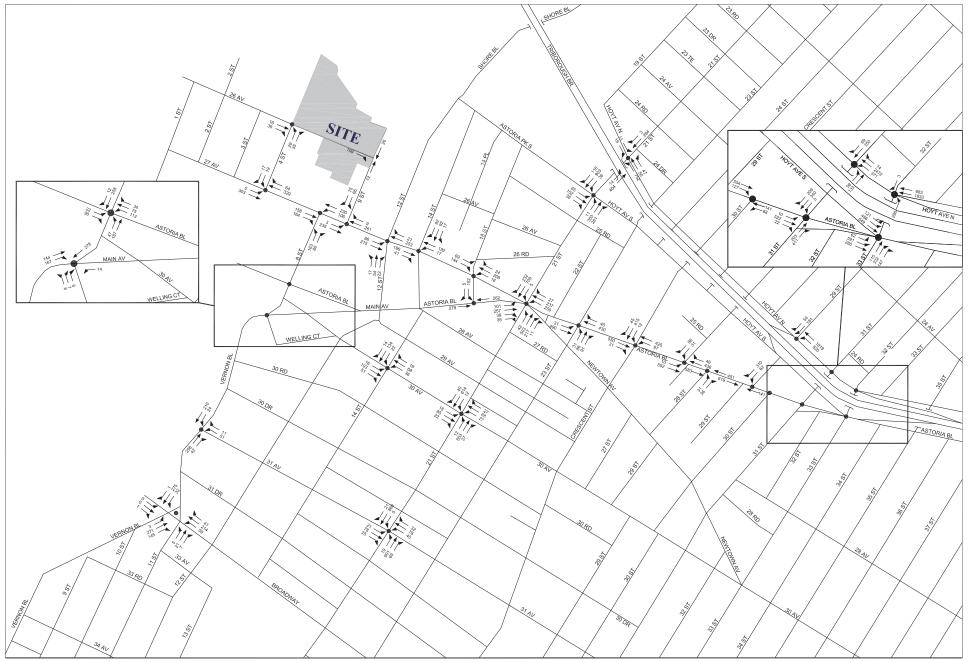
Sources: Halletts Point Rezoning FEIS (2013); Cornell NYC Tech FEIS (2012).

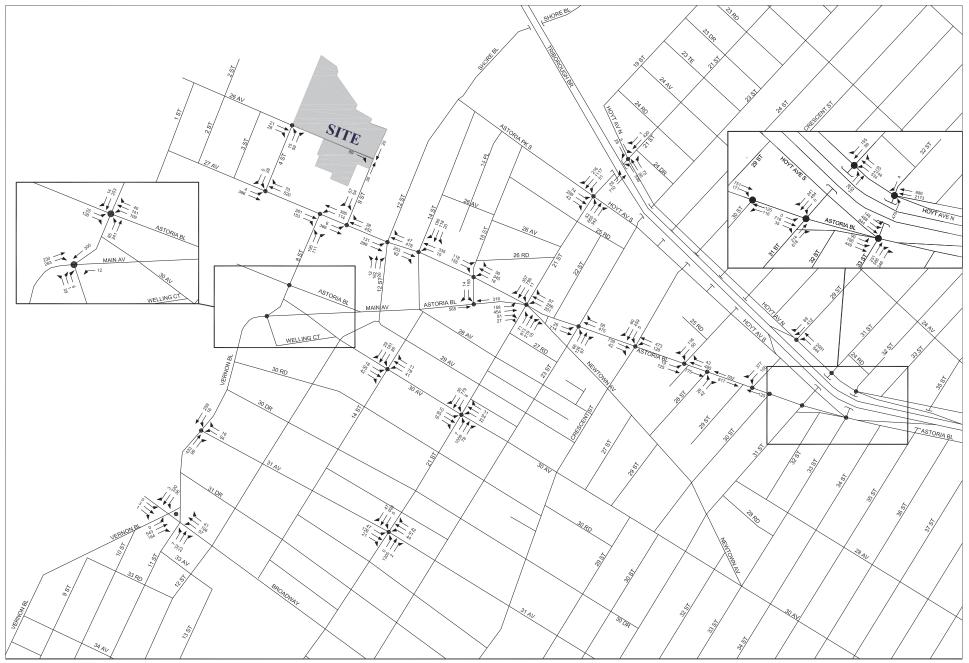
### <u>Weekday</u> Intersection Capacity Analysis

Figures 13-14, 13-15, and 13-16 show the expected No-Action weekday AM, midday, and PM peak hour traffic volumes, respectively. Table 13-18, below, shows a summary comparison of the individual lane group LOS for existing and future No-Action conditions.

As shown in Table 13-18, under the No-Action condition with the above-described traffic improvements in place, <u>five</u> individual traffic movements would operate at LOS E and <u>20</u> would operate at LOS F in the AM peak hour. During the midday peak hour, <u>two</u> individual traffic movements would operate at LOS E and <u>five</u> would operate at LOS F, while <u>three</u> and <u>14</u> individual traffic movements would operate at LOS E and LOS F, respectively, in the PM peak hour under the No-Action condition.







	Exist	ting Condi	tions	2023 No	-Action C	ondition
	Weekday	Weekday	Weekday	Weekday	Weekday	Weekday
	AM	Midday	PM	AM	Midday	PM
	Peak	Peak	Peak	Peak	Peak	Peak
	Hour	Hour	Hour	Hour	Hour	Hour
Overall LOS A/B/C	64	85	72	59	79	64
Overall LOS D	25	16	22	27	23	29
Overall LOS E	10	1	8	5	2	3
Overall LOS F	3	1	0	20	5	14
Number of						
movements at LOS	13	2	8	25	7	17
E or F						

 Table 13-18: Weekday Lane Group LOS Summary Comparison—Existing vs.

 No-Action Conditions

This table has been updated for the FEIS.

Table 13-19 shows the detailed v/c ratios, delays, and LOS by movement at the analyzed intersections in each peak hour under the No-Action condition and identifies those movements that would congested in one or more peak hours. As shown in Table 13-19, many of the movements that are congested under existing conditions would continue to operate at the same level of service with slight increases in v/c ratios and delays under the No-Action condition. The intersections where newly congested movements would occur under the No-Action condition or where the level of service of currently congested movements would degrade are discussed in the following.

### 27<sup>th</sup> Avenue & 8<sup>th</sup> Street:

- The westbound approach would deteriorate from LOS C under existing conditions to LOS F under the No-Action condition in the AM peak hour, and from LOS B to LOS F in both the midday and PM peak hours.

### Astoria Boulevard & 21<sup>st</sup> Street:

- The eastbound left-turn movement would deteriorate from LOS E under existing conditions to LOS F under the No-Action condition in the AM peak hour.
- The eastbound through/right movement would deteriorate from LOS D under existing conditions to LOS F under the No-Action condition in both the AM and PM peak hours.
- Both the westbound through/right movement and northbound approach would deteriorate from LOS D under existing conditions to LOS E under the No-Action condition in the PM peak hour.

### Astoria Boulevard & 23<sup>rd</sup> Street:

- The eastbound approach would deteriorate from LOS C under existing conditions to LOS F under the No-Action condition in the AM peak hour and from LOS C to LOS D in the PM peak hour.
- The westbound approach would deteriorate from and uncongested LOS C under existing conditions to a congested LOS C (v/c ratio greater than 0.90) under the No-Action condition in the AM peak hour.

### Astoria Boulevard & Crescent Street

- The eastbound approach would deteriorate from LOS C under existing conditions to LOS F under the No-Action condition in both the AM and PM peak hours.

		AM PE	AK HOUR	MIDDAY	PEAK HOUR	PM PEA	K HOUR
Interception		EXIS TING	NO-ACTION	EXIS TING	NO-ACTION	EXIS TING	NO-ACTION
Intersection	Lane	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS
	Group	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)
1. 26th Avenue & 4th Street	WB-LT	0.03 7.7 A		0.07 7.9 A		0.05 7.9 A	
(Unsignalized-Two Way Stop)	NB-LR	0.10 10.1 B	0.11 9.7 A	0.08 10.3 B	0.08 9.4 A	0.06 9.5 A	0.09 9.3 A
A. 26th Avenue & 9th Street (Unsignalized-Two Way Stop)	EB-R		0.09 8.9 A		0.13 8.9 A		0.10 8.8 A
2. 27th Avenue & 4th Street	EB-LT	NA 10.0 A	0.78 22.4 C	NA 9.6 A	0.45 14.1 B	NA 9.8 A	0.56 15.0 B
Existing Unsignalized-All Way Stop)	WB-T	NA 11.1 B	0.44 13.7 B	NA 10.4 B	0.43 13.1 B	NA 10.5 B	0.65 15.6 B
(No-Action Signalized)	WB-R	NA 7.9 A	0.25 12.2 B	NA 8.1 A	0.27 12.5 B	NA 8.0 A	0.29 11.8 B
	SB-LR	NA 9.8 A	0.10 20.4 C	NA 9.8 A	0.09 20.3 C	NA 9.5 A	0.08 21.6 C
3. 27th Avenue & 8th Street	EB-T		0.53 14.9 B		0.24 11.9 B		0.36 13.2 B
	EB-R		0.66 21.2 C		0.61 22.5 C		0.42 15.9 B
	EB-TR	0.59 18.5 B	17.4 B	0.54 17.2 B	17.2 B	0.48 15.6 B	14.1 B
	WB-LT	0.81 30.7 C	1.32 179.6 F	0.55 18.4 B	1.25 151.3 F *	0.41 14.9 B	1.22 138.6 F
	NB-L	0.41 24.5 C	0.52 28.4 C	0.30 22.3 C	0.36 23.3 C	0.33 22.9 C	0.48 25.8 C
	NB-R	0.26 22.0 C	0.57 34.6 C	0.28 22.4 C	0.73 47.7 D	0.30 22.6 C	0.75 47.4 D
4. 27th Avenue & 12th Street	EB-LT	0.07 8.6 A	0.64 9.9 A	0.05 8.0 A	0.47 11.2 B	0.08 8.4 A	0.54 8.2 A
Existing Unsignalized-Two Way Stop)	WB-TR		0.47 6.2 A		0.41 10.4 B		0.66 8.8 A
(No-Action Signalized)	NB-LTR	0.43 25.5 D	0.57 43.1 D	0.24 15.9 C	0.28 27.3 C	0.69 38.3 E *	0.86 65.8 E
5. 27th Avenue & 14th Street	EB-TR	NA 10.6 B	0.61 19.4 B	NA 9.2 A	0.33 11.5 B	NA 9.9 A	0.45 15.7 B
(Existing Unsignalized-All Way Stop)	WB-LT	NA 12.1 B	0.66 22.9 C	NA 9.0 A	0.29 11.0 B	NA 9.6 A	0.57 16.6 B
(No-Action Signalized)	SB-LTR	NA 16.8 C	0.89 41.0 D	NA 9.2 A	0.52 28.5 C	NA 10.5 B	0.79 36.0 D
6. 27th Avenue & 18th Street	EB-L	0.07 9.3 A	0.14 9.7 A	0.07 8.2 A	0.10 8.4 A	0.09 8.1 A	0.15 9.3 A
(Unsignalized-Two Way Stop)	WB-L	0.01 7.5 A	0.02 7.8 A	0.01 7.6 A	0.01 7.7 A	0.01 7.7 A	0.01 7.9 A
7. Astoria Boulevard & 21st Street	EB-L	0.82 59.3 E	* 1.20 156.4 F *	0.25 34.6 C	0.33 36.9 D	0.45 41.9 D	0.61 46.8 D
	EB-TR	0.82 52.5 D	1.70 365.9 F <sup>3</sup>	0.38 36.1 D	0.61 41.5 D	0.75 47.7 D	1.13 118.0 F
	WB-L	0.95 57.8 E	* 1.01 69.0 E *	0.81 49.3 D	0.86 53.2 D	0.83 58.3 E *	0.92 68.3 E
	WB-TR	0.72 42.7 D	0.82 45.2 D	0.36 35.0 D	0.46 36.4 D	0.69 48.1 D	0.99 73.3 E
	NB-LT		0.72 31.8 C		0.80 38.4 D		1.11 85.3 F
	NB-R		0.37 24.7 C		0.65 36.1 D		0.44 22.9 C
	NB-LTR	0.80 35.7 D	30.0 C	1.05 69.9 E *	37.7 D	1.02 46.2 D *	72.4 E
	SB-LT		0.87 31.3 C		0.78 38.5 D		0.78 30.0 C
	SB-R		0.59 26.9 C		0.75 39.7 D		0.80 33.1 C
	SB-LTR	1.05 60.8 E	* 30.4 C	0.97 49.1 D *	38.8 D	0.87 34.4 C	30.9 C
3. Astoria Boulevard & 23rd Street	EB-LT	0.64 20.1 C	1.21 127.5 F	0.61 16.5 B	0.81 23.1 C	0.69 21.1 C	0.95 35.5 D
	WB-TR	0.81 24.4 C	0.91 29.7 C	0.66 15.3 B	0.77 17.4 B	0.63 18.4 B	0.84 22.7 C
	NB-LTR	0.48 33.0 C	0.50 33.5 C	0.53 27.8 C	0.56 28.5 C	0.57 35.3 D	0.61 37.4 D

### Table 13-19: 2023 Future Weekday No-Action Condition–LOS at Analyzed Intersections

				AM PEA	K HOUR				M	IIDDAY P	EAK HOU	R		PM PEAK HOUR					
Intersection	[	EX	AIS TIN	G	NC	)-ACTIO	DN	E	XIS TIN	G	NO	-ACTIO	N	E	XIS TIN	G	NO	-ACTIO	)N
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
9. Astoria Boulevard & Crescent Street	EB-TR	0.72	24.0	С	1.28	159.6	F *	0.63	17.3	В	0.83	25.1	С	0.82	27.9	С	1.11	88.2	F
	WB-LT	0.86	27.5	С	1.24	139.4	F *	0.98	31.1	С *	1.27	143.1	F *	0.99	38.6	D *	1.53	267.6	F
	SB-LTR	1.05	66.5	E *	1.20	130.1	F *	1.03	54.2	D *	1.17	110.1	F *	1.00	50.7	D *	1.13	99.3	F
10. Astoria Boulevard & 27th Street	EB-LT	0.54	15.2	В	0.96	38.2	D *	0.44	13.6	В	0.59	16.2	В	0.57	15.7	В	0.79	22.1	С
	WB-TR	0.76	19.6	В	0.84	23.0	С	0.62	16.3	В	0.71	18.3	В	0.52	14.3	В	0.65	16.8	В
	SB-LR	0.75	38.8	D	0.83	41.1	D	0.47	34.1	С	0.53	34.9	С	0.71	38.0	D	0.88	42.7	D
11. Astoria Boulevard & 28th Street (Unsignalized-Two Way Stop)	NB-LR	0.32	20.8	С	0.70	68.0	F *	0.30	18.9	С	0.42	28.3	D	0.25	17.4	С	0.41	30.1	D
12. Astoria Boulevard & 29th Street	EB-T	0.97	65.6	E *	1.63	328.2	F *	0.75	24.9	С	0.97	48.8	D *	0.97	58.4	E *	1.30	179.5	F
	WB-T	0.42	27.1	С	0.44	27.5	С	0.22	13.4	В	0.23	13.5	В	0.21	20.2	С	0.22	20.3	С
	SB-L	0.17	16.9	В	0.18	17.0	В	0.12	18.0	В	0.12	18.1	В	0.16	19.5	В	0.16	19.5	В
	SB-R	0.65	26.9	С	0.75	31.3	С	0.58	26.2	С	0.70	30.5	С	0.48	25.1	С	0.66	30.4	С
13. Astoria Boulevard & 30th Street (Unsignalized-Two Way Stop)	WB-LT	0.26	11.3	В	0.00	12.9	В	0.08	9.2	А	0.10	10.1	В	0.17	10.4	В	0.23	12.6	В
14. Astoria Boulevard & 31st Street	EB-LTR	0.79	37.7	D	0.83	37.5	D	0.85	31.7	С	0.57	22.4	С	0.96	46.4	D *	0.75	34.8	С
	NB-T	0.49	41.2	D	0.52	41.8	D	0.51	33.2	С	0.54	33.7	С	0.49	41.0	D	0.52	41.6	D
	NB-R	0.63	15.3	В	0.67	16.5	В	0.50	8.5	А	0.53	8.9	А	0.79	21.4	С	0.84	24.2	С
	SB-T	0.86	31.4	С	0.99	51.0	D *	0.62	19.1	В	0.55	17.7	В	0.67	21.8	С	0.63	20.8	С
	SB-R	0.53	19.0	В	0.30	14.9	В	0.29	14.1	В	0.31	14.3	В	0.30	14.9	В	0.31	15.1	В
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	0.91	50.4	D *	1.32	192.2	F *	0.92	44.5	D *	1.02	62.4	E *	1.05	73.9	E *	1.17	121.1	F
33rd Street	NB-TR	1.05	77.0	E *	1.09	91.5	F *	0.77	37.3	D	0.76	36.6	D	1.05	69.4	E *	1.07	77.7	Е
	NB-R	1.04	77.9	E *	1.09	97.7	F *	0.76	40.7	D	0.87	49.3	D	1.04	69.9	E *	1.13	108.5	F
	Hoyt Ave (EB-LT)	0.54	25.6	С	0.63	27.1	С	0.67	26.7	С	0.78	30.4	С	0.73	35.1	D	0.87	41.3	D
16. Hoyt Ave N. & 29th Street	WB-L	0.71	11.6	В	0.80	14.6	В	0.54	11.5	В	0.57	12.0	В	0.41	12.3	В	0.45	12.7	В
	WB-LT	0.71	11.3	В	0.94	19.4	В *	0.50	10.8	В	0.68	13.2	В	0.56	14.1	В	0.86	21.6	С
	SB-R	0.99	90.5	F *	1.03	98.5	F *	0.49	34.5	С	0.53	35.5	D	0.78	49.8	D	0.85	54.2	D
17. Hoyt Ave N. & 31st Street	WB-L	1.02	87.8	F *	0.81	37.5	D	1.01	83.2	F *	0.71	36.5	D	0.42	16.0	В	0.34	15.0	В
	WB-T	0.90	21.6	C *	1.15	91.2	F *	0.71	17.2	В	0.93	26.6	C *	0.68	20.1	С	0.99	40.1	D
	WB-R	0.31	10.2	В	0.02	7.5	А	0.61	19.6	В	0.18	11.6	В	0.65	23.6	С	0.15	13.3	В
	NB-DefL	-	-	-	-	-	-	0.50	29.3	С	0.66	40.3	D	-	-	-	-	-	-
	NB-T	-	-	-	-	-	-	0.22	21.1	С	0.23	21.2	С	-	-	-	- 1	-	-
	NB-LT	0.28	35.6	D	0.32	36.4	D	-	-	-	-	-	-	0.28	28.1	С	0.29	28.3	С
	SB-T	0.26	36.0	D	0.62	44.5	D	0.44	24.1	С	0.59	27.2	С	0.15	26.5	С	0.25	28.1	С
	SB-R	0.69	53.7	D	0.74	57.8	E *	0.24	21.9	С	0.26	22.2	С	0.46	33.6	С	0.49	34.6	С

### Table 13-19 (continued): 2023 Future Weekday No-Action Condition–LOS at Analyzed Intersections

				AM PEA	K HOUR				N	IIDDAY I	PEAK HOU	R				PM PEA	K HOUR		
Intersection		EX	AIS TIN	G	NO	)-ACTIO	DN	E	XIS TIN	G	NO	-ACTIO	ON	E	XIS TIN	G	NO	-ACTIO	ON
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.51	8.6	А	0.74	13.3	В	0.35	7.8	А	0.51	9.7	А	0.31	9.1	А	0.46	10.9	В
	WB(Ramp)-T	1.05	81.1	F *	1.17	127.2	F *	0.92	22.0	C *	1.03	45.5	D *	0.89	23.5	С	1.13	84.7	F
	NB-L	0.56	43.7	D	0.65	45.2	D	0.33	28.5	С	0.32	28.4	С	0.50	38.4	D	0.52	38.6	D
	SB-R	0.03	38.0	D	0.03	38.0	D	0.02	25.9	С	0.02	25.9	С	0.02	33.3	С	0.02	33.3	С
19. Astoria Boulevard & 8th Street	EB-L	-	-	-	0.16	24.6	С	-	-	-	0.09	26.1	С	-	-	-	0.17	29.0	С
	EB-R	-	-	-	0.77	44.4	D	-	-	-	0.27	29.0	С	-	-	-	0.66	40.6	D
	EB-LR	0.25	28.5	С		41.4	D	0.12	26.4	С		28.4	С	0.26	28.6	С		39.1	D
	WB-L	0.26	28.5	С	0.32	26.9	С	0.25	28.5	С	0.36	30.6	С	0.16	27.0	С	0.31	31.0	С
	WB-TR	0.20	27.7	С	0.34	27.3	С	0.15	27.0	С	0.34	30.3	С	0.15	26.9	С	0.50	35.3	D
	NB-LT	0.34	15.1	В	0.52	20.2	С	0.31	14.8	В	0.46	17.2	В	0.40	15.5	В	0.87	27.7	С
	SB-TR	0.50	17.9	В	0.74	27.0	С	0.31	15.1	В	0.40	16.3	В	0.29	14.8	В	0.39	15.1	В
20. 30th Avenue & 14th Street	EB-LTR	NA	11.5	В	NA	13.0	В	NA	8.7	А	NA	9.1	А	NA	9.1	А	NA	9.6	А
(Unsignalized-All Way Stop)	WB-LTR	NA	12.3	В	NA	13.4	В	NA	8.7	А	NA	9.1	А	NA	9.0	А	NA	9.5	А
	SB-LTR	NA	22.3	С	NA	28.5	D	NA	9.2	А	NA	9.5	А	NA	10.6	В	NA	11.4	В
21. 30th Avenue & 21st Street	EB-LTR	0.41	36.1	D	0.52	39.0	D	0.30	33.5	С	0.35	34.5	С	0.32	33.9	С	0.37	35.1	D
	WB-LTR	0.43	36.7	D	0.48	38.0	D	0.33	34.2	С	0.39	35.6	D	0.41	36.2	D	0.50	38.8	D
	NB-LTR	0.47	13.9	В	0.53	15.0	В	0.48	14.1	В	0.53	14.9	В	0.71	19.1	В	0.78	21.7	С
	SB-LTR	0.69	18.1	В	0.76	20.3	С	0.37	12.4	В	0.43	13.1	В	0.42	13.1	В	0.49	14.0	В
22. Vernon Boulevard & Welling Court/	EB-LT	0.96	47.1	D *	1.18	116.5	F *	0.79	37.7	D	0.91	45.7	D *	1.04	66.2	E *	1.43	229.6	F
8th Street	WB-TR	0.03	21.0	С	0.04	21.1	С	0.03	21.0	С	0.04	21.1	С	0.04	21.1	С	0.06	21.3	С
	NB-LTR	0.24	31.2	С	0.33	36.1	D	0.14	28.9	С	0.17	31.0	С	0.08	28.2	С	0.18	29.5	С
	SB-R	0.73	36.2	D	1.01	68.7	E *	0.55	31.3	С	0.71	35.1	D	0.47	29.5	С	0.72	37.9	D
23. Astoria Boulevard & 18th Street	EB-T	-	-	-	0.91	39.6	D *	-	-	-	0.41	23.1	С	-	-	-	0.76	31.5	С
(Existing Unsignalized-Two Way Stop)	WB-T	-	-	-	0.66	27.1	С	-	-	-	0.41	22.9	С	-	-	-	0.44	22.2	С
(No-Action Signalized)	SB-LR	0.30	20.8	С	0.46	25.0	С	0.20	12.7	В	0.32	22.1	С	0.21	14.3	В	0.32	22.0	С
24. Hoyt Avenue N. & 21st Street	EB-L	0.02	40.4	D	0.02	40.4	D	0.11	42.0	D	0.12	44.0	D	0.09	41.7	D	0.11	43.9	D
	EB-R	0.36	47.1	D	0.37	47.5	D	0.13	42.3	D	0.15	44.5	D	0.17	43.0	D	0.19	45.3	D
	WB-L	0.89	43.3	D	1.09	88.0	F *	0.67	38.0	D	0.83	42.3	D	0.59	36.4	D	0.98	62.2	Е
	WB-TR	0.24	14.7	В	0.25	14.8	В	0.16	14.1	В	0.17	14.2	В	0.27	15.5	В	0.30	16.9	В
	NB-L	0.27	30.4	С	0.31	32.3	С	0.10	25.1	С	0.12	25.4	С	0.16	25.8	С	0.17	24.7	С
	NB-T	1.00	75.1	E *	1.20	143.8	F *	0.74	41.1	D	0.81	46.3	D	1.05	78.2	E *	1.12	99.0	F
	SB-TR	0.97	47.2	D *	1.04	65.0	E *	0.55	32.7	С	0.60	34.1	С	0.73	37.6	D	0.77	37.9	D

### Table 13-19 (continued): 2023 Future Weekday No-Action Condition–LOS at Analyzed Intersections

				AM PEA	K HOUR				Μ	IDDAY I	PEAK HOU	J <b>R</b>				PM PEA	K HOUR		
Intersection		E	XIS TIN	G	NO	)-ACTIO	DN	E	XIS TIN	G	NC	)-ACTIO	ON	E	XIS TIN	G	NO	-ACTI	ON
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
25. Hoyt Avenue S./Astoria Park S. &	EB-L	0.12	29.9	С	-	-	-	0.21	31.5	С	-	-	-	0.17	30.7	С	-	-	-
21st Street	EB-TR	1.02	61.1	Е *	-	-	-	0.40	35.3	D	- 1	-	-	0.73	43.2	D	-	-	-
	EB-LTR	-	-	-	0.84	41.9	D	-	-	-	0.36	32.0	С	-	-	-	0.58	37.9	D
	NB-LT	-	-	-	-	-	-	-	-	-	- 1	-	-	-	-	-	0.72	16.9	В
	NB-R	-	-	-	-	-	-	-	-	-	- I	-	-	-	-	-	0.51	13.3	В
	NB-LTR	0.52	14.6	В	0.61	14.3	В	0.41	13.1	В	0.48	15.0	В	0.86	22.5	С		15.7	В
	SB-LTR	0.98	33.2	C *	1.12	81.1	F *	0.59	15.5	В	0.74	20.2	С	0.84	23.6	С	1.00	40.4	D
26. 27th Avenue & 9th Street	EB-LT	0.01	8.2	А	0.02	8.5	А	0.00	7.7	А	0.01	8.1	А	0.01	7.8	А	0.01	8.8	А
Unsignalized-Two Way Stop)	SB-LR	0.11	12.0	В	0.56	29.6	D	0.07	10.0	А	0.43	15.9	С	0.04	9.7	А	0.60	31.2	D
27. Vernon Boulevard & 31st Avenue	WB-LR	0.49	23.5	С	0.66	38.2	E *	0.20	15.0	В	0.25	17.7	С	0.37	19.8	С	0.51	29.2	D
Unsignalized-T wo Way Stop)	SB-LT	0.02	8.1	А	0.02	8.3	А	0.03	7.9	А	0.03	8.1	А	0.02	8.4	А	0.02	8.9	А
28. Vernon Boulevard & Broadway/11th Street	EB-LTR	0.01	28.2	С	0.01	28.2	С	0.02	26.1	С	0.02	25.4	С	0.03	33.2	С	0.03	33.2	С
	WB-LT	-	-	-	0.87	38.9	D	-	-	-	-	-	-	-	-	-	0.77	47.0	D
	WB-R	-	-	-	0.21	29.9	С	-	-	-	-	-	-	-	-	-	0.24	35.8	D
	WB-LTR	1.01	56.0	Е *		37.7	D	0.86	43.8	D	0.96	55.5	E *	0.82	50.8	D		45.1	D
	NB (Vernon Blvd)-LT	0.24	7.8	А	0.28	8.2	А	0.25	8.2	А	0.29	9.0	А	0.44	9.0	А	0.52	10.1	в
	NB (Vernon Blvd)-R	0.04	6.4	А	0.11	6.8	А	0.16	7.5	А	0.21	8.3	А	0.12	6.3	А	0.18	6.7	А
	NB (11th Street)-LTR	0.36	40.8	D	0.38	41.1	D	0.21	32.8	С	0.22	32.8	С	0.32	38.0	D	0.33	38.2	D
	SB-LTR	0.96	45.8	D *	1.36	195.9	F *	0.51	26.2	С	0.67	31.5	С	0.57	28.0	С	0.88	45.4	D
29. 31st Avenue & 21st Street	EB-LTR	0.64	43.9	D	0.67	45.6	D	0.33	34.2	С	0.34	34.5	С	0.48	34.4	С	0.50	35.0	D
	WB-LTR	0.56	40.0	D	0.58	41.1	D	0.40	35.5	D	0.42	35.9	D	0.40	32.0	С	0.42	32.4	С
	NB-TR	0.43	13.2	В	0.50	14.2	В	0.58	15.6	В	0.64	17.0	В	0.69	20.8	С	0.79	24.2	С
	SB-TR	0.78	20.7	С	0.90	27.9	C *	0.50	14.4	В	0.58	15.7	В	0.57	18.1	В	0.67	20.3	С

#### Table 13-19 (continued): 2023 Future Weekday No-Action Condition-LOS at Analyzed Intersections

#### Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9) Analysis is based on the 2010 *Highway Capacity Manual* methodology (HCS+, version 5.5) *This table has been updated for the FEIS.* 

- The westbound approach would deteriorate from LOS C under existing conditions to LOS F under the No-Action condition in both the AM and midday peak hours and from LOS D to LOS F in the PM peak hour.
- The southbound approach would deteriorate from LOS E under existing conditions to LOS F under the No-Action condition in the AM peak hour and from LOS D to LOS <u>F</u> in both the midday and PM peak hours.

Astoria Boulevard & 27<sup>th</sup> Street

- The eastbound approach would deteriorate from LOS B under existing conditions to LOS D under the No-Action condition in the AM peak hour.

Astoria Boulevard & 28<sup>th</sup> Street (unsignalized)

- The northbound approach would deteriorate from LOS C under existing conditions to LOS F under the No-Action condition in the AM peak hour.

### Astoria Boulevard & 29th Street

- The eastbound approach would deteriorate from LOS E under existing conditions to LOS F under the No-Action condition in both the AM and PM peak hours and from LOS C to LOS D in the midday peak hour.

### Astoria Boulevard & 31<sup>st</sup> Street

- The southbound through-movement would deteriorate from LOS C under existing conditions to LOS D under the No-Action condition in the AM peak hour.

### Hoyt Avenue South/Astoria Boulevard & 33<sup>rd</sup> Street

- The eastbound approach would deteriorate from LOS D under existing conditions to LOS F under the No-Action condition in the AM peak hour, from LOS D to LOS E in the midday peak hour, and from LOS E to LOS F in the PM peak hour.
- <u>The northbound right-turn movements would deteriorate from LOS E under existing conditions to LOS F under the No-Action condition in both the AM and PM peak hours.</u>
- <u>The northbound through/right movement would deteriorate from LOS E under existing conditions</u> to LOS F in the AM peak hour.

Hoyt Avenue North & 31st Street

- The westbound through movement would deteriorate from LOS C under existing conditions to LOS <u>F</u>under the No-Action condition in the AM peak hour, from LOS B to LOS C in the midday peak hour, and from LOS C (with a v/c ratio of 0.68) to LOS C (with a v/c ratio of 0.99) in the PM peak hour.
- The southbound right-turn movement would deteriorate from LOS D under existing conditions to LOS E under the No-Action condition in the AM peak hour.

### Astoria Boulevard & 32<sup>nd</sup> Street:

- The westbound through movement at the ramp would deteriorate from LOS C under existing conditions to LOS D under the No-Action condition in the midday peak hour and from LOS C to LOS F in the PM peak hour.

### *Vernon Boulevard & Welling Court/8<sup>th</sup> Street*

- The eastbound approach would deteriorate from LOS D under existing conditions to LOS F under the No-Action condition in the AM peak hour, from an uncongested LOS D to a congested LOS

D (delay greater than 45 seconds) in the midday peak hour, and from LOS E to LOS F in the PM peak hour.

- The southbound approach would deteriorate from LOS D under existing conditions to LOS E under the No-Action condition in the AM peak hour.

Astoria Boulevard & 18<sup>th</sup> Street:

- The eastbound approach would operate at LOS D at a v/c ratio of 0.91 in the AM peak hour under the No-Action condition.

Hoyt Avenue North & 21<sup>st</sup> Street

- The westbound left-turn movement would deteriorate from LOS D under existing conditions to LOS F under the No-Action conditions in the AM peak hour and from LOS D under existing conditions to LOS E under the No-Action condition in the PM peak hour.
- The northbound through movement would deteriorate from LOS E under existing conditions to LOS F under the No-Action condition in both the AM and PM peak hours.
- The southbound approach would deteriorate from LOS D under existing conditions to LOS E under the No-Action condition in the AM peak hour.

Hoyt Avenue South/Astoria Park South & 21st Street

- The southbound approach would deteriorate from LOS C under existing conditions to LOS  $\underline{F}$  under the No-Action condition in the AM peak hour and from LOS C to LOS D in the PM peak hour.

Vernon Boulevard & 31<sup>st</sup> Street

- The westbound approach would deteriorate from LOS C under existing conditions to LOS E under the No-Action condition in the AM peak hour.

*Vernon Boulevard & Broadway/11<sup>th</sup> Street* 

- The westbound approach would deteriorate from LOS D under existing conditions to LOS E under the No-Action condition in the midday peak hour.
- The southbound approach would deteriorate from LOS D under existing conditions to LOS F under the No-Action condition in the AM peak hour.

31<sup>st</sup> Avenue & 21<sup>st</sup> Street

- <u>The southbound approach would deteriorate from LOS C (with a v/c ratio of 0.78) under existing</u> <u>conditions to LOS C (with a v/c ratio of 0.90) under the No-Action condition in the AM peak</u> <u>hour.</u>

### Future with the Proposed Action (With-Action Condition)

As discussed earlier, under the transportation RWCDS, the Proposed Action would result in the development of approximately 1,668 residential units, 84,470 sf of local retail, a 25,000 sf supermarket and a site for a public elementary school with 456 seats. 900 accessory off-street parking spaces would also be provided to accommodate project-generated parking demand. The Proposed Action is anticipated to be completed in 2023. As discussed above in Section E, "Level 2 Screening Assessment," the Proposed Action is expected to generate a total of 534, 365, and 633 net vehicle trips in the <u>weekday</u> AM, midday, and PM peak hours, respectively. The assignments of the projected vehicle trip increments generated during these peak hours are shown in Figures 13-2, 13-3, and 13-4, respectively. Proposed changes to the

roadway network and traffic circulation improvements as well as the effect that the Proposed Action would have on traffic operations, are discussed in the following.

### Proposed Roadway Network and Traffic Circulation Improvements

As noted in Chapter 1, "Project Description" and as shown in Figure 1-4 in Chapter 1, the Proposed Action includes changes to the street network to better facilitate access to the project site. As discussed above, under the 2023 No-Action condition, <u>it is assumed that 26<sup>th</sup> Avenue would</u> be built-out and extend to 9<sup>th</sup> Street, operating eastbound one-way between 4<sup>th</sup> and 9<sup>th</sup> Streets. This configuration would not change with the Proposed Action. However, the Proposed Action includes layby lanes for drop-off/pick-ups and parking along the south side of 26<sup>th</sup> Avenue between 4<sup>th</sup> and 9<sup>th</sup> Streets. In addition, 4<sup>th</sup> Street would be extended north to the waterfront and its northern end would be connected to 9<sup>th</sup> Street's northern terminus by a public access easement that would allow for vehicles to travel one-way eastbound from 4<sup>th</sup> Street to 9<sup>th</sup> Street. It should be noted that with the extension of 4<sup>th</sup> Street, the stop control at the intersection of 26<sup>th</sup> Avenue and 4<sup>th</sup> Street would be modified. While operating as a T-intersection with a two-way stop control and 26<sup>th</sup> Avenue as the major road under existing conditions, the new four-legged intersection would operate with an all-way stop control in the 2023 With-Action condition.<sup>2</sup>

### <u>Weekday</u> Intersection Capacity Analysis

Figures 13-17, 13-18, and 13-19 show the traffic network volumes under the With-Action condition for the weekday AM, midday, and PM peak hours, respectively. The volumes shown are the sum of the net incremental traffic generated by the Proposed Action and the No-Action traffic network.

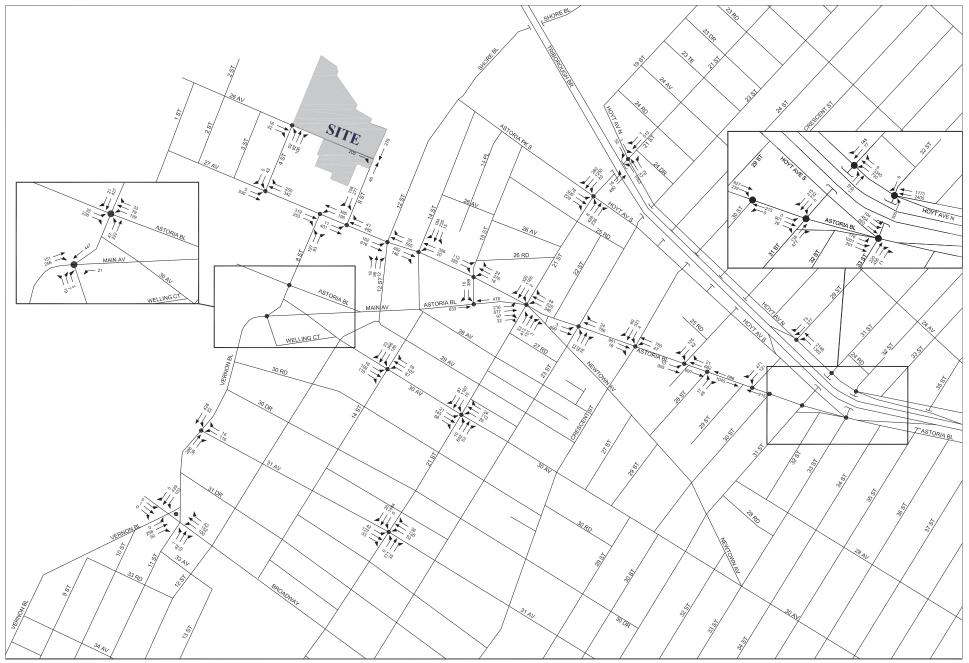
Table 13-20 shows a summary comparison of the individual lane group LOS for future No-Action and With-Action conditions. As shown in Table 13-20, five individual traffic movements would operate at LOS E and <u>26</u> would operate at LOS F in the <u>weekday</u> AM peak hour under the With-Action condition. During the <u>weekday</u> midday peak hour, three individual traffic movements would operate at LOS E and <u>five</u> would operate at LOS F, while <u>12</u> and <u>16</u> individual traffic movements would operate at LOS E and LOS F, respectively, in the <u>weekday</u> PM peak hour under the With-Action condition.

Table 13-21 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in each <u>weekday</u> peak hour under the With-Action condition and identifies those movements that are considered impacted in one or more peak hours. As shown in Table 13-21, one or more approaches or lane groups at a total of <u>23</u> of the 30 analyzed intersections would experience significant adverse impacts in one or more peak hour, as a result of the Proposed Action. <u>21</u> intersections would experience significant adverse impacts in the <u>weekday</u> AM peak hour, nine intersections would experience significant adverse impacts in the <u>weekday</u> midday peak hour, while <u>17</u> intersections would experience significant adverse impacts in the <u>weekday</u> PM peak hour, as shown earlier in more detail in Table 13-1. Potential measures to mitigate these significant adverse impacts are discussed in Chapter 20, "Mitigation."

#### Alternate Traffic Impact Analysis without Halletts Point Development

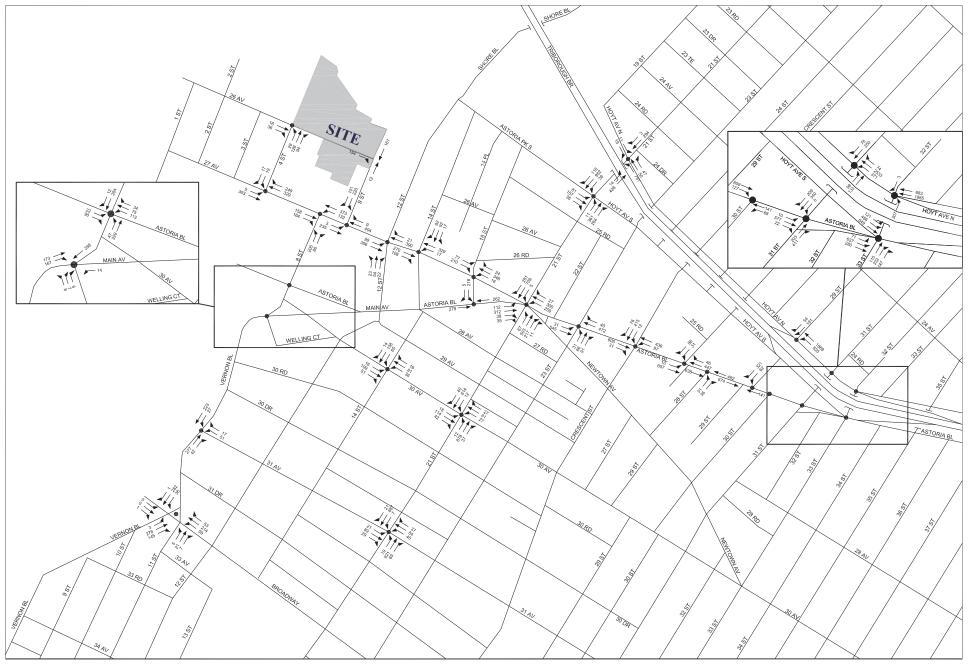
As the traffic study area would experience increased volumes due to both the Proposed Action and the Halletts Point Rezoning project, an additional analysis was conducted to determine whether the impacts disclosed in Table 13-21 would also occur absent the Halletts Point development. It should be noted that for this alternate analysis neither the traffic volumes generated by the Halletts Point development nor the

<sup>&</sup>lt;sup>2</sup> A preliminary all-way stop control warrant was prepared for the subject intersection in accordance with Section 2B.07 of the *Manual on Uniform Traffic Control Devices (MUTCD)* and determined that future With-Action traffic conditions would warrant the installation of an all-way stop control. The warrant study <u>was</u> reviewed <u>and approved by NYCDOT</u>.



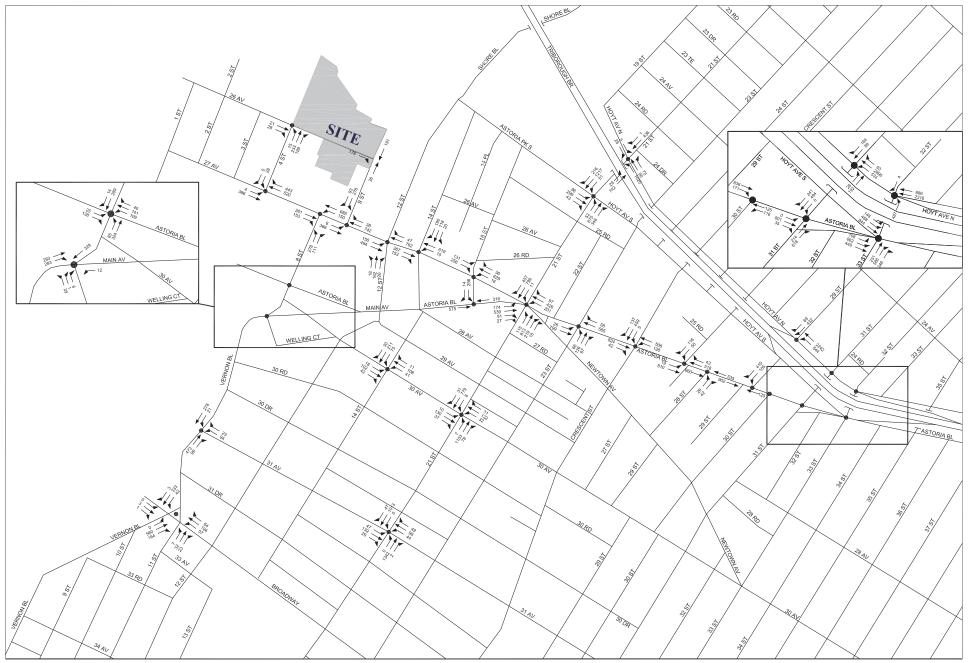
Analyzed Locations

### Astoria Cove



Analyzed Locations

# Astoria Cove



mitigation measures identified in the 2013 *Halletts Point Rezoning FEIS* and listed in Table 13-17 were accounted for. All other assumptions used to develop the future traffic networks are the same as discussed above.

	2023 No	-Action Co	ondition	2023 Wit	h-Action (	Condition
	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour
Overall LOS A/B/C	59	79	64	52	77	58
Overall LOS D	27	23	29	28	26	27
Overall LOS E	5	2	3	5	3	12
Overall LOS F	20	5	14	26	5	16
Number of intersections with significant adverse impacts				21	9	17
No. of movements at LOS E or F	25	7	17	31	8	28

Table 13-20: Weekday Lane Group LOS Summary Comparison—No-Action vs.
With-Action Conditions

This table has been updated for the FEIS.

### Alternate No-Action Condition <u>Weekday</u> Intersection Capacity Analysis

Figures 13-20, 13-21, and 13-22 show the expected weekday AM, midday, and PM peak hour traffic volumes for <u>the</u> alternate No-Action condition without the Halletts Point development. Table 13-22 below shows a summary comparison of the individual lane group LOS for existing and alternate future No-Action conditions. As shown in Table 13-22, <u>nine</u> individual traffic movements would operate at LOS E and <u>13</u> would operate at LOS F in the <u>weekday</u> AM peak hour under the alternate No-Action condition. During the <u>weekday</u> midday peak hour, <u>three</u> individual traffic movements would operate at LOS E and <u>three</u> would operate at LOS F, while <u>five</u> and ten individual traffic movements would operate at LOS E and LOS F, respectively, in the <u>weekday</u> PM peak hour under the alternate No-Action condition.

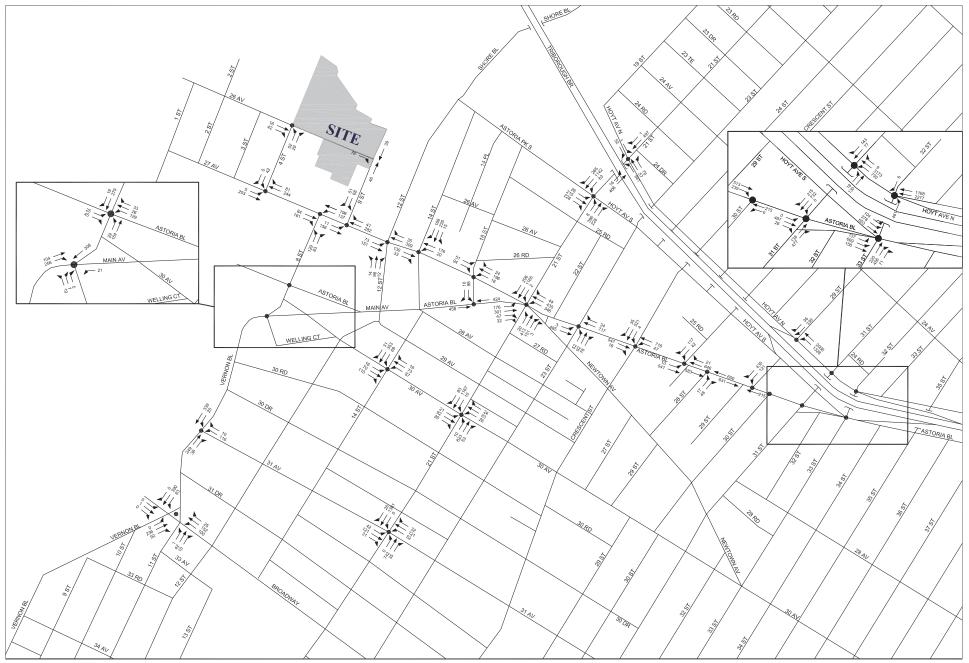
Table 13-23 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in each peak hour under the alternate No-Action condition and identifies those movements that would congested in one or more peak hour. As shown in Table 13-23, many of the movements that are congested under existing conditions would continue to operate at the same level of service with slight increases in v/c ratios and delays under the alternate No-Action condition. The intersections where newly congested movements would occur under the alternate No-Action condition or where the level of service of currently congested movements would degrade are discussed in the following.

### $27^{th}$ Avenue & $8^{th}$ Street:

- In the AM peak hour, the westbound approach would deteriorate from LOS C under existing conditions to LOS E under the alternate No-Action condition.

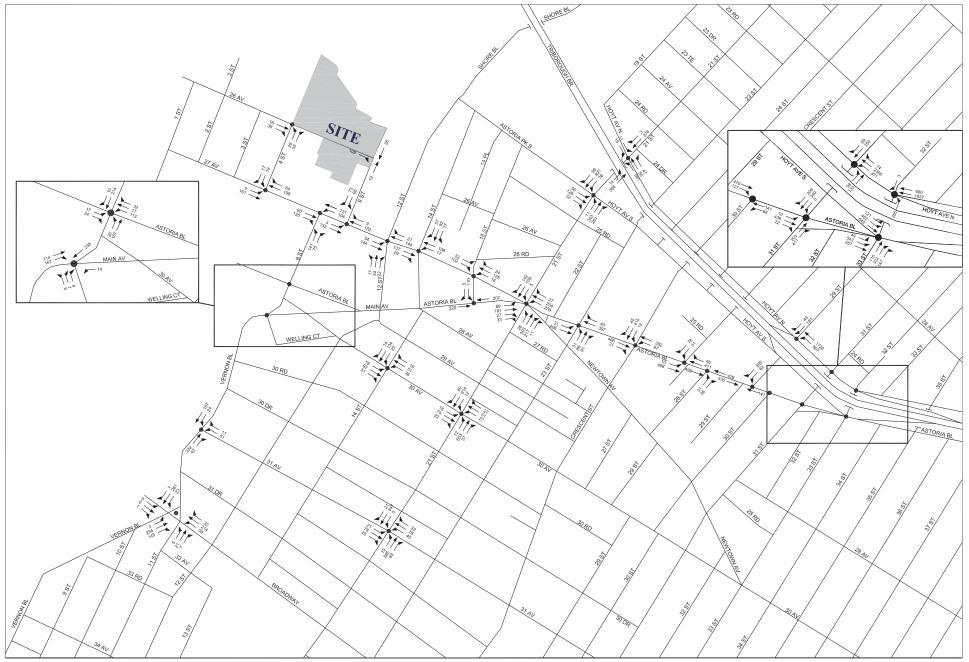
### 27<sup>th</sup> Avenue & 12<sup>th</sup> Street (unsignalized):

In the PM peak hour, the northbound approach would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition.



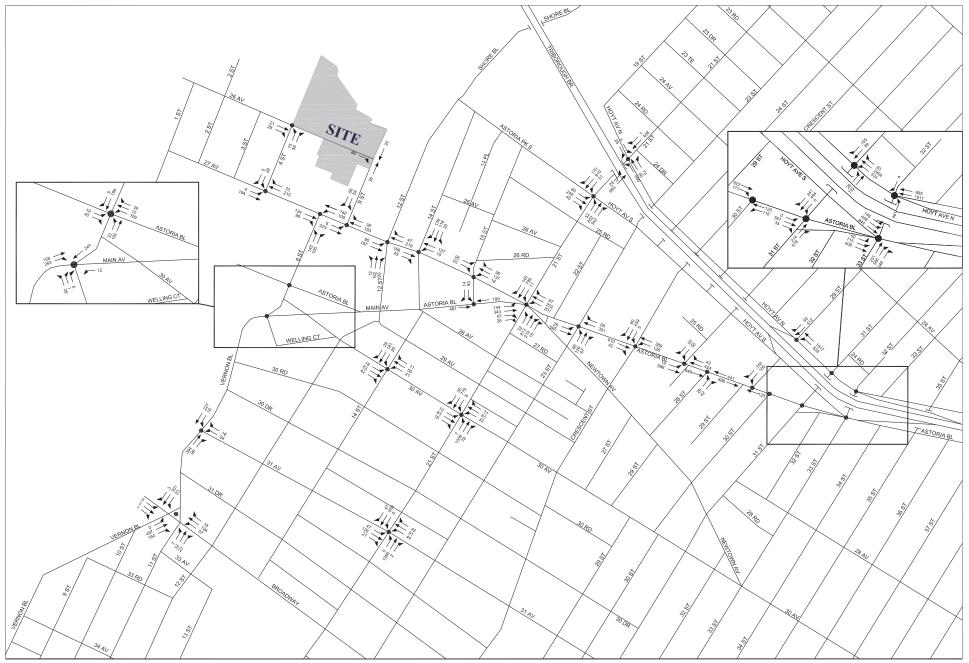
Analyzed Locations

# Astoria Cove



Analyzed Locations

### Astoria Cove



• Analyzed Locations

# Astoria Cove

				AM PEA	AK HOUR				Μ	IDDAY I	PEAK HO	UR				PM PEA	K HOUI	R	
Intersection		NO	)-ACTI	ON	WIT	H-ACT	ION	NC	-ACTIO	ON	WI	TH-ACT	ION	NO	)-ACTI	ON	WI	ГН-АСТ	ION
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
1. 26th Avenue & 4th Street	EB-LTR	-	-	-	NA	7.9	А	-	-	-	NA	7.7	А	-	-	-	NA	8.2	А
(Unsignalized-Two Way Stop)	NB-LR	0.11	9.7	А	NA	9.3	А	0.08	9.4	А	NA	9.0	А	0.09	9.3	А	NA	11.9	В
A. 26th Avenue & 9th Street (Unsignalized-Two Way Stop)	EB-R	0.09	8.9	А	0.37	13.3	В	0.13	8.9	А	0.23	10.5	В	0.10	8.8	А	0.28	11.3	В
2. 27th Avenue & 4th Street	EB-LT	0.78	22.4	С	0.78	22.4	С	0.45	14.1	В	0.45	14.1	В	0.56	15.0	В	0.56	15.0	В
(Existing Unsignalized-All Way Stop)	WB-T	0.44	13.7	В	0.44	13.7	В	0.43	13.1	В	0.43	13.1	В	0.65	15.6	В	0.65	15.6	В
(No-Action Signalized)	WB-R	0.25	12.2	В	0.68	22.3	С	0.27	12.5	В	0.89	38.7	D	0.29	11.8	В	1.42	216.9	F
	SB-LR	0.10	20.4	С	0.10	20.4	С	0.09	20.3	С	0.09	20.3	С	0.08	21.6	С	0.08	21.6	С
3. 27th Avenue & 8th Street	EB-T	0.53	14.9	В	0.53	14.9	В	0.24	11.9	В	0.24	11.9	В	0.36	13.2	В	0.36	13.2	В
	EB-R	0.66	21.2	С	0.66	21.2	С	0.61	22.5	С	0.61	22.5	С	0.42	15.9	В	0.42	15.9	В
	WB-LT	1.32	179.6	F	1.87	417.7	F *	1.25	151.3	F	1.72	354.1	F *	1.22	138.6	F	1.91	437.1	F
	NB-L	0.52	28.4	С	0.71	35.2	D	0.36	23.3	С	0.45	25.1	С	0.48	25.8	С	0.68	32.0	С
	NB-R	0.57	34.6	С	0.57	34.6	С	0.73	47.7	D	0.73	47.7	D	0.75	47.4	D	0.75	47.4	D
4. 27th Avenue & 12th Street	EB-LT	0.64	9.9	А	1.10	70.9	E *	0.47	11.2	В	0.77	19.4	В	0.54	8.2	А	0.99	40.5	D
(Existing Unsignalized-Two Way Stop)	WB-TR	0.47	6.2	А	0.60	7.4	А	0.41	10.4	В	0.61	13.9	В	0.66	8.8	А	1.01	35.0	С
(No-Action Signalized)	NB-LTR	0.57	43.1	D	0.59	44.1	D	0.28	27.3	С	0.30	27.7	С	0.86	65.8	Е	0.90	70.6	Е
5. 27th Avenue & 14th Street	EB-TR	0.61	19.4	В	1.15	95.3	F *	0.33	11.5	В	0.54	14.1	В	0.45	15.7	В	0.77	21.2	С
(Existing Unsignalized-All Way Stop)	WB-LT	0.66	22.9	С	1.27	157.2	F *	0.29	11.0	В	0.47	13.0	В	0.57	16.6	В	1.02	41.0	D
(No-Action Signalized)	SB-LTR	0.89	41.0	D	0.89	41.0	D	0.52	28.5	С	0.52	28.5	С	0.79	36.0	D	0.79	36.0	D
6. 27th Avenue & 18th Street	EB-L	0.14	9.7	А	0.17	9.9	А	0.10	8.4	А	0.14	9.2	А	0.15	9.3	А	0.24	11.6	В
(Unsignalized-Two Way Stop)	WB-L	0.02	7.8	А	0.02	8.4	А	0.01	7.7	А	0.01	8.0	А	0.01	7.9	А	0.02	8.2	А
7. Astoria Boulevard & 21st Street	EB-L	1.20	156.4	F	1.22	165.5	F *	0.33	36.9	D	0.36	37.7	D	0.61	46.8	D	0.67	48.9	D
	EB-TR	1.70	365.9	F	2.08	535.6	F *	0.61	41.5	D	0.69	44.0	D	1.13	118.0	F	1.29	186.0	F
	WB-L	1.01	69.0	Е	1.01	69.0	Е	0.86	53.2	D	0.86	53.2	D	0.92	68.3	Е	0.91	66.7	Е
	WB-TR	0.82	45.2	D	0.90	48.2	D	0.46	36.4	D	0.56	38.0	D	0.99	73.3	Е	1.26	172.6	F
	NB-LT	0.72	31.8	С	0.80	35.6	D	0.80	38.4	D	0.97	46.1	D *	1.11	85.3	F	1.29	165.3	F
	NB-R	0.37	24.7	С	0.37	24.7	С	0.65	36.1	D	0.65	36.1	D	0.44	22.9	С	0.44	22.9	С
	SB-LT	0.87	31.3	С	0.87	31.2	С	0.78	38.5	D	0.78	38.5	D	0.78	30.0	С	0.78	30.0	С
	SB-R	0.59	26.9	С	0.67	28.4	С	0.75	39.7	D	0.91	47.9	D *	0.80	33.1	С	1.02	62.3	Е
8. Astoria Boulevard & 23rd Street	EB-LT	1.21	127.5	F	1.47	243.1	F *	0.81	23.1	С	0.89	28.8	С	0.95	35.5	D	1.06	63.7	Е
	WB-TR	0.91	29.7	С	0.95	34.1	С	0.77	17.4	В	0.84	19.0	В	0.84	22.7	С	1.01	37.9	D
	NB-LTR	0.50	33.5	С	0.50	33.5	С	0.56	28.5	С	0.56	28.5	С	0.61	37.4	D	0.61	37.4	D

### Table 13-21: 2023 Future Weekday With-Action Condition–LOS at Analyzed Intersections

### Table 13-21 (continued): 2023 Future Weekday With-Action Condition–LOS at Analyzed Intersections

				AM PE	AK HOUR				M	IDDAY F	PEAK HO	UR				PM PEA	K HOU	ł	
T-to-read to-re		NC	)-ACTIO	)N	WIT	H-ACT	ION	NO	-ACTIC	ON	WI	H-ACT	ION	NO	)-ACTIO	ON	WI	ГН-АСТ	TION
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
9. Astoria Boulevard & Crescent Street	EB-TR	1.28	159.6	F	1.53	270.4	F *	0.83	25.1	С	0.91	32.0	С	1.11	88.2	F	1.23	136.4	F
	WB-LT	1.24	139.4	F	1.41	213.7	F *	1.27	143.1	F	1.35	181.2	F *	1.53	267.6	F	1.74	362.6	F
	SB-LTR	1.20	130.1	F	1.28	166.7	F *	1.17	110.1	F	1.27	154.1	F *	1.13	99.3	F	1.39	214.3	F
10. Astoria Boulevard & 27th Street	EB-LT	0.96	38.2	D	1.15	100.0	F *	0.59	16.2	В	0.65	17.4	В	0.79	22.1	С	0.88	27.5	С
	WB-TR	0.84	23.0	С	0.85	23.8	С	0.71	18.3	В	0.72	18.8	В	0.65	16.8	В	0.69	17.7	В
	SB-LR	0.83	41.1	D	0.83	41.1	D	0.53	34.9	С	0.53	34.9	С	0.88	42.7	D	0.88	42.7	D
11. Astoria Boulevard & 28th Street	NB-LR	0.70	68.0	F	0.95	139.4	F	0.42	28.3	D	0.48	33.8	D	0.41	30.1	D	0.49	39.5	Е
(Unsignalized-Two Way Stop)																			
12. Astoria Boulevard & 29th Street	EB-T	1.63	328.2	F	1.93	460.9	F *	0.97	48.8	D	1.06	72.4	E *	1.30	179.5	F	1.44	238.1	F
	WB-T	0.44	27.5	С	0.44	27.5	С	0.23	13.5	В	0.23	13.5	В	0.22	20.3	С	0.22	20.3	С
	SB-L	0.18	17.0	В	0.18	17.0	В	0.12	18.1	В	0.12	18.1	В	0.16	19.5	В	0.16	19.5	В
	SB-R	0.75	31.3	С	0.77	32.3	С	0.70	30.5	С	0.72	31.7	С	0.66	30.4	С	0.71	32.9	С
13. Astoria Boulevard & 30th Street	WB-LT	0.00	12.9	В	0.00	15.0	В	0.10	10.1	В	0.11	10.5	В	0.23	12.6	В	0.25	13.7	В
(Unsignalized-Two Way Stop)																			
14. Astoria Boulevard & 31st Street	EB-LTR	0.83	37.5	D	1.00	53.0	D *	0.57	22.4	С	0.62	23.2	С	0.75	34.8	С	0.84	36.9	D
	NB-T	0.52	41.8	D	0.52	41.8	D	0.54	33.7	С	0.54	33.7	С	0.52	41.6	D	0.52	41.6	D
	NB-R	0.67	16.5	В	0.67	16.5	В	0.53	8.9	А	0.53	8.9	Α	0.84	24.2	С	0.84	24.2	С
	SB-T	0.99	51.0	D	0.99	51.0	D	0.55	17.7	В	0.55	17.7	В	0.63	20.8	С	0.63	20.8	С
	SB-R	0.30	14.9	В	0.30	14.9	В	0.31	14.3	В	0.31	14.3	В	0.31	15.1	В	0.31	15.1	В
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	1.32	192.2	F	1.49	269.1	F *	1.02	62.4	Е	1.09	83.5	F *	1.17	121.1	F	1.24	154.2	F
33rd Street	NB-TR	1.09	91.5	F	1.09	91.5	F	0.76	36.6	D	0.76	36.6	D	1.07	77.7	Е	1.07	77.7	Е
	NB-R	1.09	97.7	F	1.09	97.7	F	0.87	49.3	D	0.87	49.3	D	1.13	108.5	F	1.13	108.5	F
	Hoyt Ave (EB-LT)	0.63	27.1	С	0.63	27.1	С	0.78	30.4	С	0.78	30.4	С	0.87	41.3	D	0.87	41.3	D
16. Hoyt Ave N. & 29th Street	WB-L	0.80	14.6	В	0.80	14.6	В	0.57	12.0	В	0.57	12.0	В	0.45	12.7	В	0.45	12.7	В
	WB-LT	0.94	19.4	В	0.96	21.1	С	0.68	13.2	В	0.71	13.6	В	0.86	21.6	С	0.93	25.9	С
	SB-R	1.03	98.5	F	1.13	130.5	F *	0.53	35.5	D	0.56	36.0	D	0.85	54.2	D	0.88	57.3	Е
17. Hoyt Ave N. & 31st Street	WB-L	0.81	37.5	D	0.81	37.5	D	0.71	36.5	D	0.71	36.5	D	0.34	15.0	В	0.34	15.0	В
	WB-T	1.15	91.2	F	1.16	98.1	F *	0.93	26.6	С	0.96	29.4	С	0.99	40.1	D	1.05	56.1	Е
	WB-R	0.02	7.5	А	0.02	7.5	А	0.18	11.6	В	0.18	11.6	В	0.15	13.3	В	0.15	13.3	В
	NB-DefL	-	-	-	-	-	-	0.66	40.3	D	0.66	40.3	D	-	-	-	-	-	-
	NB-T	-	-	-	-	-	-	0.23	21.2	С	0.23	21.2	С	-	-	-	-	-	-
	NB-LT	0.32	36.4	D	0.32	36.4	D		30.4	С	1	30.4	С	0.29	28.3	С	0.29	28.3	С
	SB-T	0.62	44.5	D	0.62	44.5	D	0.59	27.2	С	0.59	27.2	С	0.25	28.1	С	0.25	28.1	С
	SB-R	0.74	57.8	Е	0.77	60.1	Е	0.26	22.2	С	0.29	22.7	С	0.49	34.6	С	0.52	35.5	D

Та	ble 13-21 (continued): 20	23 Future <u>We</u>	<u>eekday</u> With	-Action C	Condition-L	OS at Analyzed	Intersections

				AM PEA	K HOUR				м	DDAYF	PEAK HO	1 IR				PM PEA	KHOUF	2	
		N	)-ACTI			H-ACT	ION	NO	-ACTIC			H-ACT	ION	NC	-ACTIO			H-ACT	TION
Intersection	T	V/C	Delay		V/C	Delay		V/C	Delay		V/C	Delay		V/C	Delay		V/C	Delay	
	Lane Group	Ratio	(sec.)	105	Ratio	(sec.)	105	Ratio	(sec.)	105	Ratio	(sec.)	105	Ratio	(sec.)	105	Ratio	(sec.)	105
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.74	13.3	В	0.74	13.3	В	0.51	9.7	А	0.51	9.7	А	0.46	10.9	В	0.46	10.9	В
	WB(Ramp)-T	1.17	127.2	F	1.19	136.2	- F *	1.03	45.5	D	1.06	54.9	D *	1.13	84.7	F	1.20	116.1	F
	NB-L	0.65	45.2	D	0.66	45.3	D	0.32	28.4	C	0.33	28.5	C	0.52	38.6	D	0.53	38.7	D
	SB-R	0.03	38.0	D	0.03	38.0	D	0.02	25.9	C	0.02	25.9	C	0.02	33.3	C	0.02	33.3	C
19. Astoria Boulevard & 8th Street	EB-L	0.16	24.6	С	0.16	24.6	С	0.09	26.1	С	0.09	26.1	С	0.17	29.0	С	0.17	29.0	С
	EB-R	0.77	44.4	D	0.77	44.4	D	0.27	29.0	С	0.27	29.0	С	0.66	40.6	D	0.66	40.6	D
	WB-L	0.32	26.9	С	0.32	26.9	С	0.36	30.6	С	0.36	30.6	С	0.31	31.0	С	0.31	31.0	С
	WB-TR	0.34	27.3	С	0.34	27.3	С	0.34	30.3	С	0.34	30.3	С	0.50	35.3	D	0.50	35.3	D
	NB-LT	0.52	20.2	С	0.66	23.6	С	0.46	17.2	В	0.53	18.5	В	0.87	27.7	С	1.04	59.0	Е
	SB-TR	0.74	27.0	С	0.84	32.8	С	0.40	16.3	В	0.43	16.9	В	0.39	15.1	В	0.44	15.9	В
20. 30th Avenue & 14th Street	EB-LTR	NA	13.0	В	NA	15.5	С	NA	9.1	А	NA	9.7	А	NA	9.6	А	NA	10.5	В
(Unsignalized-All Way Stop)	WB-LTR	NA	13.4	В	NA	16.3	С	NA	9.1	А	NA	9.8	А	NA	9.5	А	NA	10.7	В
	SB-LTR	NA	28.5	D	NA	60.5	F *	NA	9.5	А	NA	10.9	В	NA	11.4	В	NA	15.4	С
21. 30th Avenue & 21st Street	EB-LTR	0.52	39.0	D	0.77	51.2	D *	0.35	34.5	С	0.48	37.8	D	0.37	35.1	D	0.55	39.9	D
	WB-LTR	0.48	38.0	D	0.55	40.3	D	0.39	35.6	D	0.42	36.5	D	0.50	38.8	D	0.58	41.5	D
	NB-LTR	0.53	15.0	В	0.55	15.3	В	0.53	14.9	В	0.54	15.2	В	0.78	21.7	С	0.81	23.1	С
	SB-LTR	0.76	20.3	В	0.77	20.4	С	0.43	13.1	В	0.43	13.1	В	0.49	14.0	В	0.49	14.0	В
22. Vernon Boulevard & Welling Court/	EB-LT	1.18	116.5	F	1.26	152.3	F *	0.91	45.7	D	0.99	58.7	Е *	1.43	229.6	F	1.59	300.3	F
8th Street	WB-TR	0.04	21.1	С	0.04	21.1	С	0.04	21.1	С	0.04	21.1	С	0.06	21.3	С	0.06	21.3	С
	NB-LTR	0.33	36.1	D	0.33	36.1	D	0.17	31.0	С	0.17	31.0	С	0.18	29.5	С	0.18	29.5	С
	SB-R	1.01	68.7	Е	1.11	99.9	F *	0.71	35.1	D	0.76	37.8	D	0.72	37.9	D	0.79	42.2	D
23. Astoria Boulevard & 18th Street	EB-T	0.91	39.6	D	0.93	41.5	D	0.41	23.1	С	0.41	23.1	С	0.76	31.5	С	0.77	32.0	С
(Existing Unsignalized-Two Way Stop)	WB-T	0.66	27.1	С	0.66	27.1	С	0.41	22.9	С	0.41	22.9	С	0.44	22.2	С	0.44	22.2	С
(No-Action Signalized)	SB-LR	0.46	25.0	С	0.83	41.9	D	0.32	22.1	С	0.44	24.7	С	0.32	22.0	С	0.50	25.8	С
24. Hoyt Avenue N. & 21st Street	EB-L	0.02	40.4	D	0.02	40.4	D	0.12	44.0	D	0.12	44.0	D	0.11	43.9	D	0.11	43.9	D
	EB-R	0.37	47.5	D	0.37	47.5	D	0.15	44.5	D	0.15	44.5	D	0.19	45.3	D	0.19	45.3	D
	WB-L	1.09	88.0	F	1.12	100.7	F *	0.83	42.3	D	0.87	44.9	D	0.98	62.2	Е	1.07	87.8	F
	WB-TR	0.25	14.8	В	0.25	14.8	В	0.17	14.2	В	0.17	14.2	В	0.30	16.9	В	0.30	16.9	В
	NB-L	0.31	32.3	С	0.32	33.1	С	0.12	25.4	С	0.12	25.5	С	0.17	24.7	С	0.17	24.8	С
	NB-T	1.20	143.8	F	1.30	184.4	F *	0.81	46.3	D	0.86	51.1	D	1.12	99.0	F	1.17	119.4	F
	SB-TR	1.04	65.0	E	1.06	73.8	Е *	0.60	34.1	С	0.62	34.7	С	0.77	37.9	D	0.80	39.4	D

70.5

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				AM PEA	AK HOUR				M	IDDAY P	EAK HO	UR				PM PEA	KHOU	R		
Textore a stire.	[ [	NC	O-ACTIO	)N	WIT	H-ACTI	ON	NO	-ACTIC	ON	WI	гн-аст	ION	NO	O-ACTIO	ON	WI	TH-ACT	ION	
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	
	Group	Ratio	(sec.)	l	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		
25. Hoyt Avenue S./Astoria Park S. &	EB-LTR	0.84	41.9	D	0.93	44.9	D	0.36	32.0	С	0.40	32.6	С	0.58	37.9	D	0.63	39.0	D	٦
21st Street	NB-LT	-	-	-	-	-	-	-	-	-	-	-	-	0.72	16.9	В	0.75	17.8	В	
	NB-R	-	-	-	-	-	-	-	-	-	-	-	-	0.51	13.3	В	0.52	13.4	В	
	NB-LTR	0.61	14.3	В	0.63	14.9	В	0.48	15.0	В	0.49	15.1	В		15.7	В		16.4	В	
	SB-LTR	1.12	81.1	F	1.16	96.5	F *	0.74	20.2	С	0.77	21.2	С	1.00	40.4	D	1.06	59.1	Е	*
26. 27th Avenue & 9th Street	EB-LT	0.02	8.5	А	0.01	8.9	А	0.01	8.1	А	0.00	8.6	А	0.01	8.8	А	0.01	10.1	В	
(Unsignalized-Two Way Stop)	SB-LR	0.56	29.6	D	2.35	651.8	F *	0.43	15.9	С	1.01	79.1	F *	0.60	31.2	D	2.53	744.3	F	*
27. Vernon Boulevard & 31st Avenue	WB-LR	0.66	38.2	Е	0.72	45.7	E *	0.25	17.7	С	0.28	18.6	С	0.51	29.2	D	0.59	36.0	Е	*
(Unsignalized-Two Way Stop)	SB-LT	0.02	8.3	А	0.02	8.3	А	0.03	8.1	А	0.03	8.2	А	0.02	8.9	А	0.03	9.0	А	
28. Vernon Boulevard & Broadway/11th Street	EB-LTR	0.01	28.2	С	0.01	28.2	С	0.02	25.4	С	0.02	25.4	С	0.03	33.2	С	0.03	33.2	С	٦
	WB-LT	0.87	38.9	D	0.87	38.9	D	-	-	-	-	-	-	0.77	47.0	D	0.77	47.0	D	
	WB-R	0.21	29.9	С	0.23	30.3	С	-	-	-	-	-	-	0.24	35.8	D	0.37	37.9	D	
	WB-LTR	0.00	37.7	D		37.6	D	0.96	55.5	Е	1.01	67.6	Е *	0.00	45.1	D		44.9	D	
	NB (Vernon Blvd)-LT	0.28	8.2	А	0.29	8.3	А	0.29	9.0	А	0.30	9.1	А	0.52	10.1	В	0.54	10.4	В	
	NB (Vernon Blvd)-R	0.11	6.8	А	0.11	6.8	А	0.21	8.3	А	0.21	8.3	А	0.18	6.7	А	0.18	6.7	А	
	NB (11th Street)-LTR	0.38	41.1	D	0.38	41.1	D	0.22	32.8	С	0.22	32.8	С	0.33	38.2	D	0.33	38.2	D	

1.46 241.9

47.3

42.0

14.3

30.5

0.70

0.61

0.51

0.92

F

D

D

В

С

31.5

34.5

35.9

17.0

15.7

0.67

0.34

0.42

0.64

0.58

С

С

D

В

В

0.72 33.5

35.4

36.7

17.3

16.1

0.38

0.45

0.66

0.60

С

D

D

В

В

0.88

0.50

0.42

0.79

0.67

45.4

35.0

32.4

24.2

20.3

D

D

С

С

С

#### Table 13-21 (continued): 2023 Future Weekday With-Action Condition-LOS at Analyzed Intersections

F

D

D

В

С

1.36 195.9

45.6

41.1

14.2

27.9

0.67

0.58

0.50

0.90

#### Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

SB-LTR

EB-LTR

WB-LTR

NB-TR

SB-TR

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

29. 31st Avenue & 21st Street

\* - Denotes a significant adverse impact.

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version 5.5)

This table has been updated for the FEIS.

	Exis	ting Condi	tions	Conditi	lternate No ion without nt Developr	Halletts
	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour
Overall LOS A/B/C	64	85	72	54	80	67
Overall LOS D	25	16	22	25	16	19
Overall LOS E	10	1	8	9	3	5
Overall LOS F	3	1	0	13	3	10
Number of movements at LOS E or F	13	2	8	22	6	15

# Weekday Lane Group Level of Service Summary Comparison–Existing vs. Alternate No-Action Condition

<u>This table has been updated for the FEIS.</u>

Astoria Boulevard & 21<sup>st</sup> Street:

- The eastbound left-turn movement would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour.
- The eastbound through/right movement would deteriorate from LOS D under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour and from LOS D to LOS E in the PM peak hour.
- The northbound approach would deteriorate from LOS D under existing conditions to LOS E under the alternate No-Action condition in the AM peak hour, from LOS E to LOS F in the midday peak hour, and from LOS D to LOS F in the PM peak hour.
- The southbound approach would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour, from LOS D to LOS  $\underline{F}$  in the midday peak hour, and from LOS C to LOS  $\underline{E}$  in the PM peak hour.

### Astoria Boulevard & Crescent Street

- The eastbound approach would deteriorate from LOS C under existing conditions to LOS D under the alternate No-Action condition in the PM peak hour.
- The westbound approach would deteriorate from LOS C under existing conditions to LOS D under the alternate No-Action condition in the AM peak hour, from LOS C to LOS E in the midday peak hour, and from LOS D to LOS F in the PM peak hour.
- The southbound approach would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour and from LOS D to LOS  $\underline{F}$  in both the midday and PM peak hours.

Astoria Boulevard & 29<sup>th</sup> Street

- The eastbound approach would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in both the AM and PM peak hours.

		AM PEA	K HOUR	MIDDAY P	EAK HOUR	PM PEA	K HOUR
Intersection		EXISTING	NO-ACTION	EXISTING	NO-ACTION	EXIS TING	NO-ACTION
intersection	Lane	V/C Delay LOS					
	Group	Ratio (sec.)					
1. 26th Avenue & 4th Street	WB-LT	0.03 7.7 A		0.07 7.9 A		0.05 7.9 A	
(Unsignalized-T wo Way Stop)	NB-LR	0.10 10.1 B	0.11 9.7 A	0.08 10.3 B	0.08 9.4 A	0.06 9.5 A	0.09 9.3 A
A. 26th Avenue & 9th Street	EB-R		0.09 8.9 A		0.13 8.9 A		0.10 8.8 A
(Unsignalized-Two Way Stop)							
2. 27th Avenue & 4th Street	EB-LT	NA 10.0 A	NA 9.9 A	NA 9.6 A	NA 9.1 A	NA 9.8 A	NA 9.6 A
(Unsignalized-All Way Stop)	WB-T	NA 11.1 B	NA 11.0 B	NA 10.4 B	NA 9.9 A	NA 10.5 B	NA 10.2 B
	WB-R	NA 7.9 A	NA 7.9 A	NA 8.1 A	NA 7.8 A	NA 8.0 A	NA 8.0 A
	SB-LR	NA 9.8 A	NA 9.3 A	NA 9.8 A	NA 8.4 A	NA 9.5 A	NA 8.8 A
3. 27th Avenue & 8th Street	EB-TR	0.59 18.5 B	0.54 17.2 B	0.54 17.2 B	0.38 14.1 B	0.48 15.6 B	0.39 14.0 B
	WB-LT	0.81 30.7 C	0.98 57.1 E *	0.55 18.4 B	0.89 41.5 D	0.41 14.9 B	0.59 19.3 B
	NB-L NB-R	0.41 24.5 C 0.26 22.0 C	0.43 24.9 C 0.28 22.3 C	0.30 22.3 C 0.28 22.4 C	0.31 22.6 C 0.30 22.7 C	0.33 22.9 C 0.30 22.6 C	0.36 23.4 C 0.33 23.1 C
4. 27th Avenue & 12th Street	EB-LT	0.07 8.6 A	0.08 8.7 A	0.05 8.0 A	0.06 8.1 A	0.08 8.4 A	0.09 8.5 A
(Unsignalized-Two Way Stop)	NB-LTR	0.43 25.5 D	0.51 31.3 D	0.24 15.9 C	0.26 16.9 C	0.69 38.3 E *	0.79 52.9 F <sup>•</sup>
5. 27th Avenue & 14th Street	EB-TR	NA 10.6 B	NA 11.9 B	NA 9.2 A	NA 9.5 A	NA 9.9 A	NA 10.6 B
(Unsignalized-All Way Stop)	WB-LT	NA 12.1 B	NA 13.3 B	NA 9.0 A	NA 9.2 A	NA 9.6 A	NA 10.3 B
	SB-LTR	NA 16.8 C	NA 20.0 C	NA 9.2 A	NA 9.5 A	NA 10.5 B	NA 11.2 B
6. 27th Avenue & 18th Street	EB-L	0.07 9.3 A	0.08 9.3 A	0.07 8.2 A	0.07 8.2 A	0.09 8.1 A	0.10 8.1 A
(Unsignalized-Two Way Stop)	WB-L	0.01 7.5 A	0.01 7.5 A	0.01 7.6 A	0.01 7.6 A	0.01 7.7 A	0.01 7.7 A
7. Astoria Boulevard & 21st Street	EB-L	0.82 59.3 E *	1.08 111.5 F *	0.25 34.6 C	0.29 36.1 D	0.45 41.9 D	0.56 45.3 D
	EB-TR	0.82 52.5 D	1.03 85.1 F *	0.38 36.1 D	0.45 37.9 D	0.75 47.7 D	0.87 55.1 E
	WB-L	0.95 57.8 E *	1.01 69.0 E *	0.81 49.3 D	0.86 53.2 D	0.83 58.3 E *	0.92 68.3 E
	WB-TR	0.72 42.7 D	0.77 43.9 D	0.36 35.0 D	0.40 35.6 D	0.69 48.1 D	0.79 51.2 D
	NB-LTR	0.80 35.7 D	1.00 59.2 E *	1.05 69.9 E *	1.22 142.8 F *	1.02 46.2 D *	1.25 144.2 F
	SB-LTR	1.05 60.8 E *	1.15 102.4 F *	0.97 49.1 D *	1.08 80.7 F *	0.87 34.4 C	1.03 58.8 E
8. Astoria Boulevard & 23rd Street	EB-LT	0.64 20.1 C	0.80 25.3 C	0.61 16.5 B	0.69 18.5 B	0.69 21.1 C	0.80 24.6 C
	WB-TR	0.81 24.4 C	0.87 27.2 C	0.66 15.3 B	0.72 16.3 B	0.63 18.4 B	0.72 20.2 C
	NB-LTR	0.48 33.0 C	0.50 33.5 C	0.53 27.8 C	0.56 28.4 C	0.57 35.3 D	0.60 36.2 D

### Table 13-23: Alternate 2023 Future <u>Weekday</u> No-Action Condition–LOS at Analyzed Intersections

				AM PEA	K HOUR				MI	DDAY P	EAK HOU	UR				PM PEAI	K HOUR		
Intersection		E	XIS TIN	G	NO	-ACTIO	ON	E	AIS TIN	G	NO	-ACTIO	ON	E	XIS TIN	G	NO	-ACTIO	)N
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
9. Astoria Boulevard & Crescent Street	EB-TR	0.72	24.0	С	0.88	33.9	С	0.63	17.3	В	0.72	19.6	В	0.82	27.9	С	0.93	38.6	D
	WB-LT	0.86	27.5	С	1.01	48.0	D *	0.98	31.1	C *	1.11	75.0	Е *	0.99	38.6	D *	1.20	119.5	F
	SB-LTR	1.05	66.5	Е *	1.20	129.1	F *	1.03	54.2	D *	1.07	109.1	F *	1.00	50.7	D *	1.13	98.3	F
10. Astoria Boulevard & 27th Street	EB-LT	0.54	15.2	В	0.66	17.9	В	0.44	13.6	В	0.50	14.5	В	0.57	15.7	В	0.65	17.5	В
	WB-TR	0.76	19.6	В	0.81	21.7	С	0.62	16.3	В	0.67	17.4	В	0.52	14.3	В	0.57	15.3	В
	SB-LR	0.75	38.8	D	0.79	39.7	D	0.47	34.1	С	0.49	34.3	С	0.71	38.0	D	0.76	39.1	D
11. Astoria Boulevard & 28th Street (Unsignalized-Two Way Stop)	NB-LR	0.32	20.8	С	0.43	28.6	D	0.30	18.9	С	0.35	22.4	С	0.25	17.4	С	0.31	21.2	С
										~			~		<b>7</b> 0 /				
12. Astoria Boulevard & 29th Street	EB-T	0.97	65.6 27.1	E *	1.17	127.2	F *	0.75	24.9	C	0.84	30.6	C	0.97	58.4	E *	1.10	96.4	F
	WB-T	0.42		C	0.44	27.5	C	0.22	13.4	В	0.23	13.5	В	0.21	20.2	C	0.22	20.3	C
	SB-L SB-R	0.17 0.65	16.9 26.9	B C	0.18 0.71	17.0 29.1	B C	0.12 0.58	18.0 26.2	B C	0.12 0.64	18.1 28.1	B C	0.16 0.48	19.5 25.1	B C	0.16 0.55	19.5 26.8	B C
	3D-K	0.03	20.9	C	0.71	29.1	C	0.58	20.2	C	0.04	20.1	C	0.48	23.1	C	0.55	20.8	C
13. Astoria Boulevard & 30th Street	WB-LT	0.26	11.3	В	0.00	10.5	в	0.08	9.2	А	0.09	9.6	А	0.17	10.4	В	0.19	11.2	В
(Unsignalized-Two Way Stop)																			
14. Astoria Boulevard & 31st Street	EB-LTR	0.79	37.7	D	0.97	52.9	D *	0.85	31.7	С	0.97	43.8	D *	0.96	46.4	D *	1.09	86.5	F
	NB-T	0.49	41.2	D	0.52	41.8	D	0.51	33.2	С	0.54	33.7	С	0.49	41.0	D	0.52	41.6	D
	NB-R	0.63	15.3	В	0.67	16.5	В	0.50	8.5	А	0.53	8.9	А	0.79	21.4	С	0.84	24.2	С
	SB-T	0.86	31.4	С	0.99	51.0	D *	0.62	19.1	В	0.55	17.7	В	0.67	21.8	С	0.63	20.8	С
	SB-R	0.53	19.0	В	0.30	14.9	В	0.29	14.1	В	0.31	14.3	В	0.30	14.9	В	0.31	15.1	В
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	0.91	50.4	D *	1.05	77.8	E *	0.92	44.5	D *	1.02	62.1	Е *	1.05	73.9	Е *	1.16	117.8	F
33rd Street	NB-TR	1.05	77.0	Е *	1.09	91.5	F *	0.77	37.3	D	0.76	36.6	D	1.05	69.4	Е *	1.07	77.7	Е
	NB-R	1.04	77.9	Е *	1.09	97.7	F *	0.76	40.7	D	0.87	49.3	D	1.04	69.9	Е *	1.13	108.5	F
	Hoyt Ave (EB-LT)	0.54	25.6	С	0.59	26.4	С	0.67	26.7	С	0.71	27.5	С	0.73	35.1	D	0.78	36.4	D
16. Hoyt Ave N. & 29th Street	WB-L	0.71	11.6	В	0.76	12.6	В	0.54	11.5	В	0.56	11.9	В	0.41	12.3	В	0.44	12.6	В
	WB-LT	0.71	11.3	В	0.70	15.3	В	0.50	10.8	В	0.65	12.6	В	0.56	14.1	В	0.76	17.9	В
	SB-R	0.99	90.5	F *	1.04	104.0	F *	0.49	34.5	С	0.51	34.9	С	0.78	49.8	D	0.82	51.8	D

### Table 13-23 (continued): Alternate 2023 Future Weekday No-Action Condition–LOS at Analyzed Intersections

Intersection			1	AM PEA	K HOUR				EAK HOU	PM PEAK HOUR									
		EXISTING			NO-ACTION			EXISTING			NO	-ACTIO	DN	EXISTING			NO-ACTION		
	Lane	V/C Delay LOS		V/C Delay LOS			V/C Delay LOS			V/C Delay LOS			V/C Delay LOS			V/C Delay LOS			
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	
17. Hoyt Ave N. & 31st Street	WB-L	1.02	87.8	F *	0.81	37.5	D	1.01	83.2	F *	0.71	36.5	D	0.42	16.0	В	0.34	15.0	В
	WB-T	0.90	21.6	C *	1.10	72.5	Е *	0.71	17.2	В	0.89	23.4	С	0.68	20.1	С	0.89	27.4	С
	WB-R	0.31	10.2	В	0.02	7.5	А	0.61	19.6	В	0.18	11.6	В	0.65	23.6	С	0.15	13.3	в
	NB-DefL	0.28	35.6	D	-	-	-	-	-	-	0.66	40.0	D	-	-	-	-	-	-
	NB-T	-	-	-	-	-	-	0.50	29.3	С	0.23	21.2	С	-	-	-	-	-	-
	NB-LT	-	-	-	0.32	36.4	D	0.22	21.1	С	-	-	-	0.28	28.1	С	0.29	28.3	С
	SB-T	0.26	36.0	D	0.62	44.5	D	0.44	24.1	С	0.59	27.2	С	0.15	26.5	С	0.25	28.1	С
	SB-R	0.69	53.7	D	0.73	56.5	Е *	0.24	21.9	С	0.26	22.1	С	0.46	33.6	С	0.48	34.4	С
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.51	8.6	А	0.74	13.2	В	0.35	7.8	А	0.51	9.7	А	0.31	9.1	А	0.45	10.9	В
	WB(Ramp)-T	1.05	81.1	F *	1.13	109.3	F *	0.92	22.0	C *	0.98	31.9	C *	0.89	23.5	С	0.99	38.1	D '
	NB-L	0.56	43.7	D	0.61	44.4	D	0.33	28.5	С	0.31	28.3	С	0.50	38.4	D	0.50	38.3	D
	SB-R	0.03	38.0	D	0.03	38.0	D	0.02	25.9	С	0.02	25.9	С	0.02	33.3	С	0.02	33.3	С
19. Astoria Boulevard & 8th Street	EB-LR	0.25	28.5	С	0.26	28.8	С	0.12	26.4	С	0.13	26.5	С	0.26	28.6	С	0.28	29.0	С
	WB-L	0.26	28.5	С	0.35	30.2	С	0.25	28.5	С	0.35	30.6	С	0.16	27.0	С	0.29	29.3	С
	WB-TR	0.20	27.7	С	0.20	27.8	С	0.15	27.0	С	0.16	27.0	С	0.15	26.9	С	0.15	27.0	С
	NB-LT	0.34	15.1	В	0.37	15.5	В	0.31	14.8	В	0.33	15.1	В	0.40	15.5	В	0.43	16.0	В
	SB-TR	0.50	17.9	В	0.53	18.5	В	0.31	15.1	В	0.33	15.3	В	0.29	14.8	В	0.31	15.0	В
20. 30th Avenue & 14th Street	EB-LTR	NA	11.5	В	NA	12.1	В	NA	8.7	А	NA	8.9	А	NA	9.1	А	NA	9.3	А
(Unsignalized-All Way Stop)	WB-LTR	NA	12.3	В	NA	12.9	В	NA	8.7	А	NA	8.8	А	NA	9.0	А	NA	9.1	А
	SB-LTR	NA	22.3	С	NA	26.5	D	NA	9.2	А	NA	9.4	А	NA	10.6	В	NA	11.0	В
21. 30th Avenue & 21st Street	EB-LTR	0.41	36.1	D	0.45	37.2	D	0.30	33.5	С	0.32	33.9	С	0.32	33.9	С	0.34	34.3	С
	WB-LTR	0.43	36.7	D	0.45	37.2	D	0.33	34.2	С	0.34	34.5	С	0.41	36.2	D	0.42	36.6	D
	NB-LTR	0.47	13.9	В	0.53	15.0	В	0.48	14.1	В	0.53	14.9	В	0.71	19.1	В	0.78	21.7	С
	SB-LTR	0.69	18.1	В	0.76	20.3	С	0.37	12.4	В	0.43	13.1	В	0.42	13.1	В	0.49	14.0	В
22. Vernon Boulevard & Welling Court	EB-LT	0.96	47.1	D *	1.21	132.9	F *	0.79	37.7	D	0.90	45.7	D *	1.04	66.2	Е *	1.22	136.0	F '
/8th Street	WB-TR	0.03	21.0	С	0.04	21.1	С	0.03	21.0	С	0.04	21.1	С	0.04	21.1	С	0.06	21.3	С
	NB-LTR	0.24	31.2	С	0.28	32.0	С	0.14	28.9	С	0.15	29.1	С	0.08	28.2	С	0.18	29.5	С
	SB-R	0.73	36.2	D	0.85	44.3	D	0.55	31.3	С	0.65	34.6	С	0.47	29.5	С	0.59	32.6	С
23. Astoria Boulevard & 18th Street	SB-LR	0.30	20.8	С	0.51	32.5	D	0.20	12.7	В	0.24	13.9	В	0.21	14.3	В	0.29	17.2	С
(Unsignalized-Two Way Stop)																			

### Table 13-23 (continued): Alternate 2023 Future Weekday No-Action Condition–LOS at Analyzed Intersections

Intersection				AM PEAK HOUR						MIDDAY PEAK HOUR						PM PEA	K HOUR	PM PEAK HOUR					
		EXISTING		NO-ACTION			EXISTING			NO-ACTION			EXISTING			NO-ACTION							
	Lane	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	LOS	V/C	Delay	y LOS	V/C	Delay	LOS	V/C	Delay	LOS				
	Group	Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)		Ratio	(sec.)	)	Ratio	(sec.)		Ratio	(sec.)					
24. Hoyt Avenue N. & 21st Street	EB-L	0.02	40.4	D	0.02	40.4	D	0.11	42.0	D	0.11	42.0	D	0.09	41.7	D	0.09	41.8	D				
	EB-R	0.36	47.1	D	0.37	47.5	D	0.13	42.3	D	0.13	42.4	D	0.17	43.0	D	0.17	43.1	D				
	WB-L	0.89	43.3	D	1.00	58.1	Е *	0.67	38.0	D	0.77	41.0	D	0.59	36.4	D	0.73	40.1	D				
	WB-TR	0.24	14.7	В	0.25	14.8	в	0.16	14.1	В	0.17	14.2	В	0.27	15.5	В	0.29	15.7	В				
	NB-L	0.27	30.4	С	0.31	32.2	С	0.10	25.1	С	0.11	25.3	С	0.16	25.8	С	0.18	26.1	С				
	NB-T	1.00	75.1	Е *	1.08	98.0	F *	0.74	41.1	D	0.78	43.5	D	1.05	78.2	Е *	1.12	101.6	F				
	SB-TR	0.97	47.2	D *	1.03	61.9	Е *	0.55	32.7	С	0.58	33.6	С	0.73	37.6	D	0.78	39.9	D				
25. Hoyt Avenue S./Astoria Park S.	EB-L	0.12	29.9	С				0.21	31.5	С				0.17	30.7	С							
& 21st Street	EB-TR	1.02	61.1	Е *				0.40	35.3	D				0.73	43.2	D							
	EB-LTR		57.8	Е *	0.61	36.3	D		33.9	С	0.33	32.8	С		40.7	D	0.47	34.6	С				
	NB-LTR	0.52	14.6	В	0.61	15.9	В	0.41	13.1	В	0.45	13.6	В	0.86	22.5	С	1.02	44.2	D				
	SB-LTR	0.98	33.2	C *	1.12	79.0	Е *	0.59	15.5	В	0.65	16.9	В	0.84	23.6	С	1.00	45.2	D				
26. 27th Avenue & 9th Street	EB-LT	0.01	8.2	А	0.01	8.2	А	0.00	7.7	А	0.00	7.8	А	0.01	7.8	А	0.01	7.9	А				
(Unsignalized-Two Way Stop)	SB-LR	0.11	12.0	В	0.34	15.3	С	0.07	10.0	А	0.33	12.1	В	0.04	9.7	А	0.33	14.2	В				
27. Vernon Boulevard & 31st Avenue	WB-LR	0.49	23.5	С	0.58	29.7	D	0.20	15.0	В	0.23	16.4	С	0.37	19.8	С	0.44	23.4	С				
(Unsignalized-Two Way Stop)	SB-LT	0.02	8.1	А	0.02	8.2	А	0.03	7.9	А	0.03	8.0	А	0.02	8.4	А	0.02	8.6	А				
28. Vernon Boulevard & Broadway/	EB-LTR	0.01	28.2	С	0.01	28.2	С	0.02	26.1	С	0.02	26.1	С	0.03	33.2	С	0.03	33.2	С				
11th Street	WB-LTR	1.01	56.0	Е *	1.13	99.5	F *	0.86	43.8	D	0.96	55.7	Е *	0.82	50.8	D	0.97	69.3	Е				
	NB (Vernon Blvd)-LT	0.24	7.8	А	0.26	8.0	А	0.25	8.2	А	0.27	8.4	А	0.44	9.0	А	0.48	9.5	А				
	NB (Vernon Blvd)-R	0.04	6.4	А	0.11	6.8	А	0.16	7.5	А	0.20	7.8	А	0.12	6.3	А	0.18	6.7	А				
	NB (11th Street)-LTR	0.36	40.8	D	0.38	41.1	D	0.21	32.8	С	0.22	32.8	С	0.32	38.0	D	0.33	38.2	D				
	SB-LTR	0.96	45.8	D *	1.08	80.8	F *	0.51	26.2	С	0.58	27.9	С	0.57	28.0	С	0.66	30.7	С				
29. 31st Avenue & 21st Street	EB-LTR	0.64	43.9	D	0.67	45.6	D	0.33	34.2	С	0.34	34.5	С	0.48	34.4	С	0.50	35.0	D				
	WB-LTR	0.56	40.0	D	0.58	41.1	D	0.40	35.5	D	0.42	35.9	D	0.40	32.0	С	0.42	32.4	С				
	NB-TR	0.43	13.2	В	0.49	14.0	В	0.58	15.6	В	0.63	16.8	В	0.69	20.8	С	0.77	23.2	С				
	SB-TR		20.7	С	0.86		С	0.50	14.4	В			В		18.1	В		19.7	В				

#### Table 13-23 (continued): Alternate 2023 Future Weekday No-Action Condition-LOS at Analyzed Intersections

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9) Analysis is based on the 2010 *Highway Capacity Manual* methodology (HCS+, version 5.5) *This table has been updated for the FEIS.* 

### Astoria Boulevard & 31<sup>st</sup> Street

- <u>—</u>The eastbound approach would deteriorate from LOS D (with a v/c ratio of 0.79) under existing conditions to LOS D (with a v/c ratio of 0.97) under the alternate No-Action condition in the AM <u>peak hour</u>, from LOS C to LOS D in the midday peak hour, and from LOS D to LOS F in the PM <u>peak hour</u>.
- <u>The southbound through-movement would deteriorate from LOS C under existing conditions to</u> <u>LOS D under the alternate No-Action condition in the AM peak hour.</u>

*Hoyt Avenue South/Astoria Boulevard & 33<sup>rd</sup> Street* 

- The eastbound approach would deteriorate from LOS D under existing conditions to LOS E under the alternate No-Action condition in both the AM and midday peak hours and from LOS E to LOS F in the PM peak hour.
- <u>- The northbound through/right movement would deteriorate from LOS E under existing conditions</u> to LOS F under the alternate No-Action condition in both the AM and PM peak hours.
- <u>The northbound right-turn</u> movement would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in both the AM and PM peak hours.

Hoyt Avenue North & 31<sup>st</sup> Street

- -\_\_\_\_The southbound right-turn movement would deteriorate from LOS D under existing conditions to LOS E under the alternate No-Action condition in the AM peak hour.
- <u>The westbound through movement would deteriorate from LOS C under existing conditions to</u> LOS E under the alternate No-Action condition in the AM peak hour.

### Astoria Boulevard <u>North & 32<sup>nd</sup> Street:</u>

- The westbound through movement at the ramp would deteriorate from LOS C under existing conditions to LOS D under the alternate No-Action condition in the PM peak hour.

### Vernon Boulevard & Welling Court/8<sup>th</sup> Street

- The eastbound approach would deteriorate from LOS D under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour, from an uncongested LOS D to a congested LOS D (delay greater than 45 seconds) in the midday peak hour, and from LOS E to LOS F in the PM peak hour.

### *Hoyt Avenue North & 21<sup>st</sup> Street*

- The westbound left-turn movement would deteriorate from an uncongested LOS D under existing conditions to a congested LOS  $\underline{E}$  under the alternate No-Action condition in the AM peak hour.
- The northbound through movement would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in both the AM and PM peak hours.
- The southbound approach would deteriorate from LOS D under existing conditions to LOS E under the alternate No-Action condition in the AM peak hour.

### Hoyt Avenue South/Astoria Park South & 21st Street

- The northbound approach would deteriorate from LOS C under existing conditions to LOS D under the alternate No-Action condition in the PM peak hour.
- The southbound approach would deteriorate from LOS C under existing conditions to LOS E under the alternate No-Action condition in the AM peak hour and from LOS C to LOS D in the PM peak hour.

Vernon Boulevard & Broadway/11<sup>th</sup> Street

- The westbound approach would deteriorate from LOS E under existing conditions to LOS F under the alternate No-Action condition in the AM peak hour and from LOS D to LOS E in both the midday and PM peak hours.
- The southbound approach would deteriorate from LOS D under Existing conditions to LOS F under the alternate No-Action condition in the AM peak hour.

### Alternate With-Action Condition <u>Weekday</u> Intersection Capacity Analysis

Figures 13-23, 13-24, and 13-25 show the traffic network volumes under the alternate With-Action condition (absent the Halletts Point <u>No-Action</u> development) for the weekday AM, midday, and PM peak hours, respectively. The volumes shown are the sum of the net incremental traffic generated by the Proposed Action and the alternate No-Action traffic network described above.

Table 13-24 shows a summary comparison of the individual lane group LOS for the alternate future No-Action and With-Action conditions. As shown in Table 13-24, <u>ten</u> individual traffic movements would operate at LOS E and <u>25</u> would operate at LOS F in the <u>weekday</u> AM peak hour under the alternate With-Action condition. During the <u>weekday</u> midday peak hour, three individual traffic movements would operate at LOS E and <u>six</u> would operate at LOS F, while <u>seven</u> and <u>16</u> individual traffic movements would operate at LOS E and LOS F, respectively, in the <u>weekday</u> PM peak hour under the alternate With-Action condition.

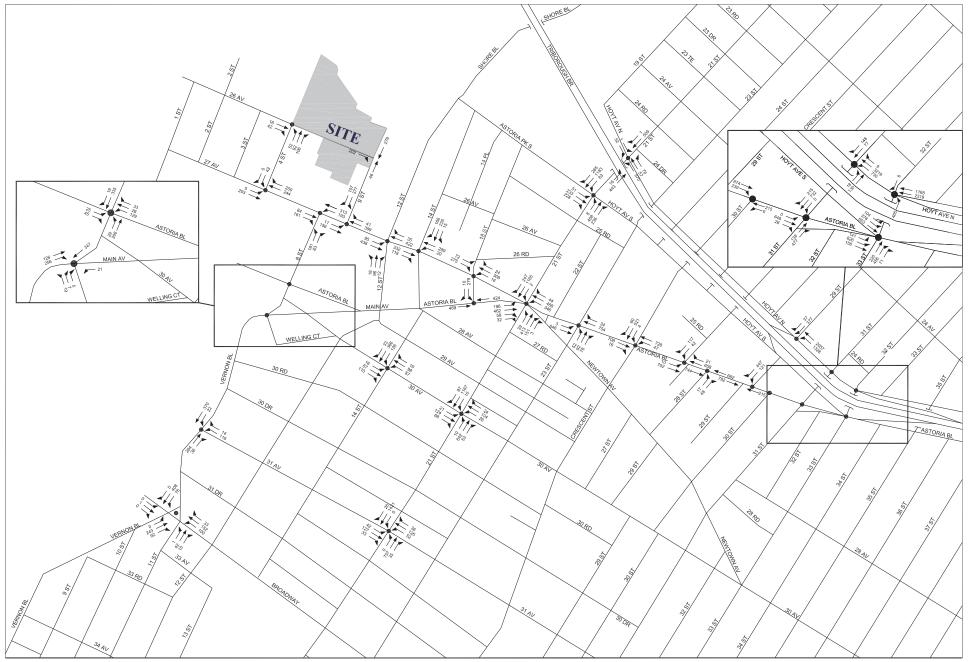
		ternate No Condition		2023 Alt	ernate Wit Condition	
	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour	Weekday AM Peak Hour	Weekday Midday Peak Hour	Weekday PM Peak Hour
Overall LOS A/B/C	54	80	67	49	71	58
Overall LOS D	25	16	19	18	21	21
Overall LOS E	9	3	5	10	3	7
Overall LOS F	13	3	10	25	6	16
Number of intersections with significant adverse impacts				20	8	14
Number of movements at LOS E or F	22	6	15	35	9	23

 Weekday
 Lane Group LOS Summary Comparison—Alternate No-Action

 vs. With-Action Conditions
 Particular State

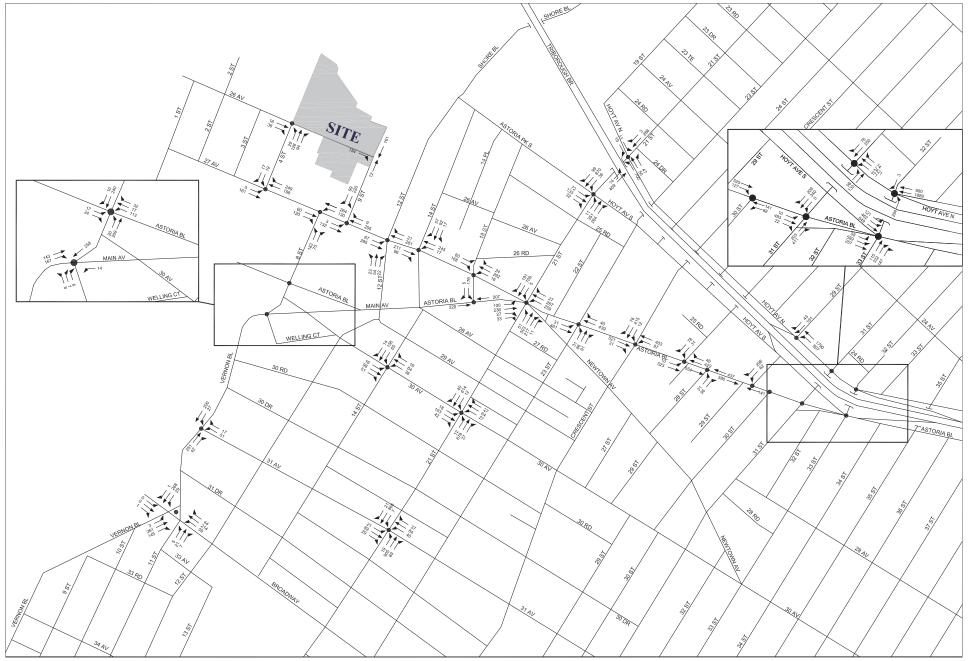
This table has been updated for the FEIS.

Table 13-25 provides a summary comparison of the impacts disclosed previously for the RWCDS that assumes the completion of the Halletts Point development and those identified in the alternate With-Action condition analysis.



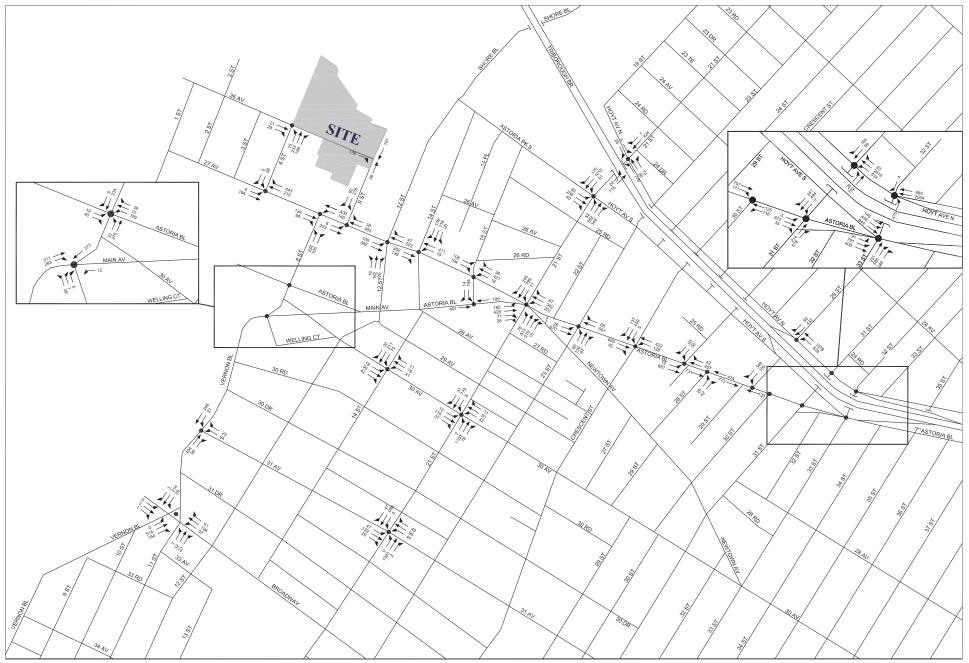
Analyzed Locations

## Astoria Cove



Analyzed Locations

# Astoria Cove



• Analyzed Locations

# Astoria Cove

Table 13-25: Comparison of <u>Weekday</u> Impact Locations—Future with Halletts Point
vs. Future without Halletts Point

		ay AM Hour Alternate		y Midday Hour Alternate		ay PM Hour Alternate
Intersection	With- Action Condition	With- Action Condition	With- Action Condition	With- Action Condition	With- Action Condition	With- Action Condition
1. 26 <sup>th</sup> Ave & 4 <sup>th</sup> St						
A. 26 <sup>th</sup> Ave & 9 <sup>th</sup> St						
2. 27 <sup>th</sup> Ave & 4 <sup>th</sup> St					Х	
3. 27 <sup>th</sup> Ave & 8 <sup>th</sup> St	Х	Х	Х	Х	Х	Х
26. 27 <sup>th</sup> Ave & 9 <sup>th</sup> St	Х	Х	Х		Х	Х
4. 27 <sup>th</sup> Ave & 12 <sup>th</sup> St	Х	Х		Х	Х	Х
5. 27 <sup>th</sup> Ave & 14 <sup>th</sup> St	Х	Х				Х
6. 27 <sup>th</sup> Ave & 18 <sup>th</sup> St						
7. Astoria Blvd & 21st St	Х	Х	Х	Х	Х	Х
8. Astoria Blvd & 23 <sup>rd</sup> St	Х	Х			Х	
9. Astoria Blvd & Crescent St	Х	Х	Х	Х	Х	Х
10. Astoria Blvd & 27th St	Х					
11. Astoria Blvd & 28th St						
12. Astoria Blvd & 29th St	Х	Х	Х		Х	Х
13. Astoria Blvd & 30th St						
14. Astoria Blvd & 31st St	Х	Х		Х		Х
15. Hoyt Ave S./Astoria Blvd & 33 <sup>rd</sup> St	Х	Х	Х	Х	Х	Х
16. Hoyt Ave N. & 29 <sup>th</sup> St	Х	Х				
17. Hoyt Ave N. & 31 <sup>st</sup> St	Х	Х			Х	
18. Astoria Blvd N. & 32 <sup>nd</sup> St	Х	Х	Х		Х	Х
19. Astoria Blvd & 8th St					Х	
20. 30 <sup>th</sup> Ave & 14 <sup>th</sup> St	Х	Х				
21. 30 <sup>th</sup> Ave & 21 <sup>st</sup> St	Х	Х				
22. Vernon Blvd & Welling Court/8 <sup>th</sup> St	Х	Х	Х	Х	Х	Х
23. Astoria Blvd & 18 <sup>th</sup> St		Х				
24. Hoyt Ave N. & 21 <sup>st</sup> St	Х	Х			Х	Х
25. Hoyt Ave S./Astoria Park S. & 21 <sup>st</sup> St	Х	Х			Х	Х
27. Vernon Blvd & 31 <sup>st</sup> Ave	Х				Х	
28. Vernon Blvd & Proodwov/11 <sup>th</sup> St	Х	Х	Х	Х	Х	Х
29. 31 <sup>st</sup> Ave & 21 <sup>st</sup> St						

Notes:

With-Action Condition: with Halletts Point Development Alternate With-Action Condition: without Halletts Point development

Bold - denotes where an intersection is signalized in With-Action condition and unsignalized in Alternate With-Action condition

X – denotes potential for significant adverse impact. <u>*This table has been updated for the FEIS.*</u>

Table 13-26 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in each peak hour under the alternate With-Action condition and identifies those movements that are considered impacted in one or more peak hours. As shown in Table 13-26, one or more approach or lane group at a total of <u>20</u> of the 30 analyzed intersections would experience significant adverse impacts in one or more peak hour, eight intersections would experience significant adverse impacts in the <u>weekday</u> AM peak hour, eight intersections would experience significant adverse impacts in the <u>weekday</u> M peak hour, and 14 intersections would experience significant adverse impacts in the <u>weekday</u> PM peak hour, as shown in Table 13-25. Potential measures to mitigate these significant adverse impacts are discussed in Chapter 20, "Mitigation."

## H. TRANSIT

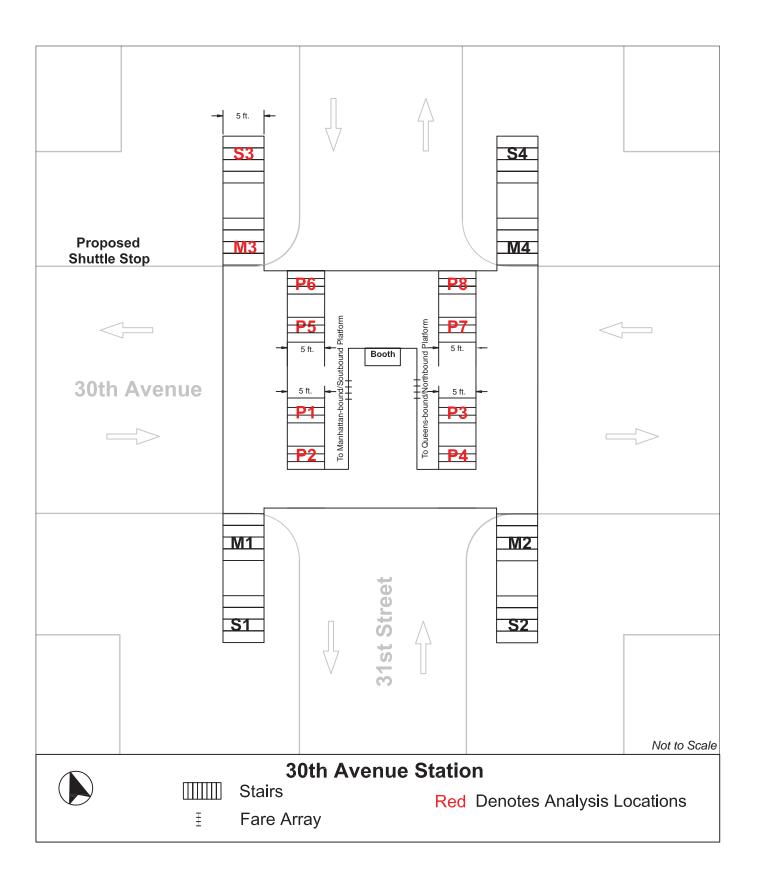
### **Existing Conditions**

### Subway

As discussed above in Section E, "Level 2 Screening Assessment", the northwest street-to-station staircase, the platform stairs, and the fare array elements within the control area at the  $30^{\text{th}}$  Avenue (N and Q line) Station would require detailed analyses as the increment in subway riders would exceed the 200 trips per hour *CEQR Technical Manual* threshold at these elements. As shown in Figure 13-26, which provides a schematic layout of the  $30^{\text{th}}$  Avenue Station, there are stairs at each of the four corners at the intersection of  $30^{\text{th}}$  Avenue and  $31^{\text{st}}$  Street that lead from street level up to the control area. There are two sets of three turnstiles to the east and west of the agent booth, which are adjacent to the northbound and southbound platforms, respectively. Beyond these turnstiles, four stairs leading up to the platform level can be accessed. The two platform stairs east of the agent booth (P3-P4 and P7-P8) connect to the Queens-bound platform, while the two platform stairs west of the agent booth (P1-P2 and P5-P6) connect to the Manhattan-bound platform.

As also shown in Figures 13-1 and 13-26, for transit analysis purposes, it is assumed that the proposed shuttle would drop off/pick up subway riders at the northwest corner of 30<sup>th</sup> Avenue and 31<sup>st</sup> Street. Because of the activity of the Q18 and Q102 bus stop, located at this corner, it is assumed that the bus stop would be lengthened west, potentially providing a second berth for the shuttle bus. The street-to-station stair at the northwest corner (S3-M3) would consequently be used by the majority of project-generated subway riders and is therefore the only street staircase that requires a detailed analysis, as noted above. Although the six turnstiles in the control area provide equal access to all four platform stairs, they are conservatively analyzed as two separate sets of three turnstiles. Out of the four platform staircases, P1-P2 and P5-P6 are analyzed in the <u>weekday</u> AM peak hour when commuter traffic is highest going to the Manhattan-bound platform, while in the <u>weekday</u> PM peak hour, P3-P4 and P7-P8 are analyzed based on the reverse commuter traffic primarily coming from the Queens-bound platform.

Table 13-27 summarizes the existing weekday AM and PM peak hour operating conditions and the results of the capacity analysis for street-to-station stair S3-M3 and platform stairs P1-P2, P3-P4, P5-P6, and P7-P8. Table 13-28 illustrates the peak period operating conditions for the 30<sup>th</sup> Avenue Station northbound and southbound turnstiles. It should be noted that the detailed transit analyses focus on the weekday AM and PM peak hours as it is during these periods that overall demand on the transit network is typically highest.



		AM PEA	K HOUR	MIDDAY P	EAK HOUR	PM PEA	K HOUR
Intersection		NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION
Intersection	Lane	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS
	Group	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)
1. 26th Avenue & 4th Street	EB-LTR		NA 7.9 A		NA 7.7 A		NA 8.2 A
(Unsignalized-Two Way Stop)	NB-LR	0.11 9.7 A	NA 9.3 A	0.08 9.4 A	NA 9.0 A	0.09 9.3 A	NA 11.9 B
A. 26th Avenue & 9th Street	EB-R	0.09 8.9 A	0.37 13.3 B	0.13 8.9 A	0.23 10.5 B	0.10 8.8 A	0.28 11.3 B
(Unsignalized-Two Way Stop)							
2. 27th Avenue & 4th Street	EB-LT	NA 9.9 A	NA 10.1 B	NA 9.1 A	NA 9.3 A	NA 9.6 A	NA 10.1 B
(Unsignalized-All Way Stop)	WB-T	NA 11.0 B	NA 11.0 B	NA 9.9 A	NA 9.9 A	NA 10.2 B	NA 10.3 B
	WB-R	NA 7.9 A	NA 9.4 A	NA 7.8 A	NA 9.2 A	NA 8.0 A	NA 13.3 B
	SB-LR	NA 9.3 A	NA 9.6 A	NA 8.4 A	NA 8.7 A	NA 8.8 A	NA 9.4 A
3. 27th Avenue & 8th Street	EB-TR	0.54 17.2 B	0.54 17.2 B	0.38 14.1 B	0.38 14.1 B	0.39 14.0 B	0.39 14.0 B
	WB-LT	0.98 57.1 E	1.46 237.9 F *	0.89 41.5 D	1.34 188.3 F *	0.59 19.3 B	1.26 154.6 F *
	NB-L	0.43 24.9 C	0.61 29.5 C	0.31 22.6 C	0.40 24.1 C	0.36 23.4 C	0.56 27.8 C
	NB-R	0.28 22.3 C	0.28 22.3 C	0.30 22.7 C	0.30 22.7 C	0.33 23.1 C	0.33 23.1 C
4. 27th Avenue & 12th Street	EB-LT	0.08 8.7 A	0.12 9.4 A	0.06 8.1 A	0.08 8.7 A	0.09 8.5 A	0.14 10.0 B
(Unsignalized-Two Way Stop)	NB-LTR	0.51 31.3 D	1.14 192.2 F *	0.26 16.9 C	0.47 32.1 D *	0.79 52.9 F	2.04 562.5 F *
5. 27th Avenue & 14th Street	EB-TR	NA 11.9 B	NA 92.8 F *	NA 9.5 A	NA 14.1 B	NA 10.6 B	NA 30.5 D *
(Unsignalized-All Way Stop)	WB-LT	NA 13.3 B	NA 35.8 E *	NA 9.2 A	NA 12.7 B	NA 10.3 B	NA 36.1 E *
	SB-LTR	NA 20.0 C	NA 52.3 F *	NA 9.5 A	NA 11.3 B	NA 11.2 B	NA 17.5 C
6. 27th Avenue & 18th Street	EB-L	0.08 9.3 A	0.11 9.5 A	0.07 8.2 A	0.10 8.6 A	0.10 8.1 A	0.15 9.7 A
(Unsignalized-Two Way Stop)	WB-L	0.01 7.5 A	0.02 8.0 A	0.01 7.6 A	0.01 7.8 A	0.01 7.7 A	0.01 8.0 A
7. Astoria Boulevard & 21st Street	EB-L	1.08 111.5 F	1.11 122.3 F *	0.29 36.1 D	0.32 36.8 D	0.56 45.3 D	0.62 47.1 D
	EB-TR	1.03 85.1 F	1.43 247.8 F *	0.45 37.9 D	0.53 39.6 D	0.87 55.1 E	1.04 84.0 F *
	WB-L	1.01 69.0 E	1.01 69.0 E	0.86 53.2 D	0.86 53.2 D	0.92 68.3 E	0.91 66.7 E
	WB-TR	0.77 43.9 D	0.85 46.0 D	0.40 35.6 D	0.50 37.1 D	0.79 51.2 D	1.07 94.9 F *
	NB-LTR	1.00 59.2 E	1.19 129.4 F *	1.22 142.8 F	1.56 295.5 F *	1.25 144.2 F	1.77 381.2 F *
	SB-LTR	1.15 102.4 F	1.19 120.5 F *	1.08 80.7 F	1.16 117.0 F *	1.03 58.8 E	1.18 119.0 F *
8. Astoria Boulevard & 23rd Street	EB-LT	0.80 25.3 C	1.06 67.4 E *	0.69 18.5 B	0.77 21.3 C	0.80 24.6 C	0.91 31.6 C
	WB-TR	0.87 27.2 C	0.91 30.2 C	0.72 16.3 B	0.79 17.7 B	0.72 20.2 C	0.89 25.2 C
	NB-LTR	0.50 33.5 C	0.50 33.5 C	0.56 28.4 C	0.56 28.4 C	0.60 36.2 D	0.60 36.2 D

## Table 13-26: Alternate 2023 Future <u>Weekday</u> With-Action Condition–LOS at Analyzed Intersections

		AM PEA	K HOUR	MIDDAY I	PEAK HOUR	PM PEA	K HOUR
To A survey of the survey		NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION
Intersection	Lane Group	V/C Delay LOS Ratio (sec.)					
9. Astoria Boulevard & Crescent Street	EB-TR	0.88 33.9 C	1.14 99.3 F *	0.72 19.6 B	0.79 22.8 C	0.93 38.6 D	1.05 66.6 E
	WB-LT	1.01 48.0 D	1.05 60.3 E *	1.11 75.0 E	1.19 109.7 F *	1.20 119.5 F	1.37 195.7 F
	SB-LTR	1.20 129.1 F	1.28 166.7 F *	1.07 109.1 F	1.27 153.0 F *	1.13 98.3 F	1.38 211.8 F
10. Astoria Boulevard & 27th Street	EB-LT	0.66 17.9 B	0.85 25.7 C	0.50 14.5 B	0.56 15.6 B	0.65 17.5 B	0.74 20.2 C
	WB-TR	0.81 21.7 C	0.83 22.4 C	0.67 17.4 B	0.69 17.8 B	0.57 15.3 B	0.61 16.0 B
	SB-LR	0.79 39.7 D	0.79 39.7 D	0.49 34.3 C	0.49 34.3 C	0.76 39.1 D	0.76 39.1 D
11. Astoria Boulevard & 28th Street (Unsignalized-Two Way Stop)	NB-LR	0.43 28.6 D	0.58 47.1 E	0.35 22.4 C	0.39 25.8 D	0.31 21.2 C	0.37 26.2 D
12. Astoria Boulevard & 29th Street	EB-T	1.17 127.2 F	1.46 253.2 F *	0.84 30.6 C	0.93 40.4 D	1.10 96.4 F	1.23 150.1 F
	WB-T	0.44 27.5 C	0.44 27.5 C	0.23 13.5 B	0.23 13.5 B	0.22 20.3 C	0.22 20.3 C
	SB-L	0.18 17.0 B	0.18 17.0 B	0.12 18.1 B	0.12 18.1 B	0.16 19.5 B	0.16 19.5 B
	SB-R	0.71 29.1 C	0.73 30.0 C	0.64 28.1 C	0.66 29.0 C	0.55 26.8 C	0.60 28.6 C
13. Astoria Boulevard & 30th Street	WB-LT	0.00 10.5 B	0.00 11.9 B	0.09 9.6 A	0.10 9.9 A	0.19 11.2 B	0.22 12.0 B
(Unsignalized-Two Way Stop)							
14. Astoria Boulevard & 31st Street	EB-LTR	0.97 52.9 D	1.27 165.1 F *	0.97 43.8 D	1.08 74.3 E *	1.09 86.5 F	1.24 148.9 F
	NB-T	0.52 41.8 D	0.52 41.8 D	0.54 33.7 C	0.54 33.7 C	0.52 41.6 D	0.52 41.6 D
	NB-R	0.67 16.5 B	0.67 16.5 B	0.53 8.9 A	0.53 8.9 A	0.84 24.2 C	0.84 24.2 C
	SB-T	0.99 51.0 D	0.99 51.0 D	0.55 17.7 B	0.55 17.7 B	0.63 20.8 C	0.63 20.8 C
	SB-R	0.30 14.9 B	0.30 14.9 B	0.31 14.3 B	0.31 14.3 B	0.31 15.1 B	0.31 15.1 B
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	1.05 77.8 E	1.22 147.0 F *	1.02 62.1 E	1.08 83.6 F *	1.16 117.8 F	1.24 154.0 F
33rd Street	NB-TR	1.09 91.5 F	1.09 91.5 F	0.76 36.6 D	0.76 36.6 D	1.07 77.7 E	1.07 77.7 E
	NB-R	1.09 97.7 F	1.09 97.7 F	0.87 49.3 D	0.87 49.3 D	1.13 108.5 F	1.13 108.5 F
	Hoyt Ave (EB-LT)	0.59 26.4 C	0.59 26.4 C	0.71 27.5 C	0.71 27.5 C	0.78 36.4 D	0.78 36.4 D
16. Hoyt Ave N. & 29th Street	WB-L	0.76 12.6 B	0.76 12.6 B	0.56 11.9 B	0.56 11.9 B	0.44 12.6 B	0.44 12.6 B
	WB-LT	0.70 15.3 B	0.90 16.1 B	0.65 12.6 B	0.67 13.0 B	0.76 17.9 B	0.82 19.9 B
	SB-R	1.04 104.0 F	1.15 140.3 F *	0.51 34.9 C	0.53 35.4 D	0.82 51.8 D	0.85 54.3 D

## Table 13-26 (continued): Alternate 2023 Future Weekday With-Action Condition–LOS at Analyzed Intersections

D

С

В

F

С

С

С

0.51

0.51

0.81

0.49

0.06

0.18

38.7 D

38.9

23.0

14.0

21.3

29.5

0.60 27.2 D

1.37 204.2

0.66 34.9

21. 30th Avenue & 21st Street

/8th Street

22. Vernon Boulevard & Welling Court

23. Astoria Boulevard & 18th Street

(Unsignalized-Two Way Stop)

EB-LTR

WB-LTR

NB-LTR

SB-LTR

EB-LT

WB-TR

NB-LTR

SB-R

SB-LR

0.45

0.45

0.53

1.21

0.04

0.28

0.85

37.2 D

37.2 D

15.0

132.9 F

21.1

32.0 С

44.3 D

0.51 32.5 D

0.76 20.3

В

С

С

		AM PEA	K HOUR	MIDDAY PEAK HOU	R	PM PEA	K HOUR
Intersection		NO-ACTION	WITH-ACTION	NO-ACTION WITH	ACTION	NO-ACTION	WITH-ACTION
intersection	Lane	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS V/C	Delay LOS	V/C Delay LOS	V/C Delay LOS
	Group	Ratio (sec.)	Ratio (sec.)	Ratio (sec.) Ratio	(sec.)	Ratio (sec.)	Ratio (sec.)
17. Hoyt Ave N. & 31st Street	WB-L	0.81 37.5 D	0.81 37.5 D	0.71 36.5 D 0.71	36.5 D	0.34 15.0 B	0.34 15.0 B
	WB-T	1.10 72.5 E	1.12 79.2 E *	0.89 23.4 C 0.92	24.9 C	0.89 27.4 C	0.95 32.1 C
	WB-R	0.02 7.5 A	0.02 7.5 A	0.18 11.6 B 0.18	11.6 B	0.15 13.3 B	0.15 13.3 B
	NB-DefL			0.66 40.0 D 0.66	40.0 D		
	NB-T			0.23 21.2 C 0.23	21.2 C		
	NB-LT	0.32 36.4 D	0.32 36.4 D			0.29 28.3 C	0.29 28.3 C
	SB-T	0.62 44.5 D	0.62 44.5 D	0.59 27.2 C 0.59	27.2 C	0.25 28.1 C	0.25 28.1 C
	SB-R	0.73 56.5 E	0.75 58.7 E	0.26 22.1 C 0.29	22.7 C	0.48 34.4 C	0.51 35.3 D
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.74 13.2 B	0.74 13.2 B	0.51 9.7 A 0.51	9.7 A	0.45 10.9 B	0.45 10.9 B
	WB(Ramp)-T	1.13 109.3 F	1.15 118.0 F *	0.98 31.9 C 1.01	38.8 D	0.99 38.1 D	1.07 60.4 E *
	NB-L	0.61 44.4 D	0.61 44.5 D	0.31 28.3 C 0.32	28.4 C	0.50 38.3 D	0.51 38.5 D
	SB-R	0.03 38.0 D	0.03 38.0 D	0.02 25.9 C 0.02	25.9 C	0.02 33.3 C	0.02 33.3 C
19. Astoria Boulevard & 8th Street	EB-LR	0.26 28.8 C	0.26 28.8 C	0.13 26.5 C 0.13	26.5 C	0.28 29.0 C	0.28 29.0 C
	WB-L	0.35 30.2 C	0.35 30.2 C	0.35 30.6 C 0.35	30.6 C	0.29 29.3 C	0.29 29.3 C
	WB-TR	0.20 27.8 C	0.20 27.8 C	0.16 27.0 C 0.16	27.0 C	0.15 27.0 C	0.15 27.0 C
	NB-LT	0.37 15.5 B	0.47 17.1 B	0.33 15.1 B 0.40	16.1 B	0.43 16.0 B	0.56 18.0 B
	SB-TR	0.53 18.5 B	0.63 20.8 C	0.33 15.3 B 0.36	15.8 B	0.31 15.0 B	0.36 15.7 B
20. 30th Avenue & 14th Street	EB-LTR	NA 12.1 B	NA 14.1 B	NA 8.9 A NA	9.4 A	NA 9.3 A	NA 10.1 B
(Unsignalized-All Way Stop)	WB-LTR	NA 12.9 B	NA 15.3 C	NA 8.8 A NA	9.4 A	NA 9.1 A	NA 10.1 B
	SB-LTR	NA 26.5 D	NA 54.0 F *	NA 9.4 A NA	10.7 B	NA 11.0 B	NA 14.6 B

0.70

0.52 39.1

0.55

1.30

0.04

0.28

0.96

47.1 D

15.3

171.8 F

21.1

32.0 С

59.7 Е

1.43 253.4 F

0.77 20.4 C

D

В

С

0.32

0.34

0.53

0.43

0.90

0.04

0.15

0.65

0.24

33.9 С

34.5

14.9

13.1

45.7

21.1

29.1

34.6 С

13.9 В

С

В

В

D

С

С

0.45

0.38

0.54

0.98

0.04

0.15

0.38

37.0 D

35.4

15.2

59.5 Е

21.1

29.1

15.9

0.43 13.1

0.71 36.9

D

в

В

С

С

D

С

0.34

0.42

0.78

1.22

0.06

0.18

0.59

0.29

34.3 С

36.6

21.7 С

21.3

29.5 С

32.6 С

136.0 F

17.2 C

0.49 14.0 B

D

С

#### Table 13-26 (continued): Alternate 2023 Future Weekday With-Action Condition-LOS at Analyzed Intersections

		AM PEA	K HOUR	MIDDAY P	EAK HOUR	PM PEA	K HOUR
Internet offer		NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION	NO-ACTION	WITH-ACTION
Intersection	Lane	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS	V/C Delay LOS
	Group	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)	Ratio (sec.)
24. Hoyt Avenue N. & 21st Street	EB-L	0.02 40.4 D	0.02 40.4 D	0.11 42.0 D	0.11 42.0 D	0.09 41.8 D	0.09 41.8 D
	EB-R	0.37 47.5 D	0.37 47.5 D	0.13 42.4 D	0.13 42.4 D	0.17 43.1 D	0.17 43.1 D
	WB-L	1.00 58.1 E	1.03 66.9 E *	0.77 41.0 D	0.81 42.9 D	0.73 40.1 D	0.82 43.7 D
	WB-TR	0.25 14.8 B	0.25 14.8 B	0.17 14.2 B	0.17 14.2 B	0.29 15.7 B	0.29 15.7 B
	NB-L	0.31 32.2 C	0.32 32.8 C	0.11 25.3 C	0.12 25.4 C	0.18 26.1 C	0.18 26.3 C
	NB-T	1.08 98.0 F	1.17 133.9 F *	0.78 43.5 D	0.83 47.3 D	1.12 101.6 F	1.17 123.0 F
	SB-TR	1.03 61.9 E	1.06 71.0 E *	0.58 33.6 C	0.60 34.2 C	0.78 39.9 D	0.81 41.6 D
25. Hoyt Avenue S./Astoria Park S.	EB-LTR	0.61 36.3 D	0.69 37.6 D	0.33 32.8 C	0.37 33.4 C	0.47 34.6 C	0.52 35.5 D
& 21st Street	NB-LTR	0.61 15.9 B	0.64 16.5 B	0.45 13.6 B	0.46 13.8 B	1.02 44.2 D	1.08 65.3 E
	SB-LTR	1.12 79.0 E	1.15 95.0 F *	0.65 16.9 B	0.68 17.5 B	1.00 45.2 D	1.08 70.3 E
26. 27th Avenue & 9th Street	EB-LT	0.01 8.2 A	0.01 8.6 A	0.00 7.8 A	0.00 8.2 A	0.01 7.9 A	0.01 8.9 A
(Unsignalized-Two Way Stop)	SB-LR	0.34 15.3 C	1.43 232.7 F *	0.33 12.1 B	0.73 27.4 D	0.33 14.2 B	1.36 210.9 F
27. Vernon Boulevard & 31st Avenue	WB-LR	0.58 29.7 D	0.64 34.6 D	0.23 16.4 C	0.26 17.2 C	0.44 23.4 C	0.51 27.7 D
(Unsignalized-Two Way Stop)	SB-LT	0.02 8.2 A	0.02 8.2 A	0.03 8.0 A	0.03 8.1 A	0.02 8.6 A	0.02 8.8 A
28. Vernon Boulevard & Broadway/	EB-LTR	0.01 28.2 C	0.01 28.2 C	0.02 26.1 C	0.02 26.1 C	0.03 33.2 C	0.03 33.2 C
11th Street	WB-LTR	1.13 99.5 F	1.17 115.9 F *	0.96 55.7 E	1.01 68.8 E *	0.97 69.3 E	1.08 99.5 F
	NB (Vernon Blvd)-LT	0.26 8.0 A	0.27 8.1 A	0.27 8.4 A	0.28 8.5 A	0.48 9.5 A	0.49 9.7 A
	NB (Vernon Blvd)-R	0.11 6.8 A	0.11 6.8 A	0.20 7.8 A	0.20 7.8 A	0.18 6.7 A	0.18 6.7 A
	NB (11th Street)-LTR	0.38 41.1 D	0.38 41.1 D	0.22 32.8 C	0.22 32.8 C	0.33 38.2 D	0.33 38.2 D
	SB-LTR	1.08 80.8 F	1.22 136.6 F *	0.58 27.9 C	0.62 29.2 C	0.66 30.7 C	0.75 34.6 C
29. 31st Avenue & 21st Street	EB-LTR	0.67 45.6 D	0.70 47.3 D	0.34 34.5 C	0.38 35.4 D	0.50 35.0 D	0.54 36.3 D
	WB-LTR	0.58 41.1 D	0.61 42.0 D	0.42 35.9 D	0.45 36.7 D	0.42 32.4 C	0.45 33.2 C
	NB-TR	0.49 14.0 B	0.50 14.2 B	0.63 16.8 B	0.65 17.1 B	0.77 23.2 C	0.79 24.1 C
	SB-TR	0.86 25.0 C	0.89 26.8 C	0.57 15.5 B	0.57 15.8 B	0.65 19.7 B	0.66 20.1 C

#### Table 13-26 (continued): Alternate 2023 Future Weekday With-Action Condition-LOS at Analyzed Intersections

#### Notes:

 $EB\text{-}East bound, \, WB\text{-}West bound, \, NB\text{-}North bound, \, SB\text{-}South bound$ 

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a significant adverse impact.

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version 5.5)

This table has been updated for the FEIS.

Peak		Total Width	Effective Width	Peak 15-Minute Volumes		Surging Factor		Friction	V/C	
Hour	Stairway	(feet)	(feet)	Up	Down	Up	Down	Factor	Ratio	LOS
	S3-M3 (northwest)	5.0	4.0	196	60	1.0	0.8	0.9	0.50	В
AM	P1-P2 (southwest)	5.0	4.0	482	10	1.0	0.75	1.0	0.83	С
	P5-P6 (northwest)	5.0	4.0	344	3	1.0	0.75	1.0	0.58	В
	S3-M3 (northwest)	5.0	4.0	53	143	1.0	0.8	0.9	0.43	А
PM	P3-P4 (southeast)	5.0	4.0	6	300	1.0	0.75	1.0	0.68	В
	P7-P8 (northeast)	5.0	4.0	6	237	1.0	0.75	1.0	0.54	В

Table 13-27: 2012 Existing Subway Stair Analysis

Notes: Methodology based on *CEQR Technical Manual* guidelines; Volumes based on data collected in October 2012, June 2013, and March 2014.

Peak			Control		15-M	eak Iinute umes		ging ctor	Friction	V/C	
Hour	Station	Direction	Element	Quantity	In <sup>1</sup>	Out <sup>2</sup>	In <sup>1</sup>	Out <sup>2</sup>	Factor	Ratio	LOS
AM	30th	Northbound	Two-way Turnstile	3	32	113	1.0	0.8	0.9	0.11	А
Alvi	Avenue	Southbound	Two-way Turnstile	3	826	13	1.0	0.8	1.0	0.66	В
PM	30th	Northbound	Two-way Turnstile	3	12	537	1.0	0.8	1.0	0.36	А
PIVI	Avenue	Southbound	Two-way Turnstile	3	218	13	1.0	0.8	0.9	0.20	А

 Table 13-28: 2012 Existing Subway Fare Array Analysis

**Notes:** Methodology based on *CEQR Technical Manual* guidelines; volumes based on data collected in October 2012 and June 2013.

<sup>1</sup> "In" refers to system entries.

<sup>2</sup> "Out" refers to system exits.

Existing service levels for the analyzed station elements were determined using the peak 15-minute volumes developed from stair usage and fare array counts conducted on October 18, 2012, June 12, 2013, and March 13, 2014.

As shown in Table 13-27 and Table 13-28, all analyzed subway station elements currently operate at LOS C or better during the weekday AM and PM peak hours.

#### Line Haul

Line haul is the volume of transit riders passing a defined point on a given transit route. For subway routes in New York City to and from Queens, line haul is typically measured either at East River bridge and tunnel crossings or at the actual maximum load point on each subway route (the point where the trains carry the greatest number of passengers during the peak hour). 2011 and 2012 maximum load point ridership for the F, N, and Q subway lines were provided by NYCT. As shown in Table 13-29, the maximum load points for the F line are the Roosevelt Island and Lexington Avenue/63<sup>rd</sup> Street Stations in the <u>weekday</u> AM and PM peak hours, respectively; the maximum load points for the N and Q lines are the Queensboro Plaza and Lexington Avenue/59<sup>th</sup> Street Stations in the <u>weekday</u> AM and PM peak hours, respectively. The peak direction of travel for these lines is Manhattan-bound in the <u>weekday</u> AM peak hour and Queens-bound in the <u>weekday</u> PM peak hour.

Route	Peak Direction	Maximum Load Point (leaving station)	Average Trains per hour	Cars per hour	Peak Hour Capacity <sup>1</sup>	Passengers per hour	V/C Ratio				
Weekday AM Peak Hour											
F	Manhattan- bound	Roosevelt Island	15.1	151	21,895	18,001	0.82				
Ν	Manhattan- bound	Queensboro Plaza	7.8	78	11,310	10,260	0.91				
Q	Manhattan- bound	Queensboro Plaza	7.6	76	11,020	10,168	0.92				
		Weekd	ay PM Pea	k Hour							
F	Queens- bound	Lexington Av/63 St	15.0	150	21,750	16,964	0.78				
N	Queens- bound	Lexington Av/59 St	7.4	74	10,730	6,496	0.61				
Q	Queens- bound	Lexington Av/59 St	6.6	66	9,570	5,499	0.57				

### Table 13-29: Existing Subway Line Haul Conditions

Source: NYCT (2011 and 2012)

Notes:

<sup>1</sup> Capacity based on NYCT guideline capacity of 145 passengers per car for 60' cars.

The line haul analysis presented in Table 13-29 focuses on the peak direction of travel in each hour. Existing conditions for each subway route are reported in terms of a v/c ratio, which is determined by dividing the number of peak hour passengers traveling through the maximum load point by the line haul capacity provided. Line haul capacity is based on the practical capacity per subway car multiplied by the number of subway cars crossing the maximum point in the peak hour. As shown in Table 13-29, no subway route is currently operating at or above capacity (a v/c ratio equal to or greater than 1.00) in either peak hour based on the NYCT 2011 and 2012 ridership data. V/c ratios in the <u>weekday</u> AM peak hour are higher than in the <u>weekday</u> PM peak hour, as peak demand is typically more concentrated in the AM. F trains typically carry the highest number of passengers with 18,001 Manhattan-bound riders in the AM peak hour and 16,964 Queens-bound riders in the PM. However, due to the lower existing peak hour capacity of the N and Q subway lines, the v/c ratios for these lines are slightly higher than the F line v/c ratio in the AM peak hour.

## Bus

As discussed previously, only the Q103 local bus route is expected to experience 50 or more new peak hour trips in one direction and therefore requires a detailed analysis pursuant to *CEQR Technical Manual* guidelines. The Q103 provides weekday-only service between a southern terminus at Vernon Boulevard and Borden Avenue in Long Island City and a northern terminus at  $27^{\text{th}}$  Avenue and  $2^{\text{nd}}$  Street, in close proximity to the project site (see Figure 13-6). The weekday operating hours are approximately 5:30 AM – 8:00 PM.

Table 13-30 shows the existing number of buses and ridership at the maximum load point in each direction for the analyzed Q103 in the <u>weekday</u> AM and PM peak hours. As shown in Table 13-30, the Q103 route currently operates with available capacity during both the AM and PM peak hours. The average number of peak hour passengers per bus ranges from 11 on the southbound Q103 in the PM to 39 on the southbound Q103 in the AM.

Peak Hour	Route	Direction	Maximum Load Point	Peak Hour Buses	Peak Hour Passengers	Average Passengers per Bus	Available Capacity <sup>1</sup>
		NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	2	36	18	72
AM	Q103	SB	Vernon Boulevard & 31 <sup>st</sup> Avenue	2	78	39	30
PM	Q103	NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	3	42	14	120
1 1/1	×105	SB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	3	33	11	129

Table 13-30: 2012 Existing Conditions Bus Line Haul Analysis

Notes:

<sup>1</sup>Available capacity based on NYCT loading guidelines of 54 passengers per standard bus.

## Future without the Proposed Action (No-Action Condition)

#### Subway

The results of the analyses of subway station stair and turnstiles at the 30<sup>th</sup> Avenue Station under the No-Action condition are shown in Tables 13-31 and 13-32, respectively. Estimates of peak hour volumes in the No-Action condition were developed by applying the *CEQR Technical Manual* recommended annual background growth rates to existing volumes and incorporating subway trips associated with large No-Action developments in the study area, such as the Halletts Point development, as well as the as-of-right No-Action development on the project site. New subway riders generated by smaller No-Action sites were accounted for in background growth. As shown in Tables 13-31 and 13-32, all analyzed subway station street stairs and fare arrays would operate at LOS C or better during the weekday AM and PM peak hours. As indicated in Table 13-31, the southwest platform stair (P1-P2) would deteriorate to LOS D during the weekday AM peak hour with a v/c ratio of 1.05. All other analyzed platform stairs would operate at LOS C.

Peak		Total Width	Effective Width	Peak 15-Minute Volumes		Surging Factor		Friction	V/C	
Hour	Stairway	(feet)	(feet)	Up	Down	Up	Down	Factor	Ratio	LOS
	S3-M3 (northwest)	5.0	4.0	233	122	1.0	0.8	0.9	0.71	С
AM	P1-P2 (southwest)	5.0	4.0	610	15	1.0	0.75	1.0	1.05	D
	P5-P6 (northwest)	5.0	4.0	466	6	1.0	0.75	1.0	0.79	С
	S3-M3 (northwest)	5.0	4.0	70	363	1.0	0.8	0.9	0.97	С
PM	P3-P4 (southeast)	5.0	4.0	12	410	1.0	0.75	1.0	0.93	С
	P7-P8 (northeast)	5.0	4.0	11	345	1.0	0.75	1.0	0.79	С

 Table 13-31: 2023 No-Action Subway Stair Analysis

Notes: Methodology based on *CEQR Technical Manual* guidelines; volumes based on data collected in October 2012, June 2013, and March 2014, annual background growth rates, the *Halletts Point Rezoning FEIS*, and projected No-Action project site development.

Table 13-33 shows the anticipated line haul conditions at the maximum load points on subway routes serving the project site in the 2023 future without the Proposed Action. The data in Table 13-33 reflects background growth and the addition of demand from the nearby Halletts Point development, based on the subway assignment presented in the 2013 *Halletts Point Rezoning FEIS*. As under existing conditions, no subway routes are expected to be operating over capacity in either analyzed peak hour in the 2023 No-Action condition, and F trains would remain the most utilized of the three analyzed subway lines, with 18,948 Manhattan-bound passengers in the AM peak hour and 17,852 Queens-bound passengers in the PM peak hour. V/c ratios would increase in the 2023 No-Action condition, with the highest v/c ratio

(0.99) anticipated on the Manhattan-bound Q line in the AM peak hour (compared to 0.92 under existing conditions).

					<b>15-M</b> i	Peak 15-Minute Volumes		inute Surging				
Peak Hour	Station	Direction	Control Element	Quantity	In <sup>1</sup>	Out <sup>2</sup>	In <sup>1</sup>	Out <sup>2</sup>	Friction Factor	V/C Ratio	LOS	
AM	30th	Northbound	Two-way Turnstile	3	52	173	1.0	0.8	0.9	0.17	А	
AM	Avenue	Southbound	Two-way Turnstile	3	1,076	21	1.0	0.8	1.0	0.87	С	
РМ	30th	Northbound	Two-way Turnstile	3	23	755	1.0	0.8	1.0	0.51	В	
PIVI	Avenue	Southbound	Two-way Turnstile	3	336	31	1.0	0.8	0.9	0.32	А	

 Table 13-32: 2023 No-Action Subway Fare Array Analysis

**Notes:** Methodology based on *CEQR Technical Manual* guidelines; volumes based on data collected in October 2012 and June 2013, annual background growth rates, the *Halletts Point Rezoning FEIS*, and projected No-Action project site development.

<sup>1</sup> "In" refers to system entries.

<sup>2</sup> "Out" refers to system exits.

Route	Peak Direction	Maximum Load Point (leaving station)	Average Trains per hour	Cars per hour	Peak Hour Capacity <sup>1</sup>	No-Action Passengers per Hour	V/C Ratio
		Weekd	ay AM Pea	k Hour			
F	Manhattan- bound	Roosevelt Island	15.1	151	21,895	18,959	0.87
Ν	Manhattan- bound	Queensboro Plaza	7.8	78	11,310	11,022	0.97
Q	Manhattan- bound	Queensboro Plaza	7.6	76	11,020	10,926	0.99
		Weekd	ay PM Pea	k Hour			
F	Queens- bound	Lexington Av/63 St	15	150	21,750	17,862	0.82
Ν	Queens- bound	Lexington Av/59 St	7.4	74	10,730	7,076	0.66
Q	Queens- bound	Lexington Av/59 St	6.6	66	9,570	6,037	0.63

#### Table 13-33: 2023 No-Action Subway Line Haul Conditions

Source: NYCT (2011 and 2012)

Notes:

<sup>1</sup> Capacity based on NYCT guideline capacity of 145 passengers per car for 60' cars.

## Bus

The result of the analysis of the Q103 bus route under No-Action conditions is shown in Table 13-34. Estimates of peak hour volumes in the No-Action condition were developed by applying the *CEQR Technical Manual* recommended annual background growth rates to existing volumes and incorporating bus trips associated with larger No-Action developments in the study area, such as Halletts Point, as well as the No-Action as-of-right residential development on the project site. As shown in Table 13-34, existing levels of bus service would not be sufficient to provide adequate supply to meet the projected

demand in the 2023 No-Action condition on the northbound and southbound Q103 route in the <u>weekday</u> AM and PM peak hours. This route would require additional capacity, which could be provided by either increasing the number of standard buses or converting the Q103 route to articulated bus service. As shown in Table 13-34, based on a loading guideline of 54 passengers per standard bus, one additional standard bus per hour would need to be added in the northbound direction in the AM peak hour, as well as three additional buses in the PM peak hour to accommodate projected <u>weekday</u> No-Action demand. In the southbound direction, five buses would need to be added in the AM peak hour and one in the PM peak hour.

						Condition with Service Levels		No-Action Condition with Potential Service Adjustments			
Peak Hour	Route	Direction	Maximum Load Point	2023 Peak Hour Passengers	Peak Hour Buses	Average Passengers per Bus	Available Capacity <sup>1</sup>	Peak Hour Buses <sup>2</sup>	Average Passengers per Bus	Available Capacity <sup>1</sup>	
		NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	113	2	57	-5	3	38	49	
АМ	Q103	SB	Vernon Boulevard & 31 <sup>st</sup> Avenue	369	2	185	-261	7	53	9	
PM	0102	NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	314	3	105	-152	6	52	10	
FIVI	Q103	SB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	190	3	64	-28	4	48	26	

 Table 13-34: 2023 No-Action Condition Bus Line Haul Analysis

Note:

<sup>1</sup> Available capacity based on NYCT loading guidelines of 54 passengers per standard bus.

<sup>2</sup> Assumes service levels adjusted to address capacity shortfalls during the 2012 through 2023 period.

## Future with the Proposed Action (With-Action Condition)

#### Subway

As shown earlier in Table 13-7, the Proposed Action is expected to generate a net total of 705 and 823 new subway trips in the <u>weekday</u> AM and PM peak hours, respectively. As discussed above, based on current station usage, the proximity to the project site, and the proposed shuttle service that would be provided to the 30<sup>th</sup> Avenue Station, 80 percent of project-generated subway trips are expected to use the 30<sup>th</sup> Avenue Station and were assigned to the analyzed stair and fare arrays. As shown in Table 13-35, 173 and 266 new subway riders would use street stair S3-M3. During the AM peak hour, platform stairs P1-P2 and P5-P6 would each experience approximately 65 and 64 new peak 15-minute trips, respectively, while during the PM peak hour, platform stairs P3-P4 and P7-P8 would each experience an increase of approximately 63 and 62 peak 15-minute trips, respectively. Pedestrian peak 15-minute traffic flows would increase by 47 and 125 trips at the northbound fare array in the <u>weekday</u> AM and PM peak hours, respectively, as shown in Table 13-36. The southbound fare array would experience 129 and 81 new trips as a result of the Proposed Action in the <u>weekday</u> AM and PM peak hours, respectively.

As shown in Table 13-35, street stair S3-M3 would deteriorate from LOS C conditions in both peak hours under the No-Action condition to LOS D and LOS E in the <u>weekday</u> AM and PM peak hours in the future with the Proposed Action, due to the anticipated pedestrian volumes at this stair from the adjacent bus stop and proposed shuttle stop. As the resultant WIT in the AM peak hour (6.14 inches) would be less than the CEQR threshold for a significant impact (seven inches), no significant adverse impact would result during this peak analysis hour. As the resultant WIT at street stair S3-M3 during the PM peak hour

(20.01 inches) would exceed the CEQR impact threshold of four inches, a significant adverse impact would result. Potential mitigation measures are discussed in Chapter 20, "Mitigation."

Peak		Total Width	Effective Width	Pr	15-MinutePeakProject15-MinuteIncrementVolumesS		Surging Factor <sup>1</sup>		Friction	Friction V/C		WIT	WIT Impact Threshold	
Hour	Stairway	(feet)	(feet)	Up	Down	Up	Down	Up	Down	Factor	Ratio	LOS	(in.)	(in.)
	S3-M3 (northwest)	5.0	4.0	134	39	367	161	0.9	0.8	0.9	1.13	D	6.14	7
AM	P1-P2 (southwest)	5.0	4.0	63	2	673	17	0.95	0.75	1.0	1.22	D	4.99	6
	P5-P6 (northwest)	5.0	4.0	63	1	529	7	0.95	0.75	1.0	0.94	С	N/A	N/A
	S3-M3 (northwest)	5.0	4.0	64	130	134	493	0.9	0.8	0.9	1.42	Е	20.01	4
PM	P3-P4 (southeast)	5.0	4.0	3	60	15	470	0.95	0.75	1.0	1.07	D	3.40	8
	P7-P8 (northeast)	5.0	4.0	3	59	14	404	0.95	0.75	1.0	0.92	С	N/A	N/A

 Table 13-35: 2023 With-Action Subway Stair Analysis

**Note:** Methodology based on *CEQR Technical Manual* guidelines; volumes based on data collected in October 2012, June 2013, and March 2013, annual background growth rates, the *Halletts Point Rezoning FEIS*, projected No-Action project site development, and the With-Action project increment.

N/A – not applicable because the With-Action v/c ratio is smaller than 1.00.

<sup>1</sup>Surging factors adjusted to account for potential surge from the proposed shuttle bus, per NYCT guidance.

Peak			Control		Pro	15-Minute Project Increment		Peak 15-Minute Volumes		Surging Factor <sup>3</sup>			
Hour	Station	Direction	Element	Quantity	In <sup>1</sup>	Out <sup>2</sup>	In <sub>1</sub>	Out <sup>2</sup>	In <sup>1</sup>	Out <sup>2</sup>	Friction Factor	V/C Ratio	LOS
AM	30th	Northbound	Two- way Turnstile	3	11	36	63	209	0.95	0.80	0.9	0.21	А
AM	Avenue	Southbound	Two- way Turnstile	3	126	3	1,202	24	0.95	0.80	1.0	1.02	D
PM	30th	Northbound	Two- way Turnstile	3	6	119	29	874	0.95	0.80	1.0	0.59	В
r IVI	Avenue	Southbound	Two- way Turnstile	3	70	11	406	42	0.95	0.80	0.9	0.41	А

#### Table 13-36: 2023 With-Action Subway Fare Array Analysis

Note: Methodology based on CEQR Technical Manual guidelines

<sup>1</sup> "In" refers to system entries.

<sup>2</sup> "Out" refers to system exits.

<sup>1</sup>Surging factors adjusted to account for potential surge from the proposed shuttle bus, per NYCT guidance.

No significant adverse impacts to the analyzed platform stairs would occur as a result of the Proposed Action. As indicated in Table 13-35, platform stair P5-P6 would operate at LOS C during the <u>weekday</u> AM and PM peak hours, respectively, and platform stair P1-P2 would continue to operate at LOS D during the AM peak hour, as under the No-Action condition. During the PM peak hour, platform stair P3-P4 would deteriorate from LOS C under No-Action conditions to LOS D in With-Action conditions, with a resultant v/c ratio of 1.07. As the WIT at platform stair P3-P4 would be 3.40 inches (less than the CEQR impact threshold of 8 inches), no significant adverse impact would result.

As shown in Table 13-36, the northbound fare array at the 30<sup>th</sup> Avenue Station would continue to operate at LOS B or better under the With-Action condition in both the AM and PM peak hours. In addition, the southbound far array would continue to operate at LOS A during the PM peak hour. As discussed above, the morning commuter rush hour results in heavy pedestrian volumes at the southbound fare array, which

would operate with a v/c ratio of 1.02 (LOS D) in the AM peak hour under With-Action conditions. As the Proposed Action would result in the southbound fare array deteriorating from a v/c ratio less than 1.0 (0.87) to a v/c ratio of 1.0 or greater (1.02) a significant adverse impact would result pursuant to CEQR. However, it should be noted that the fare array analysis conservatively assumes that all Manhattan-bound morning commuters would use the fare array closest to the <u>southbound</u> platform. If a portion of the anticipated morning commuters were to enter through the fare array that is closer to the <u>northbound</u> platform (which also provides access to the <u>southbound</u> platform), conditions at the <u>southbound</u> fare array would improve. Potential mitigation measures are discussed in Chapter 20, "Mitigation."

Table 13-37 compares the anticipated 2023 No-Action and With-Action line haul conditions of the F, N, and Q lines. As previously stated, the Proposed Action is expected to generate a net total of 705 and 823 new subway trips in the weekday AM and PM peak hours, respectively. 80 percent of these projectgenerated subway trips are expected to use the 30<sup>th</sup> Avenue Station (split evenly between the N and the Q lines), and the remaining 20 percent would travel via the F line. Anticipated origins/destinations were determined based on ACS data. As shown in Table 13-37, the F and N lines would operate below capacity in their peak directions in the AM and PM peak hours, and the Q line would operate below capacity in its peak direction in the PM peak hour. In the AM peak hour, Manhattan-bound Q trains would operate with a v/c ratio of 1.01, compared to a v/c ratio of 0.99 under No-Action conditions. However, pursuant to CEQR impact criteria, projected increases from a No-Action condition to a With-Action condition that exceeds practical capacity may be considered significant impacts if the proposed action generates five or more additional passengers per car. As shown in Table 13-37, the Proposed Action would generate less than three additional riders per car on the F, N, and Q lines in their peak directions in the AM and PM peak hours. As such, while Manhattan-bound Q trains are expected to operate over capacity in the AM peak hour in future With-Action conditions, since the Proposed Action would add only 2.66 additional riders per car, no significant adverse impact would result.

		Maximum				No-Action Condition		With-Ac	dition	
Route	Peak Direction	Load Point (leaving station)	Average Trains per hour	Cars per hour	Peak Hour Capacity	Passengers per hour	V/C Ratio	Passengers per hour	V/C Ratio	New riders per car
				Weekda	y AM Peak	Hour				
F	Manhattan -bound	Roosevelt Island	15.1	151	21,895	18,959	0.87	19,061	0.87	0.68
Ν	Manhattan -bound	Queensboro Plaza	7.8	78	11,310	11,022	0.97	11,224	0.99	2.59
Q	Manhattan -bound	Queensboro Plaza	7.6	76	11,020	10,926	0.99	11,128	1.01	2.66
				Weekd	ay PM Peak	Hour				
F	Queens- bound	Lexington Av/63 St	15	150	21,750	17,862	0.82	17,957	0.83	0.63
N	Queens- bound	Lexington Av/59 St	7.4	74	10,730	7,076	0.66	7,267	0.68	2.58
Q	Queens- bound	Lexington Av/59 St	6.6	66	9,570	6,037	0.63	6,228	0.65	2.89

Table 13-37: 2023 Subway Line Haul Analysis	-No-Action Condition vs. With-Action Condition

#### Bus

As shown earlier in Table 13-7, the Proposed Action is expected to generate 77 and 135 new bus trips during the weekday AM and PM peak hours, respectively. As shown in Table 13-38, demand on the

Q103 route is expected to increase by approximately 41 northbound trips and 126 southbound trips in the AM peak hour and by 128 northbound and 82 southbound trips in the PM peak hour. It should be noted that these trips include project-generated subway riders that are expected to utilize the Q103 bus route to transfer to/from the 21<sup>st</sup> Street-Queensbridge station.

Peak Hour	Route	Direction	Maximum Load Point	Peak Hour Buses <sup>1</sup>	No-Action Available Capacity <sup>2</sup>	Project Increment	With-Action Available Capacity <sup>1</sup>
		NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	3	49	40	9
AM			Vernon Boulevard & 31 <sup>st</sup> Avenue	7	9	127	-118
DM	0102	NB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	6	10	127	-117
PM	Q103	SB	40 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	4	26	81	-55

 Table 13-38: 2023 With-Action Condition Bus Line Haul Analysis

Note:

<sup>1</sup> Assumes service levels adjusted to address capacity shortfalls in the No-Action condition.

<sup>2</sup> Available capacity based on NYCT loading guidelines of 54 passengers per standard bus.

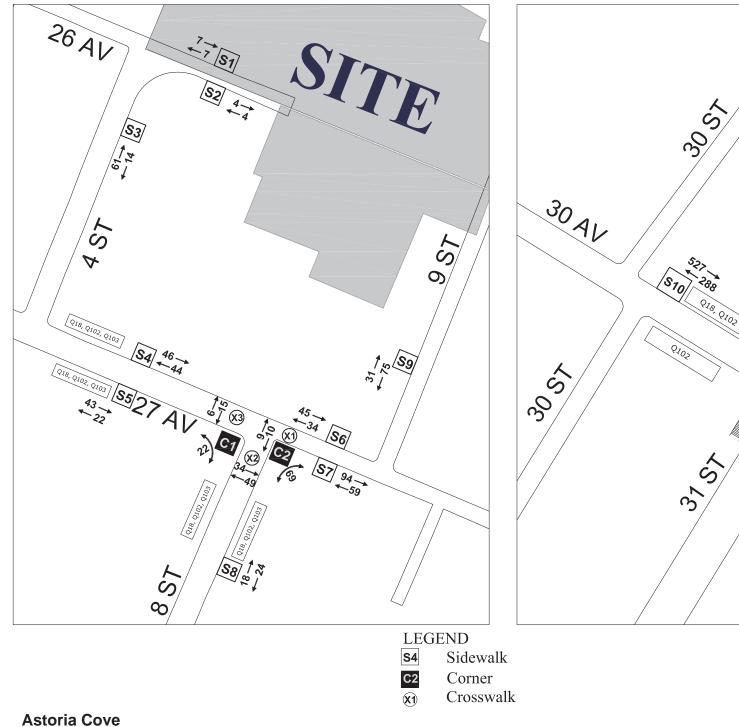
As shown in Table 13-38, based on projected levels of service in the No-Action condition, the Proposed Action would result in a capacity shortfall of 117 spaces on the northbound Q103 service in the PM peak hour. The southbound Q103 service would also experience capacity shortfalls of 118 spaces in the AM peak hour and 55 spaces in the PM peak hour. Therefore, significant adverse impacts are expected on the northbound Q103 in the PM peak hour and on the southbound Q103 in both the AM and PM peak hours, based on *CEQR Technical Manual* impact criteria. Q103 service would require additional capacity, which could be provided by either increasing the number of standard buses or converting the Q103 route to articulated bus service. Potential mitigation measures for these significant adverse bus impacts are discussed in Chapter 20, "Mitigation."

## I. PEDESTRIANS

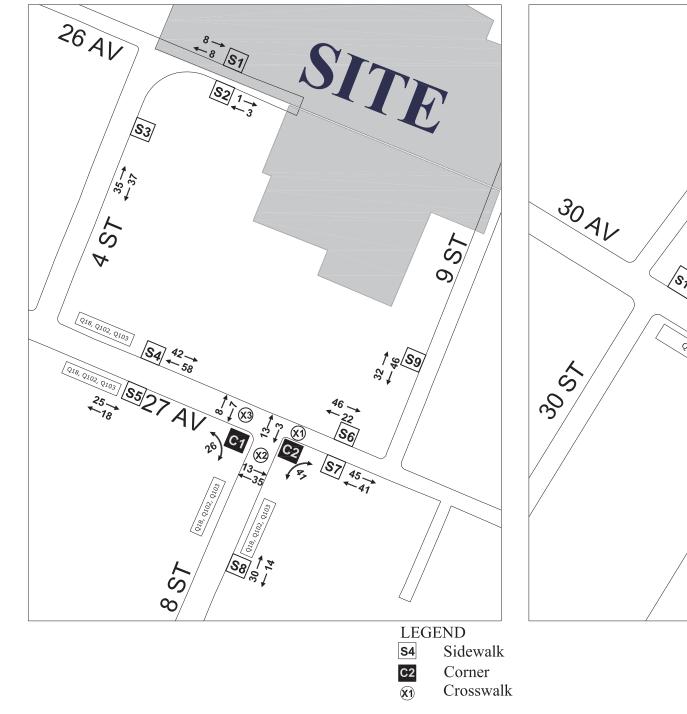
## **Existing Conditions**

As discussed previously in Section E, "Level 2 Screening Assessment," a total of 11 existing sidewalks, three corner areas, and one crosswalk where project-generated pedestrian trips are expected to exceed the 200-trip *CEQR Technical Manual* threshold in one or more peak hours have been selected for analysis. As shown in Figure 13-10, these analyzed existing pedestrian elements are primarily located along 26<sup>th</sup> and 27<sup>th</sup> Avenues in proximity to the project site as well as in the vicinity of the 30<sup>th</sup> Avenue subway station. Figures 13-27, 13-28, and 13-29 show the existing pedestrian volumes along the analyzed pedestrian elements for the weekday AM, midday, and PM peak hours, respectively. Tables 13-39 through 13-41 show existing average pedestrian space (in square feet per pedestrian) and LOS at analyzed sidewalks, corners, and crosswalks, respectively. Peak 15-minute volumes are also provided for all analyzed sidewalks and corner locations.

As shown below in Tables 13-39, 13-40, and 13-41, all analyzed pedestrian elements are currently operating at LOS C or better, which is attributable to the currently underdeveloped character of the study area and wide sidewalks along the major corridors.



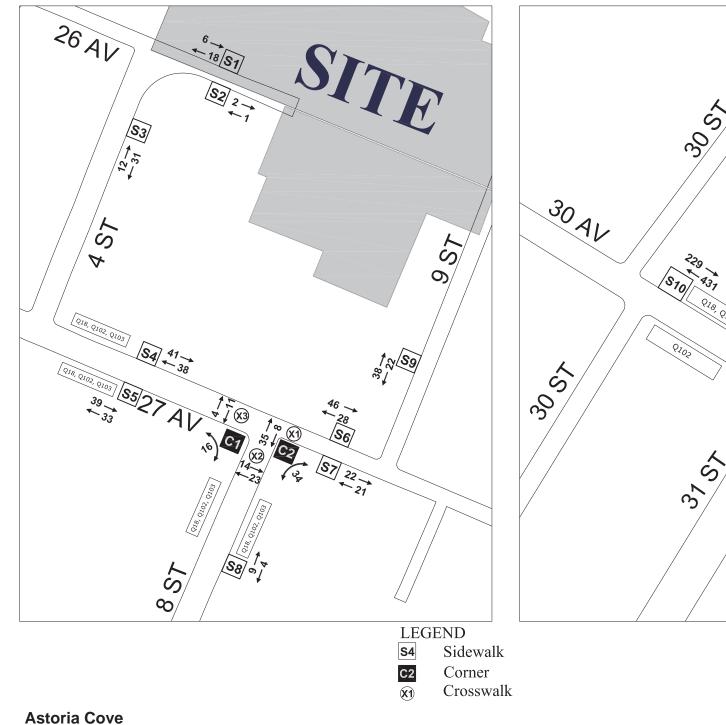
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Existing Weekday Midday Peak Hour Pedestrian Volumes



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		Effective Width		k 15-Mi Volume		Averag	Platoon-Adjusted Level of Service				
No.	Location	(feet)	AM	MD	PM	AM	MD	PM	AM	MD	PM
S1	26 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (north)	11.0	5	5	12	6930.0	6930.0	2,887.5	А	А	А
S2	26 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (south)	12.0	3	2	1	12663.0	18900.0	3,800.0	А	А	А
S3	4 <sup>th</sup> Street between 26 <sup>th</sup> Avenue & 27 <sup>th</sup> Avenue (east)	12.0	22	30	18	1713.6	1260.0	2,109.8	А	А	А
S4	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (north)	6.5	33	33	25	530.4	533.5	702.0	А	А	А
S5	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (south)	5.5	19	13	27	785.9	1146.5	552.7	А	А	А
S6	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (north)	3.5	35	28	24	267.9	339.0	393.3	В	В	В
S7	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (south)	7.5	48	25	15	423.5	810.0	1,356.3	В	А	А
S8	8 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & Astoria Boulevard (east)	7.5	42	18	10	482.1	1122.9	2056.1	В	А	А
S9	9 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & the water (west)	7.0	43	23	16	515.8	961.1	1381.8	В	А	А
S10	30 <sup>th</sup> Avenue between 30 <sup>th</sup> Street & 31 <sup>st</sup> Street (north)	9.5	287	139	179	89.1	184.4	142.8	С	В	В
S11	31 <sup>st</sup> Street between 30 <sup>th</sup> Avenue & Newtown Avenue (west)	10.5	147	113	213	192.9	251.9	133.1	В	В	В

 Table 13-39: 2012 Existing Conditions Sidewalk Analysis

Notes: Methodology based on CEQR Technical Manual guidelines.

## Table 13-40: 2012 Existing Conditions Corner Analysis

		Curb Radius	Average Pedestrian Space (ft <sup>2</sup> /ped)			Lev	vel of Ser	vice
No.	Location	(feet)	AM	MD	PM	AM	MD	PM
C1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southwest)	12.0	925.2	1262.0	1545.6	А	А	А
C2	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southeast)	12.0	601.2	1036.6	684.0	А	А	А
C3	30 <sup>th</sup> Avenue & 31 <sup>st</sup> Street (northwest)	6.0	263.0	422.3	262.5	А	А	А

Notes: Methodology based on CEQR Technical Manual guidelines.

### Table 13-41: 2012 Existing Conditions Crosswalk Analysis

			k 15-Mi Volume			age Pede ace (ft²/p		Level of Service		
No.	Location	AM	MD	PM	AM	MD	PM	AM	MD	PM
X1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (east)	9	11	24	779.9	645.4	282.6	А	А	А

#### Future without the Proposed Action (No-Action Condition)

Estimates of peak hour volumes in the No-Action condition were developed by applying the *CEQR Technical Manual* recommended annual background growth rates to existing volumes and incorporating

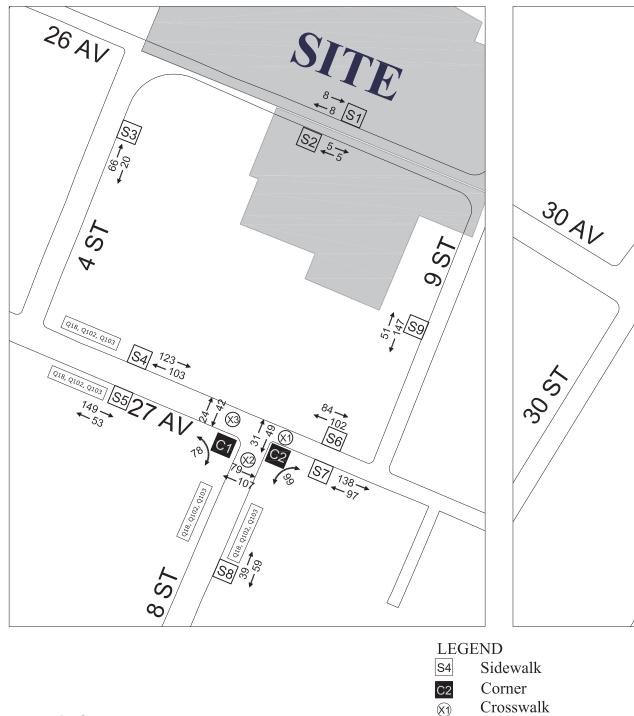
pedestrian trips associated with larger No-Action sites such as the Halletts Point development. New pedestrian trips generated by smaller No-Action sites were accounted for in the background growth. Figures 13-30, 13-31, and 13-32 show the resulting No-Action pedestrian volumes along the analyzed pedestrian elements for the weekday AM, midday, and PM peak hours, respectively. It should be noted that, as shown in Figures 13-30, 13-31, and 13-32, both the north and south sidewalks on 26<sup>th</sup> Avenue east of 4<sup>th</sup> Street would be extended to 9<sup>th</sup> Street in the 2023 No-Action condition.

Tables 13-42 through 13-44 show the forecasted No-Action average pedestrian space (square feet per pedestrian) and LOS along the analyzed sidewalks, corners, and crosswalks during the weekday AM, midday, and PM peak hours. Peak 15-minute volumes are also provided for all analyzed sidewalks and corner locations. As shown in the tables, all sidewalks would continue to operate at LOS C or better during each of the analyzed peak hours, while all analyzed corners and crosswalks would continue to operate at LOS A in all three peak hours under the No-Action condition.

		Effective Width	Peak 15-Minute Volumes			Average	n Space	Platoon-Adjusted Level of Service			
No.	Location	(feet)	AM	MD	PM	AM	MD	PM	AM	MD	PM
S1	$26^{th}$ Avenue between $4^{th}$ Street & $9^{th}$ Street (north) <sup>1</sup>	11.0	6	6	13	6063.7	6160.0	2665.4	А	А	А
S2	26 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 9 <sup>th</sup> Street (south) <sup>1</sup>	12.0	4	3	2	10130.4	12600.0	22680.0	А	А	А
S3	4 <sup>th</sup> Street between 26 <sup>th</sup> Avenue & 27 <sup>th</sup> Avenue (east)	12.0	25	33	21	1494.4	1134.0	1814.4	А	А	А
S4	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (north)	6.5	71	172	165	248.4	101.9	106.1	В	В	В
S5	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (south)	5.5	59	84	97	252.8	176.6	153.6	В	В	В
\$6	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (north)	3.5	53	83	93	162.4	114.3	101.6	В	В	В
S7	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (south)	7.5	73	75	74	275.7	268.9	273.3	В	В	В
S8	8 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & Astoria Boulevard (east)	7.5	31	63	53	661.2	319.1	378.9	А	В	В
S9	9 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & the water (west)	7.0	62	37	42	356.3	594.9	521.4	В	А	В
S10	30 <sup>th</sup> Avenue between 30 <sup>th</sup> Street & 31 <sup>st</sup> Street (north)	9.5	351	224	265	72.8	114.1	96.4	С	В	В
S11	31 <sup>st</sup> Street between 30 <sup>th</sup> Avenue & Newtown Avenue (west)	10.5	231	200	296	122.7	141.8	95.6	В	В	В

Notes: Methodology based on *CEQR Technical Manual* guidelines.

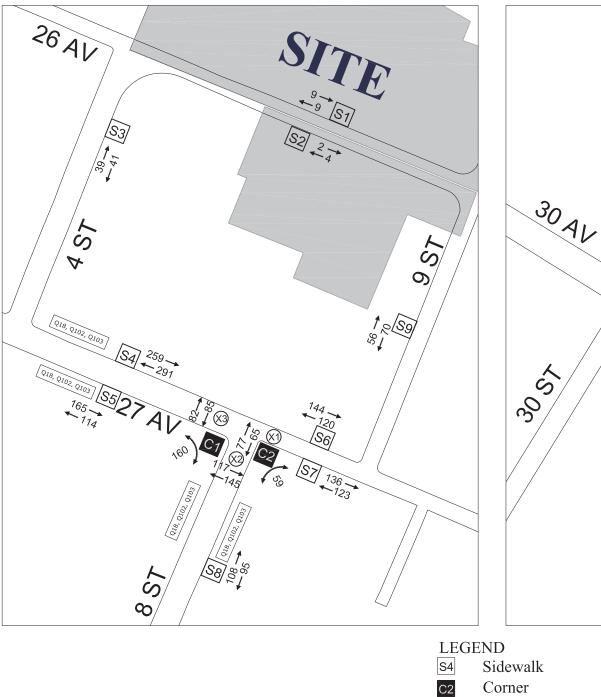
<sup>1</sup>Sidewalks would be extended to  $9^{\text{th}}$  Street under No-Action conditions.





Crosswalk

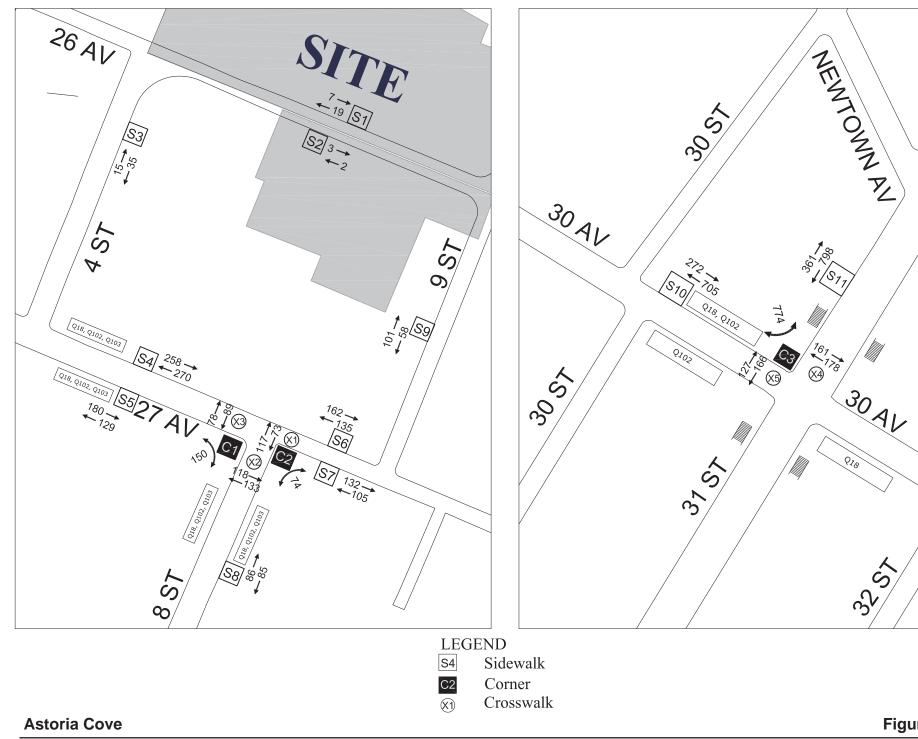
Astoria Cove





(x) Crosswalk

Astoria Cove



**Figure 13-32** 

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		Curb Radius	$(e_1^2)$			Lev	Level of Service				
No.	Location	(feet)	AM	MD	PM	AM	MD	PM			
C1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southwest)	12.0	399.5	228.2	236.5	А	А	А			
C2	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southeast)	12.0	359.3	283.5	250.0	А	А	А			
C3	30 <sup>th</sup> Avenue & 31 <sup>st</sup> Street (northwest)	6.0	198.1	284.1	195.0	А	А	А			

## Table 13-43: 2023 No-Action Condition Corner Analysis

Notes: Methodology based on CEQR Technical Manual guidelines.

#### Table 13-44: 2023 No-Action Condition Crosswalk Analysis

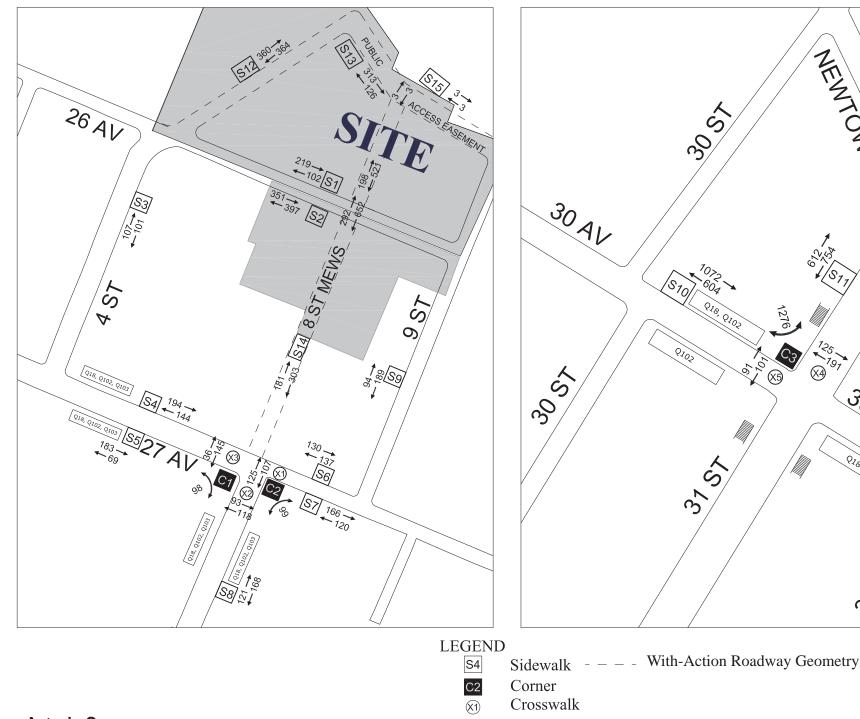
		Peak 15-Minute Volumes				age Pede ace (ft²/p		Level of Service			
No.	Location	AM	MD	PM	AM	MD	PM	AM	MD	PM	
X1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (east)	25	44	60	245.8	154.7	110.3	А	А	А	

## Future with the Proposed Action (With-Action Condition)

As discussed above in Section E, "Level 2 Screening Assessment," compared to the No-Action condition, the Proposed Action is expected to generate a net total of 1,635, 2,814, and 2,292 pedestrian trips (including walk-only, subway, and bus trips) during the weekday AM, midday, and PM peak hours, respectively. Pursuant to CEQR, passive open space typically generates 49 person trips per day per acre, while active open space typically generates 139 person trips per day per acre. Out of the total generated person trips, 80 percent are walk-only trips. Conservatively applying the higher trip generation rate for active open space, a maximum of 267 person trips per day are anticipated, which would result in approximately 214 pedestrian trips along the waterfront esplanade distributed throughout the day.

The assignment of these trips to the analyzed pedestrian elements is shown above in Figures 13-8, 13-9, and 13-10. The incremental pedestrian volumes were added to the projected No-Action volumes (see Figures 13-30, 13-31, and 13-32) to develop the With-Action pedestrian volumes for analysis. Figures 13-33, 13-34, and 13-35 show the With-Action pedestrian volumes for the weekday AM, midday, and PM peak hours, respectively.

As described above in Section G, "Traffic," there are several roadway network and traffic circulation improvements that are included in the Proposed Action. These measures would result in new pedestrian elements along the proposed extension of 4<sup>th</sup> Street north of 26<sup>th</sup> Avenue, as well as along the proposed waterfront public access easement, which would provide a connection along the waterfront between 4<sup>th</sup> and 9<sup>th</sup> Streets. Additionally, the proposed 8<sup>th</sup> Street Mews would provide a pedestrian connection between 27<sup>th</sup> Avenue to the south and the public access easement along the waterfront to the north. Out of these new pedestrian elements, which are shown in Figures 13-33, 13-34, and 13-35, those that are expected to experience the highest concentration of project-generated pedestrian trips were selected as additional analysis locations to determine if they could accommodate the anticipated project-generated demand. As shown in Table 13-45 the additional future pedestrian analysis locations are the following: the west sidewalk along 4<sup>th</sup> Street between 26<sup>th</sup> Avenue and the public access (S12); the south sidewalk along the public access easement between 4<sup>th</sup> Street and the 8<sup>th</sup> Street Mews (S13); the 8<sup>th</sup> Street Mews south of 26<sup>th</sup> Avenue (S14), where the narrowest point would be located; and the waterfront esplanade north of the public access easement (S15). As no new signalized intersections would be created



**Figure 13-33** 

## With-Action AM Peak Hour Pedestrian Volumes

NEWTOWN AV

70>

Q18, Q102

1276

C3

8

101 101

125

×197 (A)

30 AV

3

9<sub>18</sub>

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## Astoria Cove

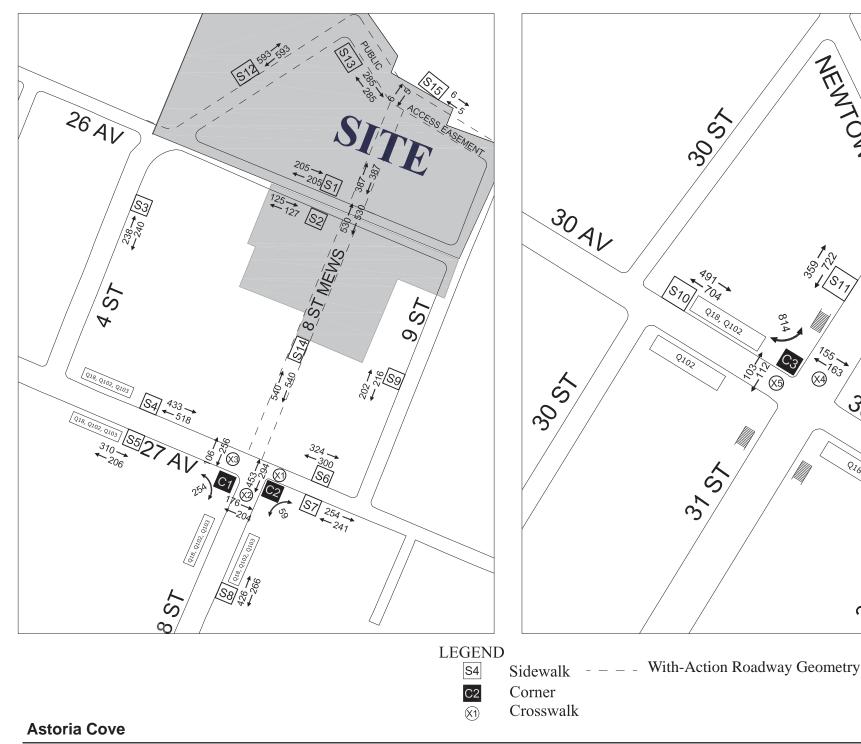


Figure 13-34

NEWTOWN AV

<sup>350</sup>

155

×3 ×1 ×4

30AV

3

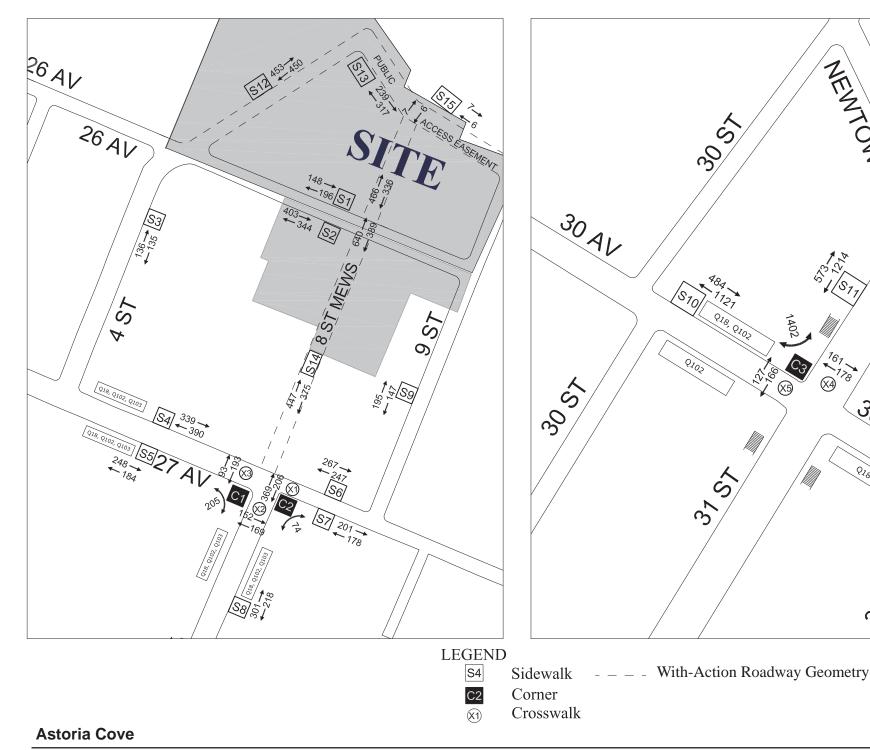
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1<sub>61</sub>

×1 ×1 ×1 ×8

30AV

9<sub>18</sub>

1402

C3

85

Lo Co

on the project site as part of the Proposed Action, a detailed pedestrian analysis of the new crosswalk elements on the project site is unwarranted, pursuant to CEQR.

		Effective		linute P			Peak 15-Minute Volumes			Flow Rate (PMF)	e	Platoon-Adjusted Level of Service			
No.	Location	Width (feet)	AM	MD	PM	AM	MD	PM	AM	MD	PM	AM	MD	PM	
S1	26 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (north)	11.0	94	122	95	100	128	108	345.3	270.3	322.2	В	В	В	
S2	26 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (south)	12.0	230	76	231	234	79	233	161.5	479.9	161.7	В	В	В	
S3	4 <sup>th</sup> Street between 26 <sup>th</sup> Avenue & 27 <sup>th</sup> Avenue (east)	12.0	36	116	64	61	149	85	617.8	252.9	446.3	А	В	А	
S4	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (north)	6.5	35	125	63	106	297	228	166.0	58.6	76.7	В	С	С	
S5	27 <sup>th</sup> Avenue between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street (south)	5.5	14	71	38	73	155	135	202.6	95.3	109.8	В	В	В	
S6	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (north)	3.5	25	112	68	83	195	161	113.0	47.9	58.4	В	С	С	
S7	27 <sup>th</sup> Avenue between 8 <sup>th</sup> Street & 9 <sup>th</sup> Street (south)	7.5	16	69	44	89	144	118	226.5	140.5	170.8	В	В	В	
S8	8 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & Astoria Boulevard (east)	7.5	59	153	109	90	216	162	224.1	93.4	124.7	В	В	В	
S9	9 <sup>th</sup> Street between 27 <sup>th</sup> Avenue & the water (west)	7.0	26	86	49	88	123	91	249.2	179.2	242.3	В	В	В	
S10	30 <sup>th</sup> Avenue between 30 <sup>th</sup> Street & 31 <sup>st</sup> Street (north)	9.5	173	104	171	524	328	436	48.5	77.8	58.4	С	С	С	
S11	31 <sup>st</sup> Street between 30 <sup>th</sup> Avenue & Newtown Avenue (west)	10.5	157	107	160	388	307	456	72.7	92.0	61.8	С	В	С	
S12	4 <sup>th</sup> Street between 26 <sup>th</sup> Avenue & the public access easement (west)	7.5	226	371	282	226	371	282	104.1	63.2	83.8	В	С	С	
S13	Public access easement between 4 <sup>th</sup> Street & 8 <sup>th</sup> Street Mews (south)	9.0	137	178	174	137	178	174	206.5	158.9	163.0	В	В	В	
S14	8 <sup>th</sup> Street Mews south of 26 <sup>th</sup> Avenue	6.0	151	338	257	151	338	257	124.7	55.4	73.1	В	С	С	
S15 <sup>1</sup>	Waterfront esplanade walkway/public access easement (north)	9.0	137	178	174	137	178	174	206.5	158.9	163.0	В	В	В	

Table 13-45: 2023 With-	Action Condition	Sidewalk Analysis
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**Notes:** Methodology based on *CEQR Technical Manual* guidelines. <sup>1</sup> For conservative analysis purposes, the higher S13 pedestrian volumes have been analyzed on the S15 sidewalk.

Tables 13-45 through 13-47 show the With-Action average pedestrian space and LOS along the analyzed sidewalks, corners, and crosswalks during the weekday AM, midday, and PM peak hours. Peak 15-minute project increments and peak 15-minute total With-Action pedestrian volumes are also provided for all analyzed sidewalks and corner locations. As shown in Table 13-45, all sidewalks and crosswalks, including the pedestrian elements that would be created as part of the proposed <u>project</u>, would operate at LOS C or better during each of the analyzed peak hours, while all analyzed corners would operate at LOS A in the future with the Proposed Action during each of the analyzed peak hours. Therefore, no significant adverse impacts would occur along the analyzed sidewalks, corners, and crosswalks during any of the peak hours.

		Curb Radius	Aver Sr	age Peder bace (ft²/p	strian ed)	Lev	el of Ser	vice
No.	Location	(feet)	AM	MD	PM	AM	MD	PM
C1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southwest)	12.0	267.8	132.7	163.6	А	А	А
C2	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (southeast)	12.0	235.9	98.6	123.7	А	А	А
C3	30 <sup>th</sup> Avenue & 31 <sup>st</sup> Street (northwest)	6.0	144.7	202.2	134.7	А	А	А

 Table 13-46: 2023 With-Action Condition Corner Analysis

Table 13-47: 2023 With-Action Condition Crosswalk Analysis

			inute P			k 15-Mi Volume		Pede	Average strian S (ft²/ped)	Space	Level of Service			
No.	Location	AM	MD	PM	AM	MD	PM	AM	MD	PM	AM	MD	PM	
X1	27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street (east)	47	190	119	72	234	179	83.0	27.0	34.4	А	С	С	

## J. PEDESTRIAN AND VEHICULAR SAFETY EVALUATION

Under *CEQR Technical Manual* guidelines, an evaluation of pedestrian and vehicular safety is needed for locations within the traffic and pedestrian study areas that have been identified as high accident locations. These locations are defined as locations where 48 or more total reportable and non-reportable crashes or five or more pedestrian/bicyclist injury crashes have occurred in any consecutive 12 months of the most recent three-year period for which data are available.<sup>3</sup>

Table 13-48 shows summary accident data for the years 2010 through 2012 that were obtained from the NYCDOT. This is the most recent three-year period for which data are available. The table shows the total number of crashes each year and the numbers of crashes each year involving pedestrians and cyclists at intersections in proximity to the project site where the majority of new vehicular and pedestrian trips would be concentrated. As shown in Table 13-48, no intersections were found to have experienced a total of 48 or more crashes or to have experienced five or more pedestrian and/or bicyclist injury crashes in one or more years; therefore, none of the intersections are considered high accident locations. As also shown in Table 13-48, none of the intersections exceeded one pedestrian and/or bicyclist injury crash in one or

<sup>&</sup>lt;sup>3</sup> Reportable accidents are defined as those involving injuries, fatalities, and/or \$1,000 or more in property damage.

more years. Therefore, based on the accident data presented in Table 13-48, no safety problems are anticipated.

		Pedestrian Injury Accidents		Bicycle Injury Accidents			Inju	Total trian/Bi ry Accid	lents	Total Accidents (Reportable + Non- Reportable			
Intersection	1	2010	2011	2012	2010	2011	2012	2010	2011	2012	2010	2011	2012
	21st Street	0	0	0	0	0	0	0	0	0	0	5	0
Hoyt Avenue North at	29th Street	0	0	0	0	0	0	0	0	0	0	0	0
Hoyt Avenue North at	31st Street	0	0	0	0	0	0	0	0	0	5	10	2
	32nd Street	0	0	0	0	0	0	0	0	0	2	0	0
Astoria Park S. / Hoyt Avenue S. at	21st Street	0	0	1	1	0	0	1	0	1	5	0	5
26th Avenue at	4th Street	0	0	0	0	0	0	0	0	0	0	0	0
	4th Street	0	0	0	0	0	0	0	0	0	0	0	1
	8th Street	0	0	0	0	0	0	0	0	0	0	0	1
27th Avenue at	9th Street	0	0	0	0	0	0	0	0	0	0	0	0
27th Avenue at	12 Street	0	0	0	0	0	0	0	0	0	0	0	0
	14th Street	0	0	0	0	0	0	0	0	0	0	0	0
	18th Street	0	0	0	0	0	0	0	0	0	1	1	1
	8th Street	0	1	0	0	0	0	0	1	0	0	1	1
	18th Street	0	0	0	0	0	0	0	0	0	0	0	0
	21st Street	0	0	0	0	0	0	0	0	0	4	4	3
	23rd Street	0	0	0	0	0	0	0	0	0	1	2	1
	Crescent Street	0	0	0	0	0	1	0	0	1	1	1	3
Astoria Boulevard at	27th Street	0	0	0	0	0	0	0	0	0	0	1	1
	28th Street	0	0	0	0	0	0	0	0	0	1	1	0
	29th Street	0	0	0	0	0	0	0	0	0	2	0	0
	30th Street	0	0	0	0	0	0	0	0	0	1	1	0
	31st Street	0	0	0	0	0	0	0	0	0	7	9	9
	33rd Street	0	0	0	0	0	0	0	0	0	6	5	7
30th Avenue at	14th Street	0	0	0	0	0	0	0	0	0	0	0	0
Jour Avenue at	21st Street	0	1	0	0	0	0	0	1	0	1	1	0
31st Avenue at	21st Street	0	0	0	0	0	0	0	0	0	3	0	0
	8th Street / Welling Ct.	0	0	0	0	0	0	0	0	0	0	0	0
Vernon Blvd / Main Avenue at	11th Street / Broadway	0	0	1	0	0	0	0	0	1	4	2	1
	31st Avenue	0	0	0	0	0	0	0	0	0	2	0	0

#### Table 13-48: Summary Accident Data 2010-2012

Source: New York State Department of Motor Vehicles (NYSDMV)/NYCDOT

It should also be noted that the proposed project would include new streets and sidewalks as well as loading docks for the future building occupants. Truck trips to the proposed project's loading docks would be minimal, with a maximum of 14 total in/out truck trips during the weekday AM peak hour (refer to Table 13-7) and are therefore not expected to interfere with pedestrian operations on adjacent sidewalks. During the weekday midday peak hour (the period during which pedestrian trips would be the highest), the project site location that would experience the greatest combined pedestrian and vehicular volumes would be the proposed 26<sup>th</sup> Avenue mid-block crossing at the 8<sup>th</sup> Street Mews. It is anticipated that approximately 1,060 pedestrians would cross 26<sup>th</sup> Avenue (combined north and south directions) at this location and a total of approximately 154 vehicles are expected in the eastbound movement. Pedestrian and vehicular volumes at all other project site crosswalks would be lower, comparatively. Traffic calming measures to reduce pedestrian and vehicular conflicts have been incorporated into the design of the proposed project and include the installation of all-way stop controls and crosswalks at the 4<sup>th</sup> Street extension and pedestrian bulb-outs at the midblock crossing along 26<sup>th</sup> Avenue. Similar measures could be installed along the waterfront public access easement to further minimize future pedestrian and bicycle safety concerns, and will be implemented, where necessary, in consultation with NYCDOT.

In addition, the proposed project would include a site for a 456-seat elementary school, which would therefore result in an increase in the number of school<u>-aged</u> children using crosswalks in the vicinity of

the project site during the weekday AM and PM peak periods at the start and end of each school day. Measures to ensure and enhance pedestrian safety in the vicinity of the school have been incorporated into the proposed project's design and include making 26<sup>th</sup> Avenue eastbound to the west of 9<sup>th</sup> Street to allow buses to drop students off directly adjacent to the Building 5 school and creating layby lanes for drop-off/pick-ups and parking along the south side of 26<sup>th</sup> Avenue between 4<sup>th</sup> and 9<sup>th</sup> Streets. The Applicant will work with NYCDOT and the New York City School Construction Authority (SCA) to implement required school signage and other typical safety features, such as high-visibility crosswalks, where necessary.

## K. PARKING

## **Existing Conditions**

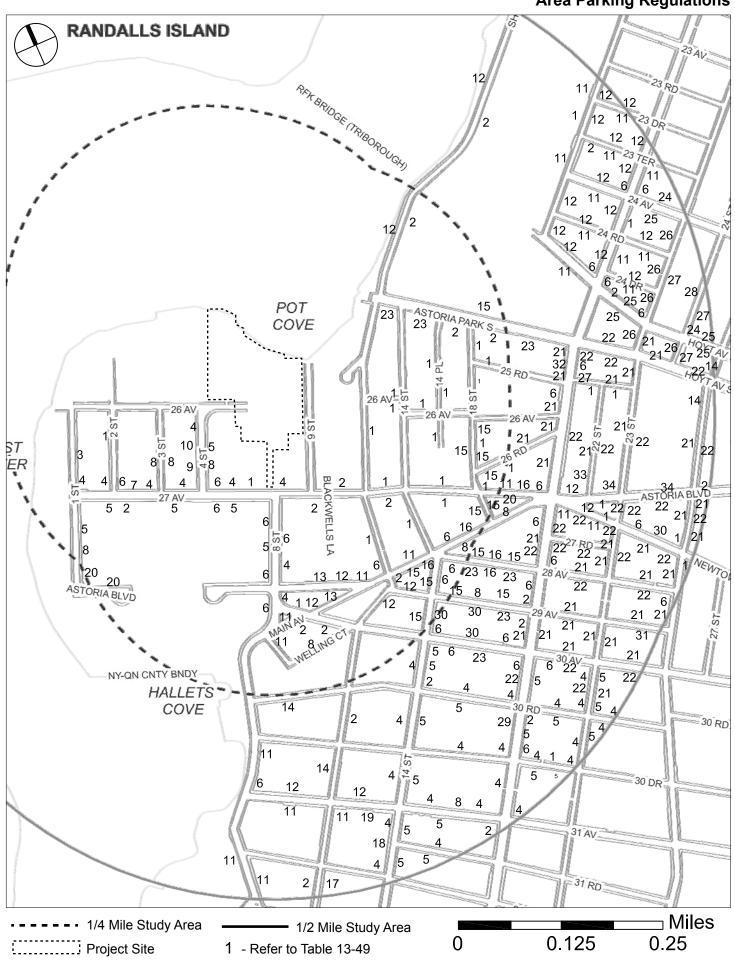
As preliminary analyses indicated that <u>weekday</u> parking demand could exceed the available accessory off-street parking capacity in the late evening and overnight hours, a detailed evening/overnight parking inventory of the area surrounding the project site was conducted on a typical weekday. The parking inventory encompassed two study areas: a <sup>1</sup>/<sub>4</sub>-mile radius (approximately a five-minute walk) from the project site, as recommended by CEQR guidelines; and a <sup>1</sup>/<sub>2</sub>-mile radius (approximately a ten-minute walk) from the project site, which is the extent to which drivers would generally go to find available parking. As shown in Figure 13-36, the <sup>1</sup>/<sub>4</sub>-mile study area is generally bounded by Astoria Park South to the north, 18<sup>th</sup> and 14<sup>th</sup> Streets to the <u>east</u>, 30<sup>th</sup> Road to the south, and the East River to the west. The <sup>1</sup>/<sub>2</sub>-mile study area is generally bounded by 23<sup>rd</sup> Drive and 24<sup>th</sup> Avenue to the north, Crescent and 23<sup>rd</sup> Streets to the east, and 31<sup>st</sup> Drive to the south.

On-street parking regulations, capacity, and occupancy were inventoried for the study areas on a blockby-block basis and are shown in Table 13-49. Several streets within the study areas have no posted parking regulations on either side of the street, and alternate side parking for street cleaning is regulated on many streets.

Table 13-50, below, presents the on-street parking occupancy within a <sup>1</sup>/<sub>4</sub>-mile and a <sup>1</sup>/<sub>2</sub>-mile of the project site. As indicated in the table, there are approximately 991 parking spaces within a <sup>1</sup>/<sub>4</sub>-mile of the project site, 88.3 percent of which were occupied in the evening/overnight hours. Considering the additional 2,143 parking spaces within a <sup>1</sup>/<sub>2</sub>-mile of the project site, there are approximately 285 parking spaces available in the <u>late</u> evening hours within a ten-minute walk of the project site. There are no public off-street parking facilities within the parking study area.

## Future without the Proposed Action (No-Action Condition)

Under the 2023 No-Action condition, background growth in the study area is expected to increase the demand for on-street parking. The same background growth rate assumed for traffic—0.5 percent per year for the first five year and 0.25 percent per year for each additional year until 2023—was applied to determine 2023 No-Action parking demand. <u>In addition, it is anticipated that parking demand generated by the nearby Halletts Point development will overflow into the surrounding area during the late evening hours , and the Halletts Point project will increase the ¼-mile on-street parking capacity by 14 spaces with the extension of Astoria Boulevard through the Astoria Houses campus. As a result of these future <u>No-Action conditions</u>, on-street parking occupancy is expected to reach 92.7 percent in the ¼-mile study area and 94.5 percent in the ¼-mile study area and <u>by</u> a total of 1<u>13</u> spaces in the ½-mile study area (see Table 13-51).</u>



No. <sup>1</sup>	Parking Regulation
1	No Parking Anytime
2	No Standing Anytime
3	No Standing Except Trucks Loading/Unloading Except Sun
4	No Parking Street Cleaning 11:30AM-1PM Mon & Thurs
5	No Parking Street Cleaning 11:30AM-1PM Tues & Fri
6	No Standing Handicap Bus Stop
7	No Engine Idling
8	No Parking 8AM-6PM Mon-Fri
9	No Standing 7AM-4PM Mon- Fri
10	No Standing 7AM-4PM Except Trucks Loading/Unloading Mon-Fri
11	No Parking Street Cleaning 11:30AM-1PM Tues
12	No Parking Street Cleaning 11:30AM-1PM Mon
13	No Parking Street Cleaning 11:00AM-2PM Mon
14	No Parking 7AM-7PM Mon-Fri
15	No Parking Street Cleaning 9:30AM-11AM Mon & Thurs
16	No Parking 8AM-6PM Except Sun
17	No Standing 8AM-5PM Mon-Fri
18	No Standing Except Farmers Market Vehicles 8AM-6PM Wed July-December
19	No Standing 8AM-6PM Mon-Fri Except Authorized Vehicles
20	No Parking 7AM-6PM Except Sunday
21	No Parking Street Cleaning 8:30AM-10AM Mon & Thurs
22	No Parking Street Cleaning 8:30AM-10AM Tues & Fri
23	No Parking Street Cleaning 9:30AM-11AM Tues & Fri
24	No Parking Street Cleaning 8:30-10AM Tuesday
25	No Parking Street Cleaning 8:30-10AM Monday
26	No Parking Street Cleaning 9:30-11AM Monday
27	No Parking Street Cleaning 9:30-11AM Tuesday
28	No Parking Street Cleaning 8-11AM Monday
29	No Parking 8AM-5PM Except Sunday
30	No Parking 7AM-4PM School Days
31	No Parking Street Cleaning 8-11AM Tues & Fri
32	No Parking 10:30AM-Noon Tues
33	No Parking 7-10AM Mon-Fri
34	No Parking 7-9AM Mon-Fri

### **Table 13-49: Study Area Parking Regulations**

Notes:

<sup>1</sup>Refer to Figure 13-36.

# Table 13-50: Existing On-Street Parking Conditions

				Parking Utilization
Study Area	Capacity	Occupied Spaces	Available Spaces	(%)
<sup>1</sup> /4-Mile Radius	991	875	116	88.3
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	2,143	1,974	169	92.1
Total	3,134	2,849	285	90.9

				Parking Utilization
Study Area	Capacity <sup>1</sup>	Occupied Spaces <sup>2</sup>	Available Spaces	(%)
<sup>1</sup> / <sub>4</sub> -Mile Radius	<u>1,005</u>	9 <u>32</u>	<u>73</u>	9 <u>2.7</u>
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	2,143	2,044	99	95.4
Total	<i>3,1<u>48</u></i>	2,9 <u>76</u>	1 <u>72</u>	94. <u>5</u>

#### Table 13-51: 2023 No-Action On-Street Parking Conditions

Notes:

<sup>1</sup> Includes a net 14 additional on-street parking spaces created as part of the Halletts Point project.

<sup>2</sup> Reflects general background growth and late evening overflow parking demand from the Halletts Point project.

This table has been updated for the FEIS.

### Future with the Proposed Action (With-Action Condition)

As shown earlier in Table 13-2, the RWCDS includes approximately 900 required accessory on-site parking spaces.

Table 13-52 shows the 24-hour parking accumulation that is expected to be generated by each land use included in the Proposed Action. Parking demand generated by <u>the proposed project's market rate</u> residential <u>component</u> was forecasted based on the average vehicles per household ratio from the 2007-2011 ACS, while <u>parking demand generated by the proposed project's affordable housing component was</u> based on the average vehicles per household at comparable developments in the ½-mile study area. <u>Parking</u> demand from the local retail, supermarket, and school land uses were derived from the respective auto trip forecast, as shown earlier in Table 13-7.

As shown in Table 13-52, the overnight demand is expected to total <u>948</u> parking spaces, while the maximum demand is expected to total <u>974</u> parking spaces from 8 - 9 PM. During this peak period, the Proposed Action would result in a shortfall of approximately <u>74</u> parking spaces, as well as in shortfall of approximately <u>48</u> overnight parking spaces. As indicated in Table 13-53, peak parking demand could be absorbed by available on-street spaces within the parking study area. <u>While not representing the peak</u> overflow parking demand generated by the proposed project, future overnight parking conditions were also assessed to determine whether there would be adequate capacity in the parking study area to accommodated overflow parking demand from both the proposed project and the nearby Halletts Point development. In the future with the Proposed Action, overnight parking capacity would adequately accommodate both project's overflow demand without resulting in a parking shortfall. Therefore, it is not expected that the Proposed Action would result in a significant adverse parking impact.

# L. WEEKEND CONDITIONS ASSESSMENT

Subsequent to issuance of the DEIS, and in response to further NYCDOT comments, a Saturday transportation analysis was prepared. As discussed above, the proposed Astoria Cove project would generate significant travel activity during the weekday peak periods. Although the planned project's development program would generate most of their trip making during the weekday period, the project's combined uses would generate a measurable amount of person trips during the weekend period, in particular, vehicle trips. Per NYCDOT guidance, to determine the potential for traffic-related impacts during non-weekday peak hours, a semi-quantitative transportation assessment of a representative weekend peak period (Saturday midday) for the proposed project was prepared. This assessment, which includes estimates of project-generated Saturday midday peak hour trips and comparisons of weekday and Saturday midday background conditions, is presented below.

	Local Retail		Supermarket Residential <sup>1</sup>			ential <sup>1</sup>		hool taff		
	In	Out	In	Out	In	Out	In	Out	Total Accumulation	
12-1 AM	0	0	0	0	7	7	0	0	<u>948</u>	
1-2	0	0	0	0	7	7	0	0	<u>948</u>	
2-3	0	0	0	0	7	7	0	0	<u>948</u>	
3-4	0	0	0	0	7	7	0	0	<u>948</u>	
4-5	0	0	0	0	7	7	0	0	<u>948</u>	
5-6	0	0	13	9	14	41	0	0	<u>925</u>	
6-7	0	0	27	9	34	118	0	0	<u>859</u>	
7-8	0	0	36	22	41	122	0	0	<u>792</u>	
8-9	2	2	51	39	79	315	17	0	<u>585</u>	
9-10	2	1	67	36	71	107	0	0	<u>581</u>	
10-11	5	3	72	54	71	123	0	0	<u>549</u>	
11-12	5	5	72	72	75	103	0	0	<u>521</u>	
12-1 PM	13	13	51	51	98	98	0	0	<u>521</u>	
1-2	6	5	80	98	100	102	0	0	<u>502</u>	
2-3	6	4	89	107	105	100	0	0	<u>491</u>	
3-4	5	5	80	107	150	90	0	0	<u>524</u>	
4-5	5	5	89	85	254	147	0	0	<u>635</u>	
5-6	7	7	85	79	281	151	0	17	<u>754</u>	
6-7	3	6	44	45	198	99	0	0	<u>849</u>	
7-8	3	5	18	27	179	79	0	0	<u>938</u>	
8-9	2	2	9	18	106	61	0	0	<u>974</u>	
9-10	1	1	0	18	34	39	0	0	<u>951</u>	
10-11	0	0	0	10	23	23	0	0	<u>941</u>	
11-12	0	0	0	0	20	13	0	0	<u>948</u>	
						Overr	ight D	emand	<u>948</u>	

**Table 13-52: Weekday Parking Accumulation Forecast** 

Sources: Local retail temporal distribution based on the 2004 No. 7 Subway Extension - Hudson Yards Rezoning and Development Program FGEIS; supermarket temporal distribution based on the 2005 Van Courtland Center EAS; residential temporal distribution based on 2005 Brooklyn Bridge Park FEIS; school staff temporal distribution based on typical school staff working hours. Notes: 25 percent link trip credit applied to Retail and Supermarket land use.

<sup>1</sup> No credit was taken for the 166 residential units in upland area in No-Action condition.

### Table 13-53: 2023 With-Action Parking Conditions

				Parking Utilization
Location	Capacity <sup>1</sup>	Occupied Spaces	Available Spaces	(%)
Project Site Off-Street	900	900	0	100
<sup>1</sup> /4-Mile Radius	<u>1,005</u>	<u>1,005</u>	0	100
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	2,143	2,0 <u>45</u>	<u>98</u>	9 <u>5.9</u>
Total	<i>4,0<u>48</u></i>	<u>4,003</u>	<u>98</u>	98 <u>9</u>

<u>Notes:</u> <u>Includes a net 14 additional on-street parking spaces created as part of the Halletts Point project.</u>

## **Saturday Travel Demand Projections**

Using the same methodology and sources of information described in Section D, "Level 1 Screening Assessment," travel demand assumptions were developed for the Saturday midday peak hour (2-3 PM). Since the proposed elementary school would be closed on weekends, it was not considered in the Saturday travel demand estimates. The Saturday midday travel demand assumptions for the proposed project are presented in Table 13-54. The person- and vehicle-trip estimates for the proposed project are shown in Table 13-55. In total, 3,064 project-generated person trips and 588 project-generated vehicle trips were projected for the Saturday midday peak hour. In comparison, the Saturday midday peak hour person trips would be six percent less than the maximum peak hour person trips projected for the weekday midday (3,272) and greater than the weekday AM and PM projected person trips. The Saturday midday peak hour vehicle trips would be approximately seven percent less than the maximum peak hour vehicle trips projected for the weekday PM (633) and greater than the weekday AM and midday projected vehicle trips.

The Saturday project-generated peak hour trips were assigned to the transportation network in the same manner as described above for the weekday peak hours and are further discussed below.

# **Traffic**

Figure 13-37 shows the assignment of vehicle trips (including auto, taxi, and truck trips) generated by the proposed project to and from the project site during the Saturday midday peak hour. Based on the projectgenerated traffic shown in Figure 13-37 and in coordination with DCP and NYCDOT, 13 key intersections within the study area were selected for detailed analysis to assess for potential significant adverse impacts as a result of the proposed project during the Saturday midday peak hour. The 13 intersections included in the Saturday midday analysis are:

- 27th Avenue & 4th Street (unsignalized)
- 27<sup>th</sup> Avenue & 8<sup>th</sup> Street <u>3</u>.
- 27<sup>th</sup> Avenue & 12<sup>th</sup> Street (unsignalized) 27<sup>th</sup> Avenue & 14<sup>th</sup> Street (unsignalized) 4.
- 5.
- 27<sup>th</sup> Avenue & 18<sup>th</sup> Street (unsignalized) 6.
- Astoria Boulevard & 21<sup>st</sup> Street 7.
- 14. Astoria Boulevard & 31<sup>st</sup> Street
- Hovt Avenue South/Astoria Boulevard & 33<sup>rd</sup> Street 15.
- Astoria Boulevard North & 32<sup>nd</sup> Street 18.
- Astoria Boulevard & 8th Street 19.
- Hoyt Avenue North & 21st Street <u>24.</u>
- Hoyt Avenue South/Astoria Park South & 21st Street 25.
- 27<sup>th</sup> Avenue & 9<sup>th</sup> Street (unsignalized) 26.

For the other 17 intersections included in the assessment of weekday peak hours conditions, per consultation with DCP and NYCDOT, it was determined that there would not be a potential for significant adverse traffic impacts during the Saturday peak hour beyond those anticipated in the weekday peak hours, and no further analysis was warranted. A more in-depth review of conditions at the 13 intersections listed above is provided below.



# Astoria Cove

# Figure 13-37

Land Use:	Local	<u>Retail</u>	Resid	ential_	<u>Supermarke</u>	<u>•t</u>
Size/Units:	84,470	gsf	1,502	DU*	25,000	gsf
Trip Generation:	(	1)	(1	1)	(1)	)
Saturday	24	40	9.	.6	23	1
	per 1,	,000 sf	per	DU	per 1,0	00 sf
Temporal Distribution:	(	0	(1	1)	(5)	)
Sat MD	10.	.0%	8.0	)%	9.09	%
		0	(3		(5)	
Modal Splits:		eriods	All Pe		Sat N	
Auto/Auto-dropoff		0%	32		76.0	
Taxi		0%	0.5% 55.4%		0.0% 0.0%	
Subway/Shuttle		0%				
Bus		6.0%		2%	6.0%	
Walk/Ferry/Other	Walk/Ferry/Other 83.0%		8.5	5%	18.0%	
	100	0.0%	100	.0%	100.0	)%
		0%	(4			
In/Out Splits:	In	Out	In	Out	In	Out
Sat MD	50%	50%	50.0%	50.0%	52%	48%
Vehicle Occupancy:	(	0	(3	3)	(5)	)
	AllPe	eriods	All Pe	eriods	Sat N	1D
Auto	2.	00	1.	11	1.4	8
Taxi	2.	00	1.	.4		
Truck Trip Generation:		0	(1	1)	(11	)
Saturday	0.	04	0.0	02	0.0	4
	per 1,	,000 sf	per	DU	per 1,0	00 sf
	(	0	(1	1)	(1)	)
Sat MD	11.	.0%	9.0	)%	4.09	%
	In	Out	In	Out	In	Out
Sat MD	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%

### Table 13-54: Saturday Transportation Planning Assumptions (Generic Supermarket)

Notes:

(1) CEQR Technical Manual

(2) Dutch Kills Rezoning and Related Actions FEIS (2008)

(3) Modal split and vehicle occupancy rates based on 2007-2011 ACS Journey to Work data (census tracts 81,83,91,97,101,103,105)

(4) Based on ITE Trip Generation Handbook, 8th Edition, Land Use Code (220) Apartment.

(5) Based on 1525 Albany Avenue Pathmark Supermarket Survey

(6) CEQR local retail delivery truck trip generation rate.

<u>\* 166 residential units in upland area in No-Action condition (1,668 DUs in With-Action condition) for net increment of 1,502.</u> <u>This table is new to the FEIS</u>.

Land Use: Size/Units:		Local Retail		Resid	Residential		Supermarket		Existing Industrial		
		84,470 gsf		1,502	DU	25,000	gsf	-194,700	gsf	Тс	otal
	Sat MD	1,5	20	1,1	54	39	0	NA	A	3,0	)64
Person T	rips:										
Sat MD	Auto	15	15	187	187	154	142	NA	NA	356	344
	Taxi	23	23	3	3	0	0	NA	NA	26	26
	Subway	46	46	320	320	0	0	NA	NA	366	366
	Bus	46	46	18	18	12	11	NA	NA	76	75
	Schoolbus							NA	NA	0	0
	Walk/Other	630	630	49	49	37	34	NA	NA	716	713
	Total	760	760	577	577	203	187	NA	NA	1,540	1,524
Vehicle T	Trips :										
Sat MD	Auto (Total)	8	8	168	168	104	96	-8	-14	272	258
	Taxi	12	12	2	2	0	0	0	0	14	14
	Taxi Balanced	24	24	4	4	0	0	0	0	28	28
	Shuttle/Schoolbus			0	0			0	0	0	0
	Truck	0	0	1	1	0	0	0	0	1	1
	Total	32	32	173	173	104	96	-8	-14	301	287

### Table 13-55: Saturday Travel Demand Forecast (Generic Supermarket)

#### Notes:

<u>- 25 percent link trips applied to retail and supermarket uses.</u> *This table is new to the FEIS.* 

#### Existing Conditions

<u>Traffic data were collected at the 13 aforementioned intersections in June 2014. Existing Saturday midday</u> traffic volumes at the analyzed intersections are shown in Figure 13-38.

Weekend Intersection Capacity Analysis

Table 13-56 summarizes the existing Saturday midday lane group LOS. As indicated in the table, of the 52 analyzed individual lane groups, five operate at LOS E, while none operate at LOS F during the Saturday midday peak hour. In comparison, eleven of these 52 individual lane groups operate at LOS E or LOS F in one or more weekday peak hour (refer to Table 13-16).

#### Table 13-56: Existing Saturday Midday Lane Group LOS Summary

	Saturday Midday PM Peak Hour
Overall LOS A/B/C	38
Overall LOS D	9
Overall LOS E	5
Overall LOS F	0
Number of movements at LOS E or F of approximately 52 movements analyzed	5

<u>This table is new to the FEIS.</u>



# Astoria Cove

Table 13-57 shows the detailed v/c ratios, delays, and LOS by movement at each of the 13 analyzed existing intersections for the Saturday midday peak hour and identifies those movements that are considered congested in the Saturday midday peak hour (i.e., movements operating at LOS E or F and/or with a high v/c ratio—0.90 and above). These congested locations, all on Astoria Boulevard, are listed below:

## <u>Astoria Boulevard & 21<sup>st</sup> Street</u>

- Northbound shared left-turn/through/right-turn
- Southbound shared left-turn/through/right-turn

# Astoria Boulevard and 31<sup>st</sup> Street

- Eastbound shared left-turn/through/right-turn

Hoyt Avenue South/Astoria Boulevard & 33rd Street

- Eastbound left-turn on Astoria Boulevard
- Eastbound left-turn on Hoyt Avenue
- Northbound right-turn

# Future without the Proposed Action (No-Action Condition)

As impact analyses are based on the incremental change to expected future conditions as a result of a proposed project, a future without the Proposed Action condition, the 2023 Saturday midday No-Action condition, was developed. The 2023 No-Action condition incorporates changes to the study area's traffic network as a result of general background growth and traffic demand and traffic operation changes associated with developments anticipated to be completed by 2023 (see Section G, "Traffic," above).

As per *CEQR Technical Manual* guidelines, an annual background growth rate of 0.5 percent was assumed for the first five years (2014-2019) and 0.25 percent for the remaining years (2020-2023). In addition, a total of 67 projects/developments are planned or proposed within or just beyond the study area. Based on their size, it was determined that background growth would account for the increase in travel demand for 36 of the 67 No-Action projects. 2023 No-Action traffic volumes were determined by adding the background growth and estimated volume increments associated with the remaining 31 more substantial No-Action projects to the existing 2014 baseline traffic volume network, consistent with the weekday conditions analysis.

In addition, as described in Section G, "Traffic," above, in conjunction with the No-Action as-of-right residential development on the project site's upland parcels, the currently unimproved and inaccessible portion of 26<sup>th</sup> Avenue is expected to be built-out in the future without the Proposed Action, thereby providing access to 9<sup>th</sup> Street. For the purposes of the traffic analysis, it is assumed that 26<sup>th</sup> Avenue would operate one-way eastbound with one travel lane and on-street parking on both sides in the 2023 No-Action condition.

Table 13-57: 2014 Existing Saturda		Saturday Midday Peak Hour				
Intersection	Lane	V/C	Delay	LOS		
	Group	Ratio	(sec/veh)	200		
2. 27 <sup>th</sup> Avenue & 4 <sup>th</sup> Street	EB-LT	NA	8.8	А		
(Unsignalized-All Way Stop)	WB-T	NA	8.7	A		
(Onsignalized Mill (Vay Stop)	WB-R	NA	7.0	A		
	SB-LR	NA	8.5	A		
	52 24		0.0			
3. 27 <sup>th</sup> Avenue & 8 <sup>th</sup> Street	EB-TR	0.30	12.8	В		
	WB-LT	0.27	12.4	В		
	NB-L	0.14	20.2	С		
	NB-R	0.16	20.5	С		
4. 27 <sup>th</sup> Avenue & 12 <sup>th</sup> Street	EB-LT	0.03	7.9	А		
(Unsignalized-Two Way Stop)	NB-LTR	0.26	14.2	В		
5. 27 <sup>th</sup> Avenue & 14 <sup>th</sup> Street	EB-TR	NA	9.2	А		
(Unsignalized-All Way Stop)	WB-LT	NA	8.6	А		
	SB-LTR	NA	9.5	А		
6. 27 <sup>th</sup> Avenue & 18 <sup>th</sup> Street	EB-L	0.09	9.4	А		
(Unsignalized-Two Way Stop)	WB-L	0.01	7.4	А		
		0.26	24.0	C		
7. Astoria Boulevard & 21 <sup>st</sup> Street	EB-L	0.26	34.0	C		
	EB-TR WB-L	0.37 0.64	35.1 39.4	D D		
	WB-L WB-TR	0.04	39.4 34.1	C		
	NB-LTR	1.05	79.7	E	*	
	SB-LTR	1.05	65.2	E	*	
	SD LIK	1.05	00.2	L		
14. Astoria Boulevard & 31st Street	EB-LTR	1.03	57.0	Е	*	
	NB-T	0.74	40.6	D		
	NB-R	0.57	9.5	А		
	SB-T	0.70	21.4	С		
	SB-R	0.35	15.0	В		
15. Hoyt Avenue S./Astoria Boulevard	Astoria Blvd (EB-LT)	1.02	58.2	Е	*	
33rd Street	NB-TR	0.89	35.1	D		
	NB-R	1.05	64.4	Е	*	
	Hoyt Ave (EB-LT)	0.93	33.6	С	*	
18. Astoria Boulevard N. & 32 <sup>nd</sup> Street	WB-Main-T	0.27	7.1	А		
10. Historia Boule value 14. de 52 – Street	WB-Ramp-T	0.27	18.9	В		
	NB-L	0.00	29.3	C		
	SB-R	0.02	25.9	C		
19. Astoria Boulevard & 8 <sup>th</sup> Street	EB-LR	0.09	26.0	С		
	WB-L	0.16	26.9	C		
	WB-TR	0.08	25.7	C		
	NB-LT	0.17	13.1	В		
	SB-TR	0.19	13.4	В		

## Table 13-57: 2014 Existing Saturday Conditions–LOS at Analyzed Intersections

		Saturda	y Midday P	eak Hour
Intersection	Lane	V/C	Delay	LOS
	Group	Ratio	(sec/veh)	
24. Hoyt Avenue N. & 21 <sup>st</sup> Street	EB-L	0.05	40.8	D
	EB-R	0.26	44.5	D
	WB-L	0.62	35.9	D
	WB-TR	0.26	15.0	В
	NB-L	0.24	28.1	С
	NB-T	0.89	52.2	D
	SB-TR	0.68	32.5	С
25. Hoyt Avenue S./Astoria Park S. &	EB-L	0.15	30.1	С
21st Street	EB-TR	0.65	36.6	D
	NB-LTR	0.70	19.3	В
	SB-LTR	0.76	18.4	В
26. 27 <sup>th</sup> Avenue & 9 <sup>th</sup> Street	EB-LT	0.00	7.7	А
(Unsignalized-Two Way Stop)	SB-LR	0.06	11.2	В

### <u>Table 13-57 (continued): 2014 Existing Saturday Conditions–LOS at Analyzed</u> Intersections

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9)

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version 5.5)

This table is new to the FEIS.

### Weekend Intersection Capacity Analysis

Figure 13-39 show the expected No-Action Saturday midday peak hour traffic volumes. Table 13-58, below, shows a summary comparison of the individual lane group LOS for existing and future No-Action conditions. As shown in Table 13-58, under the No-Action condition, one individual traffic movements would operate at LOS E and three would operate at LOS F in the Saturday peak hour. In comparison, 15 of these individual lane groups operate at LOS E or LOS F in one or more weekday peak hour (refer to Table 13-19).

Table	13-58:	Saturday	Midday	Lane	Group	LOS	<b>Summary</b>
Comparison—Existing vs. No-Action Conditions							

	Existing Conditions	2023 No-Action Condition
Overall LOS A/B/C	38	37
Overall LOS D	9	16
Overall LOS E	5	1
Overall LOS F	0	3
Number of movements at LOS E or F	5	4

Notes:

This table is new to the FEIS.



# Astoria Cove

Table 13-59 shows the detailed v/c ratios, delays, and LOS by movement at the analyzed intersections in each peak hour under the No-Action condition and identifies those movements that would be congested in the Saturday midday peak hour. As shown in Table 13-59, many of the movements that are congested under existing conditions would continue to operate at the same level of service with slight increases in v/c ratios and delays under the No-Action condition. The intersections where newly congested movements would occur under the No-Action condition or where the level of service of currently congested movements would degrade are discussed in the following.

Hoyt Avenue South/Astoria Boulevard & 33rd Street

- The Astoria Boulevard eastbound left-turn/through movement would deteriorate from LOS E under Saturday midday existing conditions to LOS F under the No-Action condition.
- The Hoyt Avenue South eastbound left-turn/through movement would deteriorate from LOS C under Saturday midday existing conditions to LOS D under the No-Action condition.
- The 33<sup>rd</sup> Street northbound through-right movement would deteriorate from LOS D (with a v/c ratio of 0.89) under Saturday midday existing conditions to LOS D (with a v/c ratio of 0.92) under the No-Action condition.
- The 33<sup>rd</sup> Street northbound right-turn movement would deteriorate from LOS E under Saturday midday existing conditions to LOS F under the No-Action condition.

Astoria Boulevard North & 32<sup>nd</sup> Street

- The westbound through movement at the ramp would deteriorate from LOS B under Saturday midday existing conditions to LOS D under the No-Action condition.

Hoyt Avenue North & 21st Street

- The northbound through movement would deteriorate from LOS D under Saturday midday existing conditions to LOS E under the No-Action condition.

Hoyt Avenue South/Astoria Park South & 21st Street

- The southbound left-turn/through/right-turn movement would deteriorate from LOS B under Saturday midday existing conditions to LOS C (with a v/c ratio of 0.98) under the No-Action condition.

It should also be noted that Saturday midday traffic conditions would improve along the northbound and southbound approaches at the intersection of Astoria Boulevard and 21<sup>st</sup> Street, as compared to existing conditions, as well as along the eastbound approach and southbound through movement at the intersection of Astoria Boulevard and 31<sup>st</sup> Street. These improvements are due to No-Action changes anticipated at these intersections as part of the traffic mitigation measures identified in the 2013 *Halletts Point Rezoning FEIS* and/or 2012 *Cornell NYC Tech Campus FEIS*.

### Future with the Proposed Action (With-Action Condition)

As discussed above, the Proposed Action is expected to generate a total of 588 net vehicle trips in the Saturday midday peak hour. The assignment of the projected vehicle trip increments is shown in Figure 13-37. In addition, as discussed in Section G, "Traffic," above, changes to the roadway network and traffic circulation improvements would be implemented as part of the Proposed Action, and were incorporated into the Saturday With-Action traffic analysis.

		Saturday Midday Peak Hour								
Intersection		E	XIS TIN	G		NO	ON			
mersection	Lane	V/C	Delay	LOS		V/C	Delay	LOS		
	Group	Ratio	(sec.)			Ratio	(sec.)			
2. 27th Avenue & 4th Street	EB-LT	NA	8.8	А		0.56	16.4	В		
(Existing Unsignalized-All Way Stop)	WB-T	NA	8.7	А		0.44	13.2	В		
(No-Action Signalized)	WB-R	NA	7.0	А		0.20	11.4	В		
	SB-LR	NA	8.5	А		0.06	20.0	С		
3. 27th Avenue & 8th Street	EB-T	-	-	-		0.34	13.1	В		
	EB-R	-	-	-		0.26	12.3	В		
	EB-TR	0.30	12.8	В			12.8	В		
	WB-LT	0.27	12.4	В		0.63	19.0	В		
	NB-L	0.14	20.2	С		0.22	21.1	С		
	NB-R	0.16	20.5	С		0.19	20.9	С		
4. 27th Avenue & 12th Street	EB-LT	0.03	7.9	А		0.50	11.8	В		
(Existing Unsignalized-Two Way Stop)	WB-TR	-	-	-		0.48	11.2	В		
(No-Action Signalized)	NB-LTR	0.26	14.2	В		0.37	28.8	С		
5. 27th Avenue & 14th Street	EB-TR	NA	9.2	А		0.36	11.8	В		
(Existing Unsignalized-All Way Stop)	WB-LT	NA	8.6	А		0.31	11.2	В		
(No-Action Signalized)	SB-LTR	NA	9.5	А		0.72	36.6	D		
6. 27th Avenue & 18th Street	EB-L	0.09	9.4	А		0.13	9.6	А		
(Unsignalized-Two Way Stop)	WB-L	0.01	7.4	А		0.01	7.7	А		
7. Astoria Boulevard & 21st Street	EB-L	0.26	34.0	С		0.35	35.3	D		
	EB-TR	0.37	35.1	D		0.66	39.9	D		
	WB-L	0.64	39.4	D		0.67	40.2	D		
	WB-TR	0.32	34.1	С		0.45	35.8	D		
	NB-LT	-	-	-		1.08	90.5	F		
	NB-R	-	-	-		0.52	36.6	D		
	NB-LTR	1.05	79.7	Е	*		78.7	E		
	SB-LT	-	-	-		0.91	40.4	D		
	SB-R SB-LTR	- 1.05	- 65.2	- E	*	0.74	38.2 39.8	D D		
14. Astoria Boulevard & 31st Street	EB-LTR	1.03	57.0	E	*	0.70	24.1	C		
	NB-T	0.74	40.6	E D		0.76	42.1	D		
	NB-T NB-R	0.57	9.5	A		0.60	10.1	B		
	SB-T	0.70	21.4	C		0.64	19.6	B		
	SB-R	0.35	15.0	В		0.37	15.2	B		
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	1.02	58.2	Е	*	1.27	160.5	F		
33rd Street	NB-TR	0.89	35.1	D		0.92	36.1	D		
	NB-R	1.05	64.4	E	*	1.10	83.3	F		
	Hoyt Ave (EB-LT)	0.93	33.6	C	*	1.00	43.4	D		

# Table 13-59: 2023 Future Saturday No-Action Condition–LOS at Analyzed Intersections

		Saturday Midday Peak Hour								
Intersection		E	XIS TIN	G	NO-ACTION					
Intersection	Lane	V/C	V/C Delay LO		V/C	Delay	LOS	5		
	Group	Ratio	(sec.)		Ratio	(sec.)				
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.27	7.1	А	0.38	8.1	А	_		
	WB(Ramp)-T	0.88	18.9	В	1.05	50.8	D			
	NB-L	0.44	29.3	С	0.49	29.8	С			
	SB-R	0.02	25.9	С	0.02	25.9	С			
19. Astoria Boulevard & 8th Street	EB-L				0.06	25.7	С			
	EB-R				0.39	31.6	С			
	EB-LR	0.09	26.0	С		30.9	С			
	WB-L	0.16	26.9	С	0.26	28.4	С			
	WB-TR	0.08	25.7	С	0.30	29.0	С			
	NB-LT	0.17	13.1	В	0.34	15.0	В			
	SB-TR	0.19	13.4	В	0.31	14.8	В			
24. Hoyt Avenue N. & 21st Street	EB-L	0.05	40.8	D	0.05	40.9	D	-		
	EB-R	0.26	44.5	D	0.27	44.6	D			
	WB-L	0.62	35.9	D	0.89	43.9	D			
	WB-TR	0.26	15.0	В	0.27	15.1	В			
	NB-L	0.24	28.1	С	0.28	29.1	С			
	NB-T	0.89	52.2	D	0.99	70.7	Е			
	SB-TR	0.68	32.5	С	0.74	33.9	С			
25. Hoyt Avenue S./Astoria Park S. &	EB-L	0.15	30.1	С	0.18	30.5	С			
21st Street	EB-TR	0.65	36.6	D	0.80	39.5	D			
	NB-LTR	0.70	19.3	В	0.87	28.2	С			
	SB-LTR	0.76	18.4	В	0.98	32.9	С			
26. 27th Avenue & 9th Street	EB-LT	0.00	7.7	А	0.01	8.4	А			
(Unsignalized-Two Way Stop)	SB-LR	0.06	11.2	В	0.27	19.1	С			

#### <u>Table 13-59 (continued): 2023 Future Saturday No-Action Condition–LOS at Analyzed</u> Intersections

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9)

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version .5)

This table is new to the FEIS.

Weekend Intersection Capacity Analysis

Figure 13-40 show the traffic network volumes under the With-Action condition for the Saturday midday peak hour. The volumes shown are the sum of the net incremental traffic generated by the Proposed Action and the No-Action traffic network. Table 13-60 shows a summary comparison of the individual lane group LOS for future No-Action and With-Action conditions. As shown in Table 13-60, one individual traffic movements would operate at LOS E and eight would operate at LOS F in the Saturday midday peak hour under the With-Action condition. In comparison, at these 13 analyzed intersections, 22 of these individual lane groups operate at LOS E or LOS F in one or more weekday peak hour (refer to Table 13-21).

Table 13-61 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in the Saturday midday peak hour under the With-Action condition and identifies those movements that are considered impacted in the Saturday midday peak hour. As shown in Table 13-61, one or more



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approaches or lane groups at a total of seven of the 13 analyzed intersections would experience significant adverse impacts in one or more peak hour as a result of the Proposed Action. In comparison, 11 of these 13 intersections would experience significant adverse impacts during one or more weekday peak hour (refer to Table 13-25). Potential measures to mitigate these significant adverse impacts are discussed in Chapter 20, "Mitigation."

Table 13-60: Saturday Midday Lane (	Froup LOS Summary Comparison
<b>No-Action vs. With-Action Conditions</b>	

	2023 No-Action Condition	2023 With-Action Condition
Overall LOS A/B/C	37	33
Overall LOS D	16	16
Overall LOS E	1	1
Overall LOS F	3	8
Number of movements at	4	0
LOS E or F	4	3

<u>This table is new to the FEIS.</u>

## Alternate Traffic Impact Analysis without Halletts Point Development

Consistent with the weekday traffic analysis, an additional analysis was conducted to determine whether the impacts disclosed in Table 13-61 would also occur absent the Halletts Point development.

## Alternate No-Action Condition Weekend Intersection Capacity Analysis

Figures 13-41 shows the expected Saturday midday peak hour traffic volumes for the alternate No-Action condition without the Halletts Point development. Table 13-62 below shows a summary comparison of the individual lane group LOS for existing and alternate future Saturday No-Action conditions. As shown in Table 13-62, one individual traffic movements would operate at LOS E and five would operate at LOS F in the Saturday midday peak hour under the alternate No-Action condition. In comparison, 16 of these individual lane groups operate at LOS E or LOS F in one or more weekday peak hour (refer to Table 13-23).

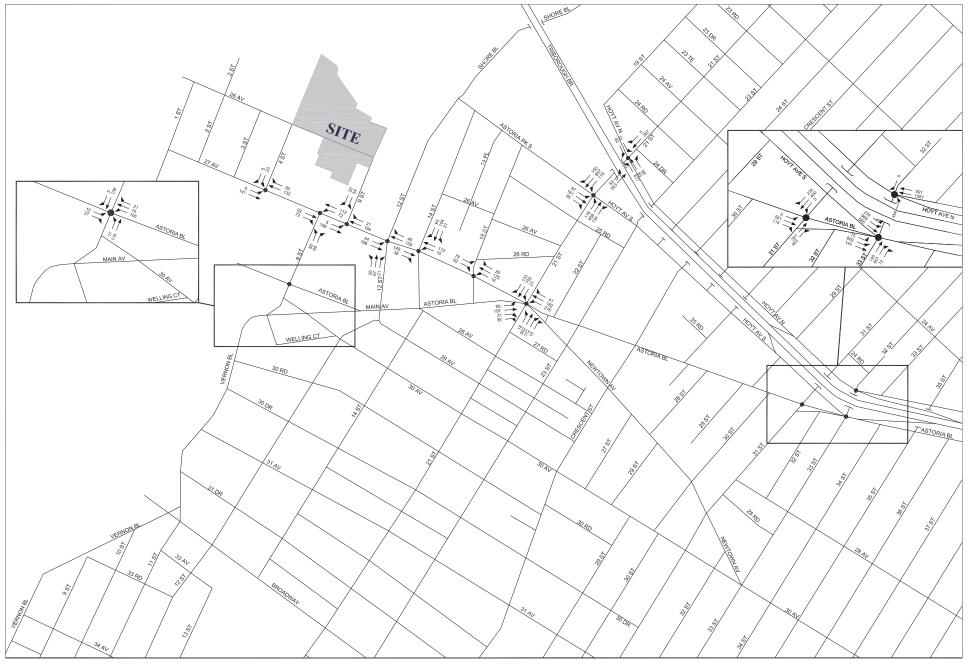
Table 13-63 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in each peak hour under the alternate No-Action condition and identifies those movements that would congested in the Saturday midday peak hour. As shown in Table 13-63, many of the movements that are congested under existing conditions would continue to operate at the same level of service with slight increases in v/c ratios and delays under the alternate No-Action condition. The intersections where newly congested movements would occur under the alternate No-Action condition or where the level of service of currently congested movements would degrade are discussed in the following.

## Astoria Boulevard & 21st Street

- The northbound shared left-turn/through/right-turn movement and the southbound shared leftturn/through/right-turn movement would both deteriorate from LOS E under Saturday midday existing conditions to LOS F under the alternate No-Action condition.

Astoria Boulevard & 31st Street

- The eastbound shared left-turn/through/right-turn movement would deteriorate from LOS E under Saturday midday existing conditions to LOS F under the alternate No-Action condition.



# Astoria Cove

# Figure 13-41

		Saturday Midday Peak Hour								
T.d		NO-ACTION WITH-ACTIO								
Intersection	Lane	V/C	Delay	LOS	V/C	Delay	y LOS			
	Group	Ratio	(sec.)		Ratio	(sec.)				
2. 27th Avenue & 4th Street	EB-LT	0.56	16.4	В	0.56	16.4	В			
(Existing Unsignalized-All Way Stop)	WB-T	0.44	13.2	В	0.44	13.2	В			
(No-Action Signalized)	WB-R	0.20	11.4	В	1.23	138.9	F			
	SB-LR	0.06	20.0	С	0.06	20.0	С			
3. 27th Avenue & 8th Street	EB-T	0.34	13.1	В	0.34	13.1	В			
	EB-R	0.26	12.3	В	0.26	12.3	В			
	WB-LT	0.63	19.0	В	1.21	130.6	F			
	NB-L	0.22	21.1	С	0.36	23.0	С			
	NB-R	0.19	20.9	С	0.19	20.9	С			
4. 27th Avenue & 12th Street	EB-LT	0.50	11.8	В	0.97	42.3	D			
(Existing Unsignalized-T wo Way Stop)	WB-TR	0.48	11.2	В	0.75	17.5	В			
(No-Action Signalized)	NB-LTR	0.37	28.8	С	0.39	29.3	С			
5. 27th Avenue & 14th Street	EB-TR	0.36	11.8	В	0.64	16.0	В			
(Existing Unsignalized-All Way Stop)	WB-LT	0.31	11.2	В	0.57	14.3	В			
(No-Action Signalized)	SB-LTR	0.72	36.6	D	0.72	36.6	D			
6. 27th Avenue & 18th Street	EB-L	0.13	9.6	А	0.15	9.8	А			
(Unsignalized-Two Way Stop)	WB-L	0.01	7.7	А	0.01	8.1	А			
7. Astoria Boulevard & 21st Street	EB-L	0.35	35.3	D	0.39	35.9	D			
	EB-TR	0.66	39.9	D	0.80	44.3	D			
	WB-L	0.67	40.2	D	0.67	40.2	D			
	WB-TR	0.45	35.8	D	0.62	38.3	D			
	NB-LT	1.08	90.5	F	1.39	223.6	F			
	NB-R	0.52	36.6	D	0.52	36.6	D			
	SB-LT SB-R	0.91 0.74	40.4 38.2	D D	0.93 0.94	41.4 45.5	D D			
14. Astoria Boulevard & 31st Street	EB-LTR	0.70	24.1	C	0.78	25.7	C			
14. Astoria Boulevalu & 51st Street	NB-T	0.76	42.1	D	0.78	42.1	D			
	NB-R	0.60	10.1	В	0.60	10.1	В			
	SB-T	0.64	19.6	В	0.64	19.6	В			
	SB-R	0.37	15.2	В	0.37	15.2	В			
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	1.27	160.5	F	1.38	208.1	F			
33rd Street	NB-TR	0.92	36.1	D	0.92	36.1	D			
	NB-R	1.10	83.3	F	1.10	83.3	F			
	Hoyt Ave (EB-LT)	1.00	43.4	D	1.00	43.4	D			
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.38	8.1	А	0.38	8.1	А			
	WB(Ramp)-T	1.05	50.8	D	1.11	72.4	Е			
	NB-L	0.49	29.8	С	0.50	29.9	С			
	SB-R	0.02	25.9	С	0.02	25.9	С			
19. Astoria Boulevard & 8th Street	EB-L	0.06	25.7	С	0.06	25.7	С			
	EB-R	0.39	31.6	С	0.39	31.6	С			
	WB-L	0.26	28.4	С	0.26	28.4	С			
	WB-TR	0.30	29.0	С	0.30	29.0	С			
	NB-LT	0.34	15.0	В	0.43	16.3	В			
	SB-TR	0.31	14.8	В	0.37	15.6	В			
					1					

### Table 13-61: 2023 Future Saturday With-Action Condition-LOS at Analyzed Intersections

		Saturday Midday Peak Hour									
Intersection		NC	)-ACTIO	ON	WITH-ACTION						
	Lane	V/C	Delay	LOS	V/C	Delay	LOS				
	Group	Ratio	(sec.)		Ratio	(sec.)					
24. Hoyt Avenue N. & 21st Street	EB-L	0.05	40.9	D	0.05	40.9	D				
	EB-R	0.27	44.6	D	0.27	44.6	D				
	WB-L	0.89	43.9	D	0.96	49.8	D '				
	WB-TR	0.27	15.1	В	0.27	15.1	В				
	NB-L	0.28	29.1	С	0.29	29.5	С				
	NB-T	0.99	70.7	Е	1.05	87.2	F '				
	SB-TR	0.74	33.9	С	0.77	34.7	С				
25. Hoyt Avenue S./Astoria Park S. &	EB-L	0.18	30.5	С	0.24	31.1	С				
21st Street	EB-TR	0.80	39.5	D	0.83	40.2	D				
	NB-DflL				1.03	106.1	F				
	NB-TR				0.80	24.1	С				
	NB-LTR	0.87	28.2	С		36.4	D				
	SB-LTR	0.98	32.9	С	0.96	29.1	С				
26. 27th Avenue & 9th Street	EB-LT	0.01	8.4	А	0.01	9.3	А				
(Unsignalized-T wo Way Stop)	SB-LR	0.27	19.1	С	1.95	477.0	F ?				

#### <u>Table 13-61 (continued): 2023 Future Saturday With-Action Condition–LOS at Analyzed</u> Intersections

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a significant adverse impact.

Analysis is based on the 2010 *Highway Capacity Manual* methodology (HCS+, version 5.5) *This table is new to the FEIS.* 

#### <u>Table 13-62: Saturday Midday Lane Group LOS Summary Comparison</u> <u>Existing vs. Alternate No-Action Condition</u>

	Existing Conditions	Alternate No-Action Condition
Overall LOS A/B/C	38	37
Overall LOS D	9	9
Overall LOS E	5	1
Overall LOS F	0	5
Number of movements at LOS E or F	5	6

Notes:

This table is new to the FEIS.

Hoyt Avenue South/Astoria Boulevard & 33rd Street

- <u>The Astoria Boulevard eastbound left-turn/through movement would deteriorate from LOS E</u> <u>under Saturday midday existing conditions to LOS F under the alternate No-Action condition.</u>
- The Hoyt Avenue South eastbound left-turn/through movement would deteriorate from LOS C under Saturday midday existing conditions to LOS D under the alternate No-Action condition.
- The 33<sup>rd</sup> Street northbound through-right movement would deteriorate from LOS D (with a v/c ratio of 0.89) under Saturday midday existing conditions to LOS D (with a v/c ratio of 0.92) under the alternate No-Action condition.
- <u>The 33<sup>rd</sup> Street northbound right-turn movement would deteriorate from LOS E under Saturday</u> midday existing conditions to LOS F under the alternate No-Action condition.

		Saturday Midday Peak Hour								
Intersection		E	XISTIN	G		NO-ACTION				
intersection	Lane	V/C	Delay	LOS		V/C Delay LOS				
	Group	Ratio	(sec.)			Ratio	(sec.)			
2. 27th Avenue & 4th Street	EB-LT	NA	8.8	А		NA	8.7	А		
(Unsignalized-All Way Stop)	WB-T	NA	8.7	А		NA	8.7	А		
	WB-R	NA	7.0	А		NA	7.1	А		
	SB-LR	NA	8.5	А		NA	8.3	А		
3. 27th Avenue & 8th Street	EB-TR	0.30	12.8	В		0.28	12.5	В		
	WB-LT	0.27	12.4	В		0.33	13.2	В		
	NB-L	0.14	20.2	С		0.15	20.3	С		
	NB-R	0.16	20.5	С		0.17	20.6	С		
4. 27th Avenue & 12th Street	EB-LT	0.03	7.9	А		0.04	8.0	А		
(Unsignalized-Two Way Stop)	NB-LTR	0.26	14.2	В		0.29	15.3	С		
5. 27th Avenue & 14th Street	EB-TR	NA	9.2	А		NA	9.6	А		
(Unsignalized-All Way Stop)	WB-LT	NA	8.6	А		NA	9.0	А		
	SB-LTR	NA	9.5	А		NA	9.9	А		
6. 27th Avenue & 18th Street	EB-L	0.09	9.4	А		0.10	9.4	А		
(Unsignalized-Two Way Stop)	WB-L	0.01	7.4	А		0.01	7.5	А		
7. Astoria Boulevard & 21st Street	EB-L	0.26	34.0	С		0.29	34.4	С		
	EB-TR	0.37	35.1	D		0.42	35.9	D		
	WB-L	0.64	39.4	D		0.67	40.2	D		
	WB-TR	0.32	34.1	С		0.37	34.7	С		
	NB-LTR	1.05	79.7	Е	*	1.34	198.1	F *		
	SB-LTR	1.05	65.2	Е	*	1.29	171.8	F *		
14. Astoria Boulevard & 31st Street	EB-LTR	1.03	57.0	Е	*	1.16	105.4	F *		
	NB-T	0.74	40.6	D		0.76	42.1	D		
	NB-R	0.57	9.5	А		0.60	10.1	В		
	SB-T	0.70	21.4	С		0.64	19.6	В		
	SB-R	0.35	15.0	В		0.37	15.2	В		
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)		58.2	E	*	1.12	95.1	F *		
33rd Street	NB-TR	0.89	35.1	D		0.92	36.1	D *		
	NB-R	1.05	64.4	E	*	1.10	83.3	F *		
	Hoyt Ave (EB-LT)	0.93	33.6	С	*	0.98	39.0	D *		
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.27	7.1	A		0.37	8.0	A		
	WB(Ramp)-T	0.88	18.9	B		0.95	26.8	C *		
	NB-L SB-R	0.44 0.02	29.3 25.9	C C		0.47 0.02	29.6 25.9	C C		
		<b></b>								
19. Astoria Boulevard & 8th Street	EB-LR	0.09	26.0	С		0.10	26.1	С		
	WB-L	0.16	26.9	С		0.26	28.4	С		
	WB-TR	0.08	25.7	С		0.08	25.8	С		
	NB-LT	0.17	13.1	В		0.18	13.3	В		
	SB-TR	0.19	13.4	В		0.20	13.6	В		

# Table 13-63: Alternate 2023 Future Saturday No-Action Condition–LOS at Analyzed Intersections

### <u>Table 13-63 (continued): Alternate 2023 Future Saturday No-Action Condition–LOS at Analyzed</u> <u>Intersections</u>

		Saturday Midday Peak Hour								
Intersection		EXISTING	NO-ACTION							
	Lane	V/C Delay LOS	V/C Delay LOS							
	Group	Ratio (sec.)	Ratio (sec.)							
24. Hoyt Avenue N. & 21st Street	EB-L	0.05 40.8 D	0.05 40.9 D							
	EB-R	0.26 44.5 D	0.27 44.6 D							
	WB-L	0.62 35.9 D	0.73 38.2 D							
	WB-TR	0.26 15.0 B	0.27 15.1 B							
	NB-L	0.24 28.1 C	0.27 28.8 C							
	NB-T	0.89 52.2 D	0.93 58.4 E *							
	SB-TR	0.68 32.5 C	0.72 33.4 C							
25. Hoyt Avenue S./Astoria Park S.	EB-L	0.15 30.1 C	0.15 30.2 C							
& 21st Street	EB-TR	0.65 36.6 D	0.68 37.1 D							
	NB-LTR	0.70 19.3 B	0.80 23.7 C							
	SB-LTR	0.76 18.4 B	0.87 22.2 C							
26. 27th Avenue & 9th Street	EB-LT	0.00 7.7 A	0.00 7.8 A							
(Unsignalized-T wo Way Stop)	SB-LR	0.06 11.2 B	0.15 12.2 B							

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a congested movement (LOS E or F, or V/C ratio greater than or equal to 0.9)

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version 5.5)

This table is new to the FEIS.

# Astoria Boulevard North & 32<sup>nd</sup> Street

- The westbound through movement at the ramp would deteriorate from LOS B under Saturday midday existing conditions to LOS C (with a v/c ratio of 0.95) under the alternate No-Action condition.

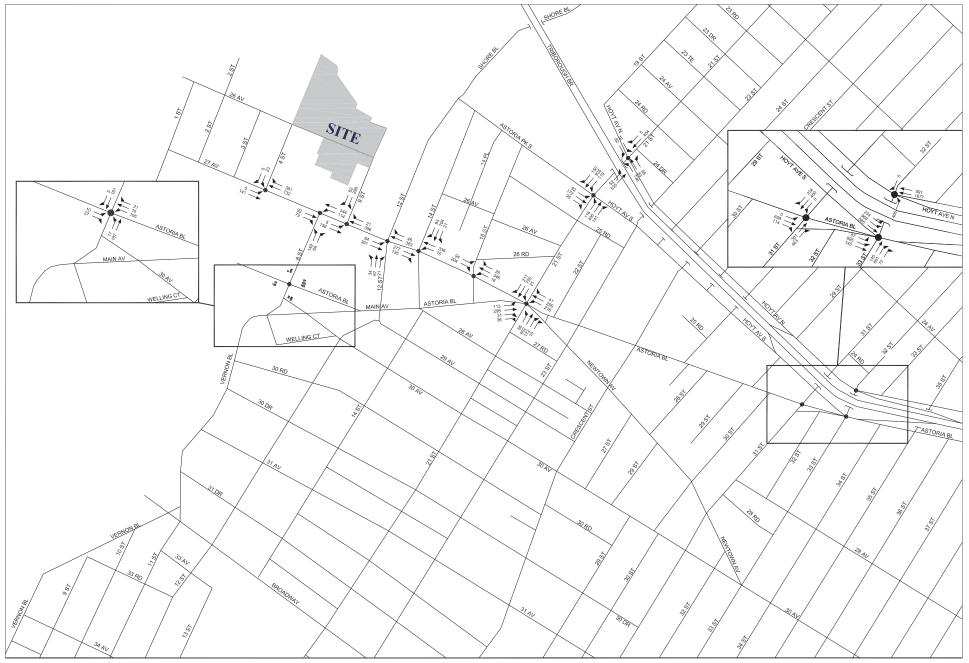
Hoyt Avenue North & 21st Street

- The northbound through movement would deteriorate from LOS D under Saturday midday existing conditions to LOS E under the alternate No-Action condition.

Alternate With-Action Condition Weekend Intersection Capacity Analysis

Figure 13-42 show the traffic network volumes under the alternate With-Action condition for the Saturday midday peak hour. The volumes shown are the sum of the net incremental traffic generated by the Proposed Action and the alternate No-Action traffic network. Table 13-64 shows a summary comparison of the individual lane group LOS for the alternate No-Action and alternate With-Action conditions. As shown in Table 13-64, two individual traffic movements would operate at LOS E and six would operate at LOS F in the Saturday midday peak hour under the alternate With-Action condition. In comparison, 22 of these individual lane groups operate at LOS E or LOS F in one or more weekday peak hour (refer to Table 13-26).

<u>Table 13-65 provides a summary comparison of the impacts disclosed previously for the RWCDS that</u> <u>assumes the completion of the Halletts Point development and those identified in the alternate With-</u> <u>Action condition analysis.</u>



# Astoria Cove

# Figure 13-42

	2023 Alternate No-Action Condition	2023 Alternate With-Action Condition
Overall LOS A/B/C	37	33
Overall LOS D	9	11
Overall LOS E	1	2
Overall LOS F	5	6
Number of movements at LOS E or F	6	8

#### <u>Table 13-64: Saturday Midday Lane Group LOS Summary Comparison</u> <u>Alternate No-Action vs. Alternate With-Action Conditions</u>

This table is new to the FEIS.

#### <u>Table 13-65: Comparison of Saturday Impact Locations—Future with Halletts Point vs. Future</u> without Halletts Point

Intersection	With-Action Condition	Alternate With-Action Condition
2. 27 <sup>th</sup> Ave & 4 <sup>th</sup> St	Х	
3. 27 <sup>th</sup> Ave & 8 <sup>th</sup> St	Х	
4. 27 <sup>th</sup> Ave & 12 <sup>th</sup> St		Х
5. 27 <sup>th</sup> Ave & 14 <sup>th</sup> St		
6. 27 <sup>th</sup> Ave & 18 <sup>th</sup> St		
7. Astoria Blvd & 21 <sup>st</sup> St	Х	Х
14. Astoria Blvd & 31 <sup>st</sup> St		Х
15. Hoyt Ave S./Astoria Blvd & 33 <sup>rd</sup> St	X	Х
18. Astoria Blvd N. & 32 <sup>nd</sup> St	X	
19. Astoria Blvd & 8 <sup>th</sup> St		
24. Hoyt Ave N. & 21 <sup>st</sup> St	Х	Х
25. Hoyt Ave S./Astoria Park S. & 21st St		
26. 27 <sup>th</sup> Avenue & 9 <sup>th</sup> Street	Х	Х

Notes:

With-Action Condition: with Halletts Point development

Alternate With-Action Condition: without Halletts Point development

Bold - denotes where an intersection is signalized in With-Action condition and unsignalized in Alternate

With-Action condition

X – denotes potential for significant adverse impact.

This table is new to the FEIS.

Table 13-66 shows the detailed v/c ratios, delays, and LOS by movement at all analyzed intersections in each peak hour under the alternate With-Action condition and identifies those movements that are considered impacted in one or more peak hours. As shown in Table 13-66, one or more approach or lane group at a total of six of the 13 analyzed intersections would experience significant adverse impacts in the Saturday midday peak hour as a result of the Proposed Action. In comparison, ten of these 13 intersections would experience significant adverse impacts during one or more weekday peak hour under the alternate With-Action condition (refer to Table 13-25). The most significant change in LOS would occur at the 27<sup>th</sup> Avenue and 9<sup>th</sup> Street southbound approach, which would deteriorate from LOS B under the alternate No-Action condition to LOS F under the alternate With-Action condition, due to the significant increase in southbound traffic leaving the project site via 9<sup>th</sup> Street. This approach would similarly operate at LOS F in the weekday AM and PM peak hour under the alternate With-Action Chapter 20, "Mitigation."

		Saturday Midday Peak Hour							
Intersection		NO	-ACTIO	ON	WITH-ACTION				
intersection	Lane	V/C	Delay	LOS	V/C Delay I				
	Group	Ratio	(sec.)		Ratio	(sec.)			
2. 27th Avenue & 4th Street	EB-LT	NA	8.7	А	NA	9.2	А		
(Unsignalized-All Way Stop)	WB-T	NA	8.7	А	NA	8.7	А		
	WB-R	NA	7.1	А	NA	10.8	В		
	SB-LR	NA	8.3	А	NA	8.9	А		
3. 27th Avenue & 8th Street	EB-TR	0.28	12.5	В	0.28	12.5	В		
	WB-LT	0.33	13.2	В	0.78	24.9	С		
	NB-L	0.15	20.3	С	0.29	22.0	С		
	NB-R	0.17	20.6	С	0.17	20.6	С		
4. 27th Avenue & 12th Street	EB-LT	0.04	8.0	А	0.07	8.9	А		
(Unsignalized-Two Way Stop)	NB-LTR	0.29	15.3	С	0.64	44.3	Е	*	
5. 27th Avenue & 14th Street	EB-TR	NA	9.6	А	NA	18.4	С		
(Unsignalized-All Way Stop)	WB-LT	NA	9.0	А	NA	16.9	С		
	SB-LTR	NA	9.9	А	NA	13.3	В		
6. 27th Avenue & 18th Street	EB-LTR	0.10	9.4	А	0.11	9.5	А		
(Unsignalized-Two Way Stop)	WB-LTR	0.01	7.5	А	0.01	7.8	А		
7. Astoria Boulevard & 21st Street	EB-L	0.29	34.4	С	0.33	35.0	С		
	EB-TR	0.42	35.9	D	0.58	38.3	D		
	WB-L	0.67	40.2	D	0.67	40.2	D		
	WB-TR	0.37	34.7	С	0.54	37.0	D		
	NB-LTR	1.34	198.1	F	1.97	480.0	F	*	
	SB-LTR	1.29	171.8	F	1.46	247.8	F	*	
14. Astoria Boulevard & 31st Street	EB-LTR	1.16	105.4	F	1.32	176.3	F	*	
	NB-T	0.76	42.1	D	0.76	42.1	D		
	NB-R	0.60	10.1	В	0.60	10.1	В		
	SB-T	0.64	19.6	В	0.64	19.6	В		
	SB-R	0.37	15.2	В	0.37	15.2	В		
15. Hoyt Avenue S./Astoria Boulevard &	Astoria Blvd (EB-LT)	1.12	95.1	F	1.23	140.8	F	*	
33rd Street	NB-TR	0.92	36.1	D	0.92	36.1	D		
	NB-R	1.10	83.3	F	1.10	83.3	F		
	Hoyt Ave (EB-LT)	0.98	39.0	D	0.98	39.0	D		
18. Astoria Boulevard N. & 32nd Street	WB(Main)-T	0.37	8.0	А	0.37	8.0	А	_	
	WB(Ramp)-T	0.95	26.8	С	1.01	39.3	D		
	NB-L	0.47	29.6	С	0.48	29.7	С		
	SB-R	0.02	25.9	С	0.02	25.9	С		
19. Astoria Boulevard & 8th Street	EB-LR	0.10	26.1	С	0.10	26.1	С	_	
	WB-L	0.26	28.4	С	0.26	28.4	С		
	WB-TR	0.08	25.8	С	0.08	25.8	С		
	NB-LT	0.18	13.3	В	0.28	14.2	В		
	SB-TR	0.20	13.6	В	0.26	14.2	В		

# Table 13-66: Alternate 2023 Future Saturday With-Action Condition-LOS at Analyzed Intersections

		Saturday Midday Peak Hour				
Intersection		NO-ACTION	WITH-ACTION			
intersection	Lane	V/C Delay LOS	V/C Delay LOS			
	Group	Ratio (sec.)	Ratio (sec.)			
24. Hoyt Avenue N. & 21st Street	EB-L	0.05 40.9 D	0.05 40.9 D			
	EB-R	0.27 44.6 D	0.27 44.6 D			
	WB-L	0.73 38.2 D	0.79 39.9 D			
	WB-TR	0.27 15.1 B	0.27 15.1 B			
	NB-L	0.27 28.8 C	0.28 29.2 C			
	NB-T	0.93 58.4 E	0.99 71.2 E *			
	SB-TR	0.72 33.4 C	0.75 34.1 C			
25. Hoyt Avenue S./Astoria Park S.	EB-L	0.15 30.2 C	0.21 30.8 C			
& 21st Street	EB-TR	0.68 37.1 D	0.71 37.6 D			
	NB-LTR	0.80 23.7 C	0.84 26.1 C			
	SB-LTR	0.87 22.2 C	0.92 25.5 C			
26. 27th Avenue & 9th Street	EB-LT	0.00 7.8 A	0.01 8.6 A			
(Unsignalized-Two Way Stop)	SB-LR	0.15 12.2 B	1.16 128.6 F *			

#### Table 13-66: Alternate 2023 Future Saturday With-Action Condition–LOS at Analyzed Intersections

Notes:

EB-Eastbound, WB-Westbound, NB-Northbound, SB-Southbound

L-Left, T-Through, R-Right, DefL-Analysis considers a defacto left lane on this approach

V/C Ratio - Volume to Capacity Ratio, sec/veh - Seconds per Vehicle

LOS - Level of Service

\* - Denotes a significant adverse impact

Analysis is based on the 2010 Highway Capacity Manual methodology (HCS+, version 5.5)

<u>This table is new to the FEIS.</u>

### <u>Transit</u>

As shown in Table 13-55, 732 project-generated subway trips and 151 project-generated bus trips were estimated for the Saturday afternoon peak hour. In comparison, the Saturday peak hour subway trips would be approximately 11 percent less than the maximum subway trips projected for the weekday PM commuter peak hour and approximately the same as the weekday AM commuter peak hour. Although the Proposed Action is projected to result in more than 200 peak hour subway trips in the Saturday midday peak period, these trips would be off-peak when the subway system typically has ample capacity compared to the weekday AM and PM peak hours. These Saturday midday peak hour subway trips would be distributed to the 30<sup>th</sup> Avenue (N and Q lines) Station and the 21<sup>st</sup> Street-Queensbridge (F line) Station and would be evenly split between inbound and outbound trips, unlike commuter peak hour trips, which are more weighted in one direction. With generally lower background ridership levels during the Saturday midday peak hour and the more even distribution of inbound and outbound trips at the subway station elements, the lower number of subway trips generated by the proposed project is not expected to result in the significant adverse fare array or street stair impacts identified at the 30<sup>th</sup> Avenue Station in Section H, "Transit," above.

For buses, the projected Saturday peak hour trips would be distributed to area bus routes with an even split between inbound and outbound trips (unlike the weekday AM and PM peak commuter hours). Due to the more even distribution of the Saturday midday bus person-trips to area bus routes, as compared to the weekday AM and PM peak hours as well as the lower background bus ridership levels during the Saturday midday peak hour, the bus network conditions during the Saturday midday peak hour would be less congested than during the weekday AM and PM peak commuter hours. Therefore, the transit analysis presented above in Section H represents the worst-case condition for analysis purposes.

## **Pedestrians**

As shown in Table 13-55, 1,429 walk-only trips, 732 subway trips, and 151 bus trips were estimated for the Saturday midday peak hour, for a total of 2,312 project-generated pedestrian trips. In comparison, the Saturday peak hour pedestrian trips would be approximately 21 percent less than the maximum pedestrian trips projected for the weekday midday peak hour. In addition, in areas most proximate to the project site (where project-generated pedestrian trips would be highest), background pedestrian levels are generally lower on a Saturday (when there would be substantially fewer employees traveling to/from the project site and surrounding area) than on a weekday. As noted above, the proposed elementary school would be closed on weekends, and, therefore, would not generate pedestrian trips during the Saturday midday peak hour, unlike the weekday peak hours analyzed in Section I, "Pedestrians," above.

As detailed in Section I, the proposed project would not result in any weekday peak hour impacts on the analyzed pedestrian elements. As such, based on the lower anticipated project-generated Saturday midday peak hour increment and background volumes, as well as the results of the weekday midday peak hour pedestrian analyses, it was determined that no significant adverse pedestrian impacts would result in the Saturday midday peak hour.

## <u>Parking</u>

## Existing Conditions

As preliminary analyses indicated that Saturday parking demand could exceed the available accessory off-street parking capacity in the evening and overnight hours, peaking between 5 and 6 PM. Therefore, a detailed parking inventory of the area surrounding the project site was conducted on a typical Saturday for the period when Saturday parking demand is expected to be greatest. Consistent with the weekday parking inventory, the Saturday parking inventory encompassed two study areas: a <sup>1</sup>/<sub>4</sub>-mile radius (approximately a five-minute walk) from the project site, as recommended by CEQR guidelines; and a <sup>1</sup>/<sub>2</sub>-mile radius (approximately a ten-minute walk) from the project site, which is the extent to which drivers would generally go to find available parking. It should be noted that, in the area surrounding the project site, weekend curbside parking regulations are generally more relaxed than on weekdays, with more available on-street parking spaces (refer to Table 13-49).

Table 13-67, below, presents the Saturday evening on-street parking occupancy within a ¼-mile and a ½mile of the project site. As indicated in the table, there are approximately 1,048 parking spaces within a ¼-mile of the project site, 74.6 percent of which were occupied in the Saturday evening hours. Considering the additional 3,014 parking spaces within a ½-mile of the project site, there are approximately 606 parking spaces available in the Saturday evening hours within a ten-minute walk of the project site, for a ½-mile parking utilization rate of 85.1 percent (compared to 90.9 during the weekday late evening hours). There are no public off-street parking facilities within the parking study area.

				Parking Utilization
Study Area	Capacity	Occupied Spaces	Available Spaces	(%)
<sup>1</sup> / <sub>4</sub> -Mile Radius	1,048	782	266	74.6
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	3,014	2,674	340	88.7
Total	4,062	3,456	606	85.1

Table 13-67: Existing Saturday On-Street Parking Conditions

This table is new to the FEIS.

## Future without the Proposed Action (No-Action Condition)

Under the 2023 No-Action condition, background growth in the study area is expected to increase the demand for on-street parking. The same background growth rate assumed for traffic—0.5 percent per year for the first five year and 0.25 percent per year for each additional year until 2023—was applied to determine 2023 No-Action Saturday parking demand. In addition, it is anticipated that parking demand generated by the nearby Halletts Point development will overflow into the surrounding area, and the Halletts Point project will increase the ¼-mile on-street parking capacity by 14 spaces with the extension of Astoria Boulevard through the Astoria Houses campus. As a result of these future No-Action conditions, on-street parking occupancy is expected to reach 94.6 percent in the ¼-mile study area and 92.6 percent in the ¼-mile study area during the Saturday evening hours, decreasing the number of available spaces by 209 in the ¼-mile study area and by a total of 304 spaces in the ½-mile study area (see Table 13-68). In comparison, during the weekday evening hours, the No-Action ½-mile parking utilization rate is expected to be approximately 94.5 percent.

### Table 13-68: 2023 Saturday No-Action On-Street Parking Conditions

				Parking Utilization
Study Area	Capacity <sup>1</sup>	<b>Occupied Spaces<sup>2</sup></b>	Available Spaces	(%)
<sup>1</sup> /4-Mile Radius	1,062	1,005	57	94.6
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	3,014	2,769	245	91.9
Total	4,076	3,774	302	92.6

Notes:

<sup>1</sup> Includes a net 14 additional on-street parking spaces created as part of the Halletts Point project.

<sup>2</sup> Reflects general background growth and evening overflow parking demand from the Halletts Point project.

This table is new to the FEIS.

### Future with the Proposed Action (With-Action Condition)

Table 13-69 shows the 24-hour parking accumulation that is expected to be generated by each land use included in the Proposed Action. As indicated in Table 13-69, the peak Saturday parking demand (1,005) would occur between 5 and 6 PM on Saturdays, compared to 8-9 PM on weekdays. During this peak period, the Proposed Action would result in a shortfall of approximately 105 parking spaces. As indicated in Table 13-70, peak parking demand could be absorbed by available on-street spaces within the parking study area. Therefore, it is not expected that the Proposed Action would result in a significant adverse parking impact.

	Local			market	Residential <sup>1</sup>		
10.1.434	In	Out	In	Out	In	Out	Total Accumulation
12-1 AM	0	0	0	0	22	22	948
1-2	0	0	0	0	22	22	948
2-3	0	0	0	0	11	11	948
3-4	0	0	0	0	4	4	948
4-5	0	0	0	0	4	4	948
5-6	0	0	0	0	4	7	945
6-7	0	0	10	9	6	15	937
7-8	1	0	31	10	22	69	912
8-9	3	3	55	52	69	163	821
9-10	2	2	65	31	130	172	813
10-11	6	4	76	42	130	195	784
11-12	6	6	87	66	163	163	805
12-1 PM	8	8	104	96	187	187	813
1-2	8	7	102	94	186	186	822
2-3	8	5	94	120	167	167	799
3-4	6	6	98	124	178	134	817
4-5	7	7	98	131	235	100	819
5-6	8	8	112	107	208	127	1,005
6-7	5	7	86	98	163	163	991
7-8	4	7	65	53	139	139	1,000
8-9	3	5	20	31	93	93	987
9-10	2	2	10	20	69	69	977
10-11	0	0	0	20	69	69	957
11-12	0	0	0	9	57	57	948
Overnight Demand 948						<i>94</i> 8	

### **Table 13-69: Saturday Parking Accumulation Forecast**

Sources: Local retail temporal distribution based on the 2004 No. 7 Subway Extension – Hudson Yards Rezoning and Development Program FGEIS; supermarket temporal distribution based on the 2005 Van Courtland Center EAS; residential temporal distribution based on 1993 ABC West Avenue Properties FEIS.

Notes: 25 percent link trip credit applied to Retail and Supermarket land use.

<sup>1</sup> No credit was taken for the 166 residential units in upland area in No-Action condition. This table is new to the FEIS.

#### Table 13-70: 2023 Saturday With-Action Parking Conditions

				Parking Utilization
Location	Capacity <sup>1</sup>	Occupied Spaces	Available Spaces	(%)
Project Site Off-Street	900	900	0	100.0
<sup>1</sup> /4-Mile Radius	1,062	1,062	0	100.0
<sup>1</sup> / <sub>4</sub> - to <sup>1</sup> / <sub>2</sub> -Mile Radius	3,014	2,817	197	93.5
Total	4,976	4,779	197	96.0

Notes: <sup>1</sup> Includes a net 14 additional on-street parking spaces created as part of the Halletts Point project. This table is new to the FEIS.